



COMUNE DI SAN BARTOLOMEO IN GALDO

Provincia di Benevento

PROGETTO:

PROGETTO PER IL RISANAMENTO IDROGEOLOGICO
DELLE AREE A VALLE DEL CENTRO ABITATO

PROGETTO ESECUTIVO

I° STRALCIO FUNZIONALE

DESCRIZIONE ELABORATO:

Relazione geotecnica

LOCALITA' VADORICCI

PROGRESSIVO

CODICE

16

R.1.6

SCALA:

-

RTP PROGETTAZIONE:

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Geotecnica
Elenco colonne stratigrafiche

Simbologia

St.

=Strato

z

=Profondità della superficie superiore dello strato

Unità geotecnica

=Unità geotecnica

Class.

=Classificazione

Coes.

= Coesivo

Inc.

= Incoerente

Roc.

= Roccia

N. c.

= Non classificato

Colonna stratigrafica numero 1

St.	z <m>	Unità geotecnica	Class.
1	0	1 Argilla bassa o media plasticità alta consistenza	Coes.

Falda non presente

Elenco unità geotecniche

1 Argilla bassa o media plasticità alta consistenza:

Classificazione: Coesivo

- Pesi:
- Peso specifico del terreno naturale: $\gamma = 1900.00$ daN/mc
 - Peso specifico del terreno saturo: $\gamma_{sat} = 1950.00$ daN/mc

- Proprietà indice:
- Indice di plasticità: $I_p = 10.00$ <%>
- Parametri plastici:
- Angolo di attrito efficace: $\phi' = 20.00$ grad
 - Coesione efficace: $c' = 2000.00$ daN/mq
 - Coesione non drenata: $c_u = 20000.00$ daN/mq
- Caratteristiche litostatiche:
- Grado di sovraconsolidazione: $OCR = 1.00$
 - Coeff. di spinta a riposo: $\kappa_0 = 0.66$

- Parametri elastici:
- Modulo elastico normale: $E = 750000.00$ daN/mq
 - Modulo elastico tangenziale: $G = 267857.00$ daN/mq
 - Esponente del parametro tensionale: $k_j = 0.00$
 - Coeff. di Poisson: $\nu = 0.40$
 - Modulo edometrico: $E_{ed} = 1610000.00$ daN/mq
 - Modulo elastico non drenato: $E_u = 803571.00$ daN/mq

Report grafico complessivo

Colonna stratigrafica numero 1

Simbologia

St.

=Strato

z

=Profondità della superficie superiore dello strato

Unità geotecnica

=Unità geotecnica

Class.

=Classificazione

Coes.

= Coesivo

Inc.

= Incoerente

Roc.

= Roccia

N. c.

= Non classificato

γ

=Peso specifico del terreno naturale

γ_{sat}

=Peso specifico del terreno saturo

D_r

=Densità relativa

I_p

=Indice di plasticità

ϕ'

=Angolo di attrito efficace

c'

=Coesione efficace

c_u

=Coesione non drenata

OCR

=Grado di sovraconsolidazione

κ_0

=Coeff. di spinta a riposo

Crit.

=Criterio di progetto

St.	z <m>	Unità geotecnica	Class.	γ <daN/mc>	γ_{sat} <daN/mc>	D_r	I_p	ϕ' <grad>	c' <daN/mq>	c_u <daN/mq>	OCR	κ_0	Crit.
1	0	1 Argilla bassa o media plasticità alta consistenza	Coes.	1900	1950	0	10	20	2000	20000	1	0.66	1

Simbologia

St.

=Strato

Relazione geotecnica

z = Profondità della superficie superiore dello strato
 Unità geotecnica = Unità geotecnica
 Class. = Classificazione
 Coes. = Coesivo
 Inc. = Incoerente
 Roc. = Roccia
 N. c. = Non classificato
 γ = Peso specifico del terreno naturale
 γ_{sat} = Peso specifico del terreno saturo
 D_r = Densità relativa
 I_p = Indice di plasticità
 ϕ' = Angolo di attrito efficace
 c' = Coesione efficace
 c_u = Coesione non drenata
 OCR = Grado di sovraconsolidazione
 κ_0 = Coeff. di spinta a riposo
 Crit. = Criterio di progetto

St.	z	E	G	k_j	ν	E_{ed}	E_u	Crit.
	<m>	<daN/mq>	<daN/mq>			<daN/mq>	<daN/mq>	
1	0	750000	267857	0	0.4	1610000	803571	1

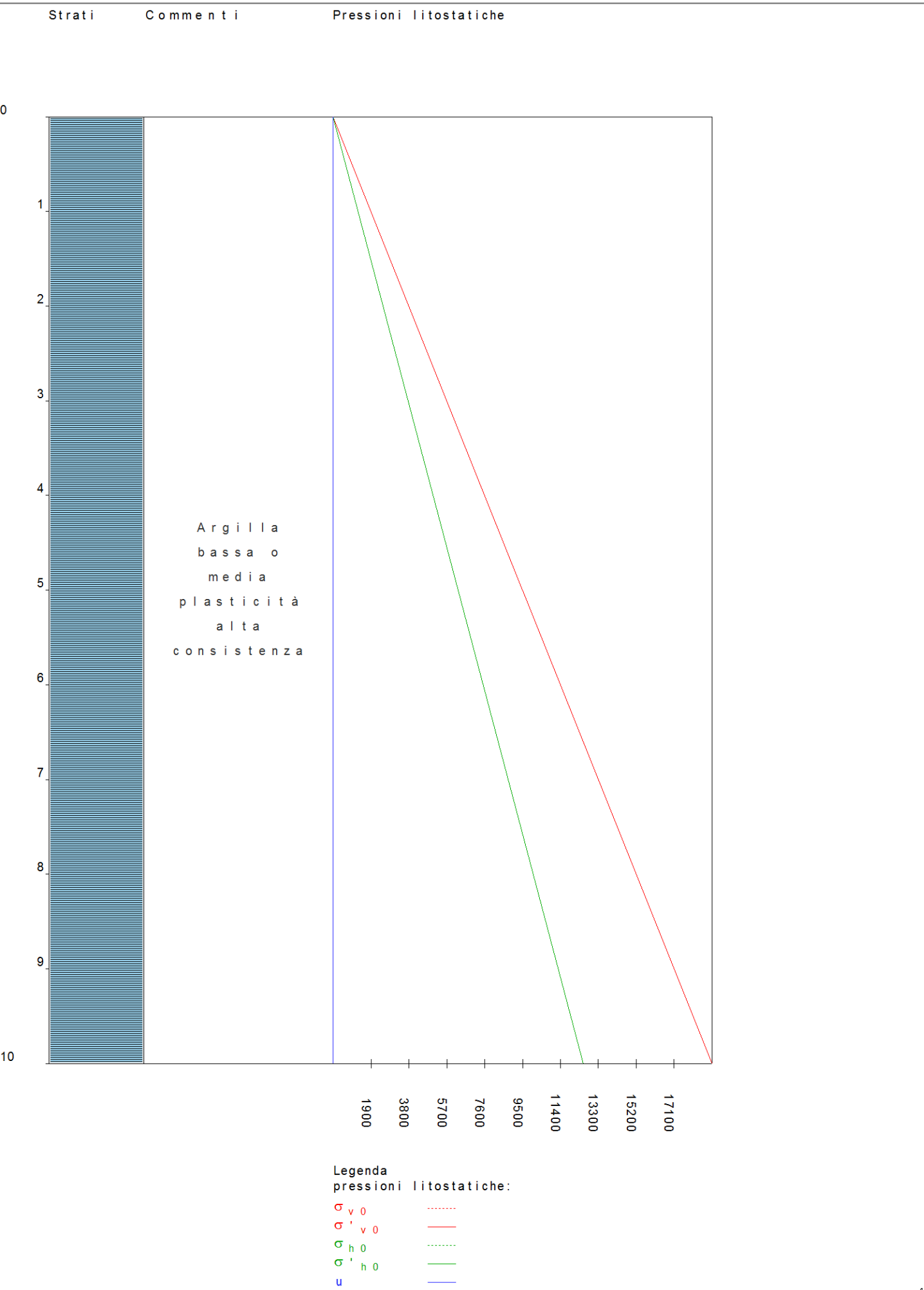


Figura numero 1: Colonna stratigrafica numero 1

Le verifiche degli elementi di fondazione sono state effettuate utilizzando l'approccio 2.

Coefficienti parziali per le azioni, per verifiche in condizioni statiche:

Permanenti strutturali, sicurezza a favore $\gamma_A = 1.00$;
 Permanenti strutturali, sicurezza a sfavore $\gamma_A = 1.30$;
 Permanenti non strutturali, sicurezza a favore $\gamma_A = 0.00$;
 Permanenti non strutturali, sicurezza a sfavore $\gamma_A = 1.50$;
 Variabili, sicurezza a favore $\gamma_A = 0.00$;
 Variabili, sicurezza a sfavore $\gamma_A = 1.50$.

I coefficienti parziali per le azioni sono posti pari all'unità per le verifiche in condizioni sismiche.

Tali coefficienti sono comunque desumibili dalla tabella delle combinazioni delle CCE (Parametri di calcolo).

Coefficienti parziali per i parametri geotecnici:

Tangente dell'angolo di attrito $\gamma_M = 1.00$;
 Coesione efficace $\gamma_M = 1.00$;
 Coesione non drenata $\gamma_M = 1.00$;

Coefficienti parziali per la resistenza delle fondazioni superficiali:

Capacità portante $\gamma_R = 2.30$;
 Scorrimento $\gamma_R = 1.10$;
 Coefficienti parziali per la resistenza delle fondazioni profonde:
 Per pali infissi:

Resistenza alla base $\gamma_{R,b} = 1.15$;
 Resistenza laterale in compressione $\gamma_{R,s} = 1.15$;
 Resistenza laterale in trazione $\gamma_{R,t} = 1.25$;

Per pali trivellati:

Resistenza alla base $\gamma_{R,b} = 1.35$;
 Resistenza laterale in compressione $\gamma_{R,s} = 1.15$;
 Resistenza laterale in trazione $\gamma_{R,t} = 1.25$;

Per pali ad elica continua:

Resistenza alla base $\gamma_{R,b} = 1.30$;
 Resistenza laterale in compressione $\gamma_{R,s} = 1.15$;
 Resistenza laterale in trazione $\gamma_{R,t} = 1.25$;

Fattore di correlazione per la determinazione della resistenza caratteristica desumibile dai criteri di progetto.

Fondazioni superficiali

Simbologia

B = Base della fondazione
 L = Lunghezza della fondazione ($L > B$)
 D = Profondità del piano di posa della fondazione
 β = Inclinazione del piano di campagna
 η = Inclinazione del piano di posa della fondazione
 γ_r = Peso specifico rappresentativo del terreno di fondazione
 $\sigma_{v0,f}$ = Pressione verticale alla profondità del piano di posa della fondazione
 ϕ'_r = Angolo di attrito rappresentativo del terreno di fondazione
 c'_r = Coesione efficace rappresentativa del terreno di fondazione
 N_q = Coefficiente di capacità portante relativo al sovraccarico laterale
 N_c = Coefficiente di capacità portante relativo alla coesione del terreno di fondazione
 N_g = Coefficiente di capacità portante relativo al peso del terreno di fondazione
 b_q = Fattore di inclinazione del piano di fondazione relativo a sovraccarico laterale
 b_c = Fattore di inclinazione del piano di fondazione relativo a coesione
 b_g = Fattore di inclinazione del piano di fondazione relativo a peso del terreno
 c_{ur} = Coesione non drenata rappresentativa del terreno di fondazione
 CC = Numero della combinazione delle condizioni di carico elementari
 N = Sforzo normale
 Tx = Taglio in dir. X
 Ty = Taglio in dir. Y
 Mx = Momento intorno all'asse X
 My = Momento intorno all'asse Y
 B' = Base della fondazione reagente
 L' = Lunghezza della fondazione reagente
 s_q = Fattore di forma relativo al sovraccarico laterale
 s_c = Fattore di forma relativo alla coesione
 s_g = Fattore di forma relativo al peso del terreno
 i_q = Fattore di inclinazione relativo al sovraccarico laterale
 i_c = Fattore di inclinazione relativo alla coesione
 i_g = Fattore di inclinazione relativo al peso del terreno
 q_{lim} = Pressione limite
 R_d = Resistenza di progetto (Carico limite)
 Sic. = Sicurezza a rottura

Verifiche capacità portante

Verifiche di capacità portante per rottura generale in condizioni statiche

Metodo utilizzato: Indicazioni EC7

Travata 401

B=0.40 <m> L=42.46 <m> D=1.00 <m> $\beta=0.00$ <grad> $\eta=0.00$ <grad> $\gamma_r=1900.00$ <daN/mc>
 $\sigma_{v0,r}=1900.00$ <daN/mq>

Verifiche in condizioni drenate

$\phi'_r=20.00$ <grad> $c'_r=2000.00$ <daN/mq>
 $N_q=6.40$ $N_c=14.83$ $N_g=3.93$ $b_q=1.00$ $b_c=1.00$ $b_g=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _q	s _c	s _g	i _q	i _c	i _g	q _{lim} <daN/mq>	R _d <daN>	Sic.
33	216373	3690.28	10254.6	88.45	90978.6	0.4	41.62	1	1	1	1	1	1	43469.7	313995	1.45
34	216491	9601.79	10299.7	88.4	99493.9	0.4	41.54	1	1	1	1	1	1	43470	313408	1.45
35	214075	6601.72	8661.13	82.6	94505.6	0.4	41.58	1	1	1	1	1	1	43470.1	313717	1.47
36	218790	6690.35	11893.3	94.25	95966.9	0.4	41.58	1	1	1	1	1	1	43469.7	313686	1.43

Verifiche in condizioni non drenate

c_{ur}=20000.00 <daN/mq>
 $N_q=1.00$ $N_c=5.14$ $b_q=0.00$ $b_c=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _c	i _q	i _c	q _{lim} <daN/mq>	R _d <daN>	Sic.
33	216373	3690.28	10254.6	88.45	90978.6	0.4	41.62	1	0	1	104929	757935	3.5
34	216491	9601.79	10299.7	88.4	99493.9	0.4	41.54	1	0	1	104930	756515	3.49
35	214075	6601.72	8661.13	82.6	94505.6	0.4	41.58	1	0	1	104929	757259	3.54
36	218790	6690.35	11893.3	94.25	95966.9	0.4	41.58	1	0	1	104929	757192	3.46

Verifiche di capacità portante per rottura generale in condizioni statiche

Metodo utilizzato: Indicazioni EC7

Travata 402

B=0.40 <m> L=35.61 <m> D=1.00 <m> $\beta=0.00$ <grad> $\eta=0.00$ <grad> $\gamma_r=1900.00$ <daN/mc>
 $\sigma_{v0,r}=1900.00$ <daN/mq>

Verifiche in condizioni drenate

$\phi'_r=20.00$ <grad> $c'_r=2000.00$ <daN/mq>
 $N_q=6.40$ $N_c=14.83$ $N_g=3.93$ $b_q=1.00$ $b_c=1.00$ $b_g=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _q	s _c	s _g	i _q	i _c	i _g	q _{lim} <daN/mq>	R _d <daN>	Sic.
33	184646	-6597.26	-7566.56	-17.37	89968.4	0.4	34.64	1	1	1	1	1	1	43502.8	261919	1.42
34	184790	-1504.75	-7562.27	-17.56	96357.5	0.4	34.57	1	1	1	1	1	1	43503.2	261402	1.41
35	186886	-4121.05	-8981.02	-12.04	94030.6	0.4	34.6	1	1	1	1	1	1	43503.2	261720	1.4
36	182550	-3980.95	-6147.81	-22.89	92295.3	0.4	34.6	1	1	1	1	1	1	43502.7	261600	1.43

Verifiche in condizioni non drenate

c_{ur}=20000.00 <daN/mq>
 $N_q=1.00$ $N_c=5.14$ $b_q=0.00$ $b_c=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _c	i _q	i _c	q _{lim} <daN/mq>	R _d <daN>	Sic.
33	184646	-6597.26	-7566.56	-17.37	89968.4	0.4	34.64	1	0	1	104969	631992	3.42
34	184790	-1504.75	-7562.27	-17.56	96357.5	0.4	34.57	1	0	1	104970	630744	3.41
35	186886	-4121.05	-8981.02	-12.04	94030.6	0.4	34.6	1	0	1	104970	631507	3.38
36	182550	-3980.95	-6147.81	-22.89	92295.3	0.4	34.6	1	0	1	104970	631225	3.46

Verifiche di capacità portante per rottura generale in condizioni statiche

Metodo utilizzato: Indicazioni EC7

Travata 403

B=0.40 <m> L=12.19 <m> D=1.00 <m> $\beta=0.00$ <grad> $\eta=0.00$ <grad> $\gamma_r=1900.00$ <daN/mc>
 $\sigma_{v0,r}=1900.00$ <daN/mq>

Verifiche in condizioni drenate

$\phi'_r=20.00$ <grad> $c'_r=2000.00$ <daN/mq>
 $N_q=6.40$ $N_c=14.83$ $N_g=3.93$ $b_q=1.00$ $b_c=1.00$ $b_g=1.00$

CC	N <daN>	T _x <daN>	T _y <daN>	M _x <daNm>	M _y <daNm>	B' <m>	L' <m>	s _q	s _c	s _g	i _q	i _c	i _g	q _{lim} <daN/mq>	R _d <daN>	Sic.
33	129529	9144.1	-536.92	-16.46	12275.8	0.4	12	1.01	1.01	0.99	1	1	1	43845.1	91448.2	0.71
34	131106	10498	-532.92	-12.92	12349.1	0.4	12	1.01	1.01	0.99	1	1	1	43845.4	91470.6	0.7
35	130275	9801.68	-1605.9	-14.7	8556.92	0.4	12.06	1.01	1.01	0.99	1	1	1	43842.7	91893.1	0.71
36	130360	9840.46	536.06	-14.68	16068	0.4	11.94	1.01	1.01	0.99	1	1	1	43847.8	91026.1	0.7

Verifiche in condizioni non drenate

$c_{ur}=20000.00$ <daN/mq>
 $N_q=1.00$ $N_c=5.14$ $b_q=0.00$ $b_c=1.00$

CC	N <daN>	T _x <daN>	T _y <daN>	M _x <daNm>	M _y <daNm>	B' <m>	L' <m>	s _c	i _q	i _c	q _{lim} <daN/mq>	R _d <daN>	Sic.
33	129529	9144.1	-536.92	-16.46	12275.8	0.4	12	1.01	0	1	105417	219869	1.7
34	131106	10498	-532.92	-12.92	12349.1	0.4	12	1.01	0	1	105417	219922	1.68
35	130275	9801.68	-1605.9	-14.7	8556.92	0.4	12.06	1.01	0	1	105414	220944	1.7
36	130360	9840.46	536.06	-14.68	16068	0.4	11.94	1.01	0	1	105420	218848	1.68

Verifiche di capacità portante per rottura generale in condizioni statiche

Metodo utilizzato: Indicazioni EC7

Travata 404

$B=0.40$ <m> $L=12.19$ <m> $D=1.00$ <m> $\beta=0.00$ <grad> $\eta=0.00$ <grad> $\gamma_r=1900.00$ <daN/mc>
 $\sigma_{v0,r}=1900.00$ <daN/mq>

Verifiche in condizioni drenate

$\phi'_r=20.00$ <grad> $c'_r=2000.00$ <daN/mq>
 $N_q=6.40$ $N_c=14.83$ $N_g=3.93$ $b_q=1.00$ $b_c=1.00$ $b_g=1.00$

CC	N <daN>	T _x <daN>	T _y <daN>	M _x <daNm>	M _y <daNm>	B' <m>	L' <m>	s _q	s _c	s _g	i _q	i _c	i _g	q _{lim} <daN/mq>	R _d <daN>	Sic.
33	149736	10511.4	327.92	28.25	13830.1	0.4	12.01	1.01	1.01	0.99	1	1	1	43844.3	91455	0.61
34	150140	13244.4	339.02	26.08	13888.7	0.4	12.01	1.01	1.01	0.99	1	1	1	43844.5	91460	0.61
35	149900	11846.3	-966.28	27.18	10496.8	0.4	12.05	1.01	1.01	0.99	1	1	1	43842.4	91794.8	0.61
36	149977	11909.5	1633.23	27.15	17222	0.4	11.96	1.01	1.01	0.99	1	1	1	43846.4	91120.5	0.61

Verifiche in condizioni non drenate

$c_{ur}=20000.00$ <daN/mq>
 $N_q=1.00$ $N_c=5.14$ $b_q=0.00$ $b_c=1.00$

CC	N <daN>	T _x <daN>	T _y <daN>	M _x <daNm>	M _y <daNm>	B' <m>	L' <m>	s _c	i _q	i _c	q _{lim} <daN/mq>	R _d <daN>	Sic.
33	149736	10511.4	327.92	28.25	13830.1	0.4	12.01	1.01	0	1	105416	219889	1.47
34	150140	13244.4	339.02	26.08	13888.7	0.4	12.01	1.01	0	1	105417	219900	1.46
35	149900	11846.3	-966.28	27.18	10496.8	0.4	12.05	1.01	0	1	105414	220710	1.47
36	149977	11909.5	1633.23	27.15	17222	0.4	11.96	1.01	0	1	105419	219079	1.46

Verifiche di capacità portante per rottura generale in condizioni statiche

Metodo utilizzato: Indicazioni EC7

Travata 405

$B=0.40$ <m> $L=12.19$ <m> $D=1.00$ <m> $\beta=0.00$ <grad> $\eta=0.00$ <grad> $\gamma_r=1900.00$ <daN/mc>
 $\sigma_{v0,r}=1900.00$ <daN/mq>

Verifiche in condizioni drenate

$\phi'_r=20.00$ <grad> $c'_r=2000.00$ <daN/mq>
 $N_q=6.40$ $N_c=14.83$ $N_g=3.93$ $b_q=1.00$ $b_c=1.00$ $b_g=1.00$

CC	N <daN>	T _x <daN>	T _y <daN>	M _x <daNm>	M _y <daNm>	B' <m>	L' <m>	s _q	s _c	s _g	i _q	i _c	i _g	q _{lim} <daN/mq>	R _d <daN>	Sic.
33	157841	5538.17	1223.19	3.89	16344	0.4	11.98	1.01	1.01	0.99	1	1	1	43846.9	91365	0.58
34	157866	8646.3	1243.08	2.81	16399	0.4	11.98	1.01	1.01	0.99	1	1	1	43847	91363.3	0.58
35	157816	7057.97	-95.8	3.35	13084.6	0.4	12.02	1.01	1.01	0.99	1	1	1	43845.1	91677.5	0.58
36	157891	7126.5	2562.07	3.34	19658.4	0.4	11.94	1.01	1.01	0.99	1	1	1	43848.8	91050.9	0.58

Verifiche in condizioni non drenate

Relazione geotecnica

$c_{ur}=20000.00$ <daN/mq>
 $N_q=1.00$ $N_c=5.14$ $b_q=0.00$ $b_c=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _c	i _q	i _c	Q _{lim} <daN/mq>	R _d <daN>	Sic.
33	157841	5538.17	1223.19	3.89	16344	0.4	11.98	1.01	0	1	105418	219663	1.39
34	157866	8646.3	1243.08	2.81	16399	0.4	11.98	1.01	0	1	105418	219658	1.39
35	157816	7057.97	-95.8	3.35	13084.6	0.4	12.02	1.01	0	1	105416	220418	1.4
36	157891	7126.5	2562.07	3.34	19658.4	0.4	11.94	1.01	0	1	105421	218903	1.39

Verifiche di capacità portante per rottura generale in condizioni statiche

Metodo utilizzato: Indicazioni EC7

Travata 406

$B=0.40$ <m> $L=12.19$ <m> $D=1.00$ <m> $\beta=0.00$ <grad> $\eta=0.00$ <grad> $\gamma_r=1900.00$ <daN/mc>
 $\sigma_{v0,r}=1900.00$ <daN/mq>

Verifiche in condizioni drenate

$\phi'_r=20.00$ <grad> $c'_r=2000.00$ <daN/mq>
 $N_q=6.40$ $N_c=14.83$ $N_g=3.93$ $b_q=1.00$ $b_c=1.00$ $b_g=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _q	s _c	s _g	i _q	i _c	i _g	Q _{lim} <daN/mq>	R _d <daN>	Sic.
33	158277	1895.73	1862.68	-5.03	20176	0.4	11.94	1.01	1.01	0.99	1	1	1	43849	91001.1	0.57
34	158267	5078.39	1885.39	-5.89	20258.8	0.4	11.93	1.01	1.01	0.99	1	1	1	43849	90990.6	0.57
35	158227	3446.25	531.05	-5.48	16931	0.4	11.98	1.01	1.01	0.99	1	1	1	43847.1	91308.2	0.58
36	158317	3527.87	3217.02	-5.44	23503.9	0.4	11.89	1.01	1.01	0.99	1	1	1	43850.8	90683.7	0.57

Verifiche in condizioni non drenate

$c_{ur}=20000.00$ <daN/mq>
 $N_q=1.00$ $N_c=5.14$ $b_q=0.00$ $b_c=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _c	i _q	i _c	Q _{lim} <daN/mq>	R _d <daN>	Sic.
33	158277	1895.73	1862.68	-5.03	20176	0.4	11.94	1.01	0	1	105421	218784	1.38
34	158267	5078.39	1885.39	-5.89	20258.8	0.4	11.93	1.01	0	1	105421	218758	1.38
35	158227	3446.25	531.05	-5.48	16931	0.4	11.98	1.01	0	1	105419	219526	1.39
36	158317	3527.87	3217.02	-5.44	23503.9	0.4	11.89	1.01	0	1	105423	218016	1.38

Verifiche di capacità portante per rottura generale in condizioni statiche

Metodo utilizzato: Indicazioni EC7

Travata 407

$B=0.40$ <m> $L=12.19$ <m> $D=1.00$ <m> $\beta=0.00$ <grad> $\eta=0.00$ <grad> $\gamma_r=1900.00$ <daN/mc>
 $\sigma_{v0,r}=1900.00$ <daN/mq>

Verifiche in condizioni drenate

$\phi'_r=20.00$ <grad> $c'_r=2000.00$ <daN/mq>
 $N_q=6.40$ $N_c=14.83$ $N_g=3.93$ $b_q=1.00$ $b_c=1.00$ $b_g=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _q	s _c	s _g	i _q	i _c	i _g	Q _{lim} <daN/mq>	R _d <daN>	Sic.
33	150780	-7331.15	1315.37	-26.27	30058.1	0.4	11.79	1.01	1.01	0.99	1	1	1	43854	89851.3	0.6
34	150726	-4225	1321.9	-27.42	30264.6	0.4	11.79	1.01	1.01	0.99	1	1	1	43854	89825.9	0.6
35	150688	-5829.8	-42.84	-26.87	26907	0.4	11.83	1.01	1.01	0.99	1	1	1	43852	90162.3	0.6
36	150817	-5726.36	2680.11	-26.82	33415.6	0.4	11.75	1.01	1.01	0.99	1	1	1	43855.9	89515.1	0.59

Verifiche in condizioni non drenate

$c_{ur}=20000.00$ <daN/mq>
 $N_q=1.00$ $N_c=5.14$ $b_q=0.00$ $b_c=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _c	i _q	i _c	Q _{lim} <daN/mq>	R _d <daN>	Sic.
33	150780	-7331.15	1315.37	-26.27	30058.1	0.4	11.79	1.01	0	1	105429	216011	1.43
34	150726	-4225	1321.9	-27.42	30264.6	0.4	11.79	1.01	0	1	105429	215950	1.43
35	150688	-5829.8	-42.84	-26.87	26907	0.4	11.83	1.01	0	1	105427	216763	1.44
36	150817	-5726.36	2680.11	-26.82	33415.6	0.4	11.75	1.01	0	1	105432	215198	1.43

Verifiche di capacità portante per rottura generale in condizioni statiche

Relazione geotecnica

Metodo utilizzato: Indicazioni EC7

Travata 408

B=0.40 <m> L=12.19 <m> D=1.00 <m> β =0.00 <grad> η =0.00 <grad> γ_r =1900.00 <daN/mc>
 $\sigma_{v0, f}$ =1900.00 <daN/mq>

Verifiche in condizioni drenate

ϕ'_r =20.00 <grad> c'_r =2000.00 <daN/mq>
 N_q =6.40 N_c =14.83 N_g =3.93 b_q =1.00 b_c =1.00 b_g =1.00

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _q	s _c	s _g	i _q	i _c	i _g	Q _{lim} <daN/mq>	R _d <daN>	Sic.
33	119500	-18769.7	-1803.1	-90.67	53168.6	0.4	11.3	1.01	1.01	0.99	1	1	1	43871.2	85890.5	0.72
34	119140	-16021.3	-1833.85	-92.43	53593.4	0.4	11.29	1.01	1.01	0.99	1	1	1	43871.5	85809.1	0.72
35	119259	-17360.3	-3199.92	-91.47	50193.1	0.4	11.35	1.01	1.01	0.99	1	1	1	43868.8	86247.7	0.72
36	119382	-17430.7	-437.04	-91.64	56568.9	0.4	11.24	1.01	1.01	0.99	1	1	1	43874	85452.4	0.72

Verifiche in condizioni non drenate

c_{ur} =20000.00 <daN/mq>
 N_q =1.00 N_c =5.14 b_q =0.00 b_c =1.00

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _c	i _q	i _c	Q _{lim} <daN/mq>	R _d <daN>	Sic.
33	119500	-18769.7	-1803.1	-90.67	53168.6	0.4	11.3	1.01	0	1	105457	206463	1.73
34	119140	-16021.3	-1833.85	-92.43	53593.4	0.4	11.29	1.01	0	1	105458	206267	1.73
35	119259	-17360.3	-3199.92	-91.47	50193.1	0.4	11.35	1.01	0	1	105454	207327	1.74
36	119382	-17430.7	-437.04	-91.64	56568.9	0.4	11.24	1.01	0	1	105461	205404	1.72

Verifiche di capacità portante per rottura generale in condizioni statiche

Metodo utilizzato: Indicazioni EC7

Travata 409

B=0.40 <m> L=3.54 <m> D=1.00 <m> β =0.00 <grad> η =0.00 <grad> γ_r =1900.00 <daN/mc>
 $\sigma_{v0, f}$ =1900.00 <daN/mq>

Verifiche in condizioni drenate

ϕ'_r =20.00 <grad> c'_r =2000.00 <daN/mq>
 N_q =6.40 N_c =14.83 N_g =3.93 b_q =1.00 b_c =1.00 b_g =1.00

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _q	s _c	s _g	i _q	i _c	i _g	Q _{lim} <daN/mq>	R _d <daN>	Sic.
33	43402.9	-5668.4	160.73	-28.75	6535	0.4	3.24	1.04	1.05	0.96	1	1	1	45253.1	25420.6	0.59
34	42820.4	-5039.45	227.83	-30.06	6474.52	0.4	3.24	1.04	1.05	0.96	1	1	1	45253.2	25405.7	0.59
35	42612.5	-5374.17	-21.33	-29.89	6327.14	0.4	3.24	1.04	1.05	0.96	1	1	1	45249.9	25446.6	0.6
36	43610.8	-5333.68	409.89	-28.92	6682.37	0.4	3.24	1.04	1.05	0.96	1	1	1	45256.3	25380.6	0.58

Verifiche in condizioni non drenate

c_{ur} =20000.00 <daN/mq>
 N_q =1.00 N_c =5.14 b_q =0.00 b_c =1.00

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _c	i _q	i _c	Q _{lim} <daN/mq>	R _d <daN>	Sic.
33	43402.9	-5668.4	160.73	-28.75	6535	0.4	3.24	1.02	0	1	107262	60253.7	1.39
34	42820.4	-5039.45	227.83	-30.06	6474.52	0.4	3.24	1.02	0	1	107262	60218.4	1.41
35	42612.5	-5374.17	-21.33	-29.89	6327.14	0.4	3.24	1.02	0	1	107258	60317.3	1.42
36	43610.8	-5333.68	409.89	-28.92	6682.37	0.4	3.24	1.02	0	1	107266	60156.9	1.38

Verifiche di capacità portante per rottura generale in condizioni statiche

Metodo utilizzato: Indicazioni EC7

Travata 411

B=0.40 <m> L=3.35 <m> D=1.00 <m> β =0.00 <grad> η =0.00 <grad> γ_r =1900.00 <daN/mc>
 $\sigma_{v0, f}$ =1900.00 <daN/mq>

Verifiche in condizioni drenate

ϕ'_r =20.00 <grad> c'_r =2000.00 <daN/mq>
 N_q =6.40 N_c =14.83 N_g =3.93 b_q =1.00 b_c =1.00 b_g =1.00

CC	N	Tx	Ty	Mx	My	B'	L'	s _q	s _c	s _g	i _q	i _c	i _g	Q _{lim}	R _d	Sic.
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Relazione geotecnica

	<daN>	<daN>	<daN>	<daNm>	<daNm>	<m>	<m>							<daN/mq>	<daN>	
33	30233.5	-3919.43	-2549.87	-53.92	603.85	0.4	3.31	1.04	1.05	0.96	1	1	1	45195.2	25766.7	0.85
34	29825.2	-3582.15	-2650.45	-54.24	575.86	0.4	3.31	1.04	1.05	0.96	1	1	1	45193.8	25771.7	0.86
35	30051.6	-3588.02	-3198.27	-52.8	466	0.4	3.32	1.04	1.05	0.96	1	1	1	45190.5	25837	0.86
36	30007.2	-3913.56	-2002.05	-55.35	713.72	0.4	3.3	1.04	1.05	0.96	1	1	1	45198.5	25701.2	0.86

Verifiche in condizioni non drenate

$c_{ur}=20000.00$ <daN/mq>
 $N_q=1.00$ $N_c=5.14$ $b_q=0.00$ $b_c=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _c	i _q	i _c	Q _{lim} <daN/mq>	R _d <daN>	Sic.
33	30233.5	-3919.43	-2549.87	-53.92	603.85	0.4	3.31	1.02	0	1	107197	61115	2.02
34	29825.2	-3582.15	-2650.45	-54.24	575.86	0.4	3.31	1.02	0	1	107195	61127.9	2.05
35	30051.6	-3588.02	-3198.27	-52.8	466	0.4	3.32	1.02	0	1	107191	61284.6	2.04
36	30007.2	-3913.56	-2002.05	-55.35	713.72	0.4	3.3	1.02	0	1	107202	60958.1	2.03

Verifiche di capacità portante per rottura generale in condizioni statiche

Metodo utilizzato: Indicazioni EC7

Travata 412

$B=0.40$ <m> $L=35.17$ <m> $D=1.00$ <m> $\beta=0.00$ <grad> $\eta=0.00$ <grad> $\gamma_r=1900.00$ <daN/mc>
 $\sigma_{v0,r}=1900.00$ <daN/mq>

Verifiche in condizioni drenate

$\phi'_r=20.00$ <grad> $c'_r=2000.00$ <daN/mq>
 $N_q=6.40$ $N_c=14.83$ $N_g=3.93$ $b_q=1.00$ $b_c=1.00$ $b_g=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _q	s _c	s _g	i _q	i _c	i _g	Q _{lim} <daN/mq>	R _d <daN>	Sic.
33	206667	-1772.88	-138.21	-30.85	-5131.75	0.4	35.12	1	1	1	1	1	1	43499.8	265494	1.28
34	206915	4084.39	-87.03	-31.02	-509.03	0.4	35.17	1	1	1	1	1	1	43499.6	265830	1.28
35	206759	1107.35	-5081.14	-25.31	-2693.16	0.4	35.14	1	1	1	1	1	1	43499.9	265709	1.29
36	206823	1204.16	4855.9	-36.56	-2947.62	0.4	35.14	1	1	1	1	1	1	43499.5	265615	1.28

Verifiche in condizioni non drenate

$c_{ur}=20000.00$ <daN/mq>
 $N_q=1.00$ $N_c=5.14$ $b_q=0.00$ $b_c=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _c	i _q	i _c	Q _{lim} <daN/mq>	R _d <daN>	Sic.
33	206667	-1772.88	-138.21	-30.85	-5131.75	0.4	35.12	1	0	1	104966	640641	3.1
34	206915	4084.39	-87.03	-31.02	-509.03	0.4	35.17	1	0	1	104966	641454	3.1
35	206759	1107.35	-5081.14	-25.31	-2693.16	0.4	35.14	1	0	1	104966	641158	3.1
36	206823	1204.16	4855.9	-36.56	-2947.62	0.4	35.14	1	0	1	104966	640938	3.1

Verifiche di capacità portante per rottura generale in condizioni statiche

Metodo utilizzato: Indicazioni EC7

Travata 412

$B=0.40$ <m> $L=7.44$ <m> $D=1.00$ <m> $\beta=0.00$ <grad> $\eta=0.00$ <grad> $\gamma_r=1900.00$ <daN/mc>
 $\sigma_{v0,r}=1900.00$ <daN/mq>

Verifiche in condizioni drenate

$\phi'_r=20.00$ <grad> $c'_r=2000.00$ <daN/mq>
 $N_q=6.40$ $N_c=14.83$ $N_g=3.93$ $b_q=1.00$ $b_c=1.00$ $b_g=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _q	s _c	s _g	i _q	i _c	i _g	Q _{lim} <daN/mq>	R _d <daN>	Sic.
33	69128.4	-11978.3	-4745.98	-29.6	31033.9	0.4	6.54	1.02	1.02	0.98	1	1	1	44278.8	50272.7	0.73
34	68690.8	-10581.6	-4840.46	-29.58	31213.5	0.4	6.53	1.02	1.02	0.98	1	1	1	44280.4	50189.8	0.73
35	69036.7	-11105.1	-6273.04	-26.15	30860.2	0.4	6.55	1.02	1.02	0.98	1	1	1	44278.9	50314.7	0.73
36	68782.5	-11454.7	-3313.41	-33.03	31387.2	0.4	6.53	1.02	1.02	0.98	1	1	1	44280.4	50147.8	0.73

Verifiche in condizioni non drenate

$c_{ur}=20000.00$ <daN/mq>
 $N_q=1.00$ $N_c=5.14$ $b_q=0.00$ $b_c=1.00$

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _c	i _q	i _c	Q _{lim} <daN/mq>	R _d <daN>	Sic.
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Relazione geotecnica

33	69128.4	-11978.3	-4745.98	-29.6	31033.9	0.4	6.54	1.01	0	1	105987	120334	1.74
34	68690.8	-10581.6	-4840.46	-29.58	31213.5	0.4	6.53	1.01	0	1	105989	120133	1.75
35	69036.7	-11105.1	-6273.04	-26.15	30860.2	0.4	6.55	1.01	0	1	105986	120434	1.74
36	68782.5	-11454.7	-3313.41	-33.03	31387.2	0.4	6.53	1.01	0	1	105989	120033	1.75

Verifiche di capacità portante per rottura generale in condizioni statiche

Metodo utilizzato: Indicazioni EC7

Travata 413

B=0.40 <m> L=8.96 <m> D=1.00 <m> β =0.00 <grad> η =0.00 <grad> γ_r =1900.00 <daN/mc>
 $\sigma_{v0,r}$ =1900.00 <daN/mq>

Verifiche in condizioni drenate

ϕ'_r =20.00 <grad> c'_r =2000.00 <daN/mq>
 N_q =6.40 N_c =14.83 N_g =3.93 b_q =1.00 b_c =1.00 b_g =1.00

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _q	s _c	s _g	i _q	i _c	i _g	q _{lim} <daN/mq>	R _d <daN>	Sic.
33	62260.4	-3919.43	-2549.87	-57.74	19304.1	0.4	8.34	1.02	1.02	0.99	1	1	1	44066.1	63639.3	1.02
34	61654.8	-3582.15	-2650.45	-59.14	19229.4	0.4	8.34	1.02	1.02	0.99	1	1	1	44066	63601.1	1.03
35	62779.5	-3588.02	-3198.27	-55.03	19856.4	0.4	8.33	1.02	1.02	0.99	1	1	1	44067.8	63562.8	1.01
36	61135.7	-3913.56	-2002.05	-61.84	18677.1	0.4	8.35	1.02	1.02	0.99	1	1	1	44064.3	63679.2	1.04

Verifiche in condizioni non drenate

c_{ur} =20000.00 <daN/mq>
 N_q =1.00 N_c =5.14 b_q =0.00 b_c =1.00

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B' <m>	L' <m>	s _c	i _q	i _c	q _{lim} <daN/mq>	R _d <daN>	Sic.
33	62260.4	-3919.43	-2549.87	-57.74	19304.1	0.4	8.34	1.01	0	1	105713	152669	2.45
34	61654.8	-3582.15	-2650.45	-59.14	19229.4	0.4	8.34	1.01	0	1	105714	152578	2.47
35	62779.5	-3588.02	-3198.27	-55.03	19856.4	0.4	8.33	1.01	0	1	105715	152482	2.43
36	61135.7	-3913.56	-2002.05	-61.84	18677.1	0.4	8.35	1.01	0	1	105712	152769	2.5

Simbologia

B =Base della fondazione
L =Lunghezza della fondazione (L>B)
D =Profondità del piano di posa della fondazione
H =Spessore del terreno responsabile del cedimento
 E_r =Modulo elastico rappresentativo del terreno di fondazione
 ν_r =Coefficiente di Poisson rappresentativo del terreno di fondazione
 I_s =Coefficiente di influenza
 I_r =Coefficiente di profondità
kw =Costante di sottofondo
CC =Numero della combinazione delle condizioni di carico elementari
N =Sforzo normale
 q_{es} =Pressione di esercizio
Ced=Cedimento calcolato

Travata 401

B=0.40 <m> L=42.46 <m> D=1.00 <m> H=2.00 <m> E_r =750000.00 <daN/mq> ν_r =0.40
 I_s =0.79 I_r =3.35 kw=423465.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	117914	6942.66	1.64
2	119379	7028.93	1.66
3	136957	8063.86	1.9
4	135746	7992.58	1.89
5	119498	7035.93	1.66
6	120741	7109.09	1.68
7	138541	8157.13	1.93
8	137107	8072.74	1.91
9	96252.4	5667.24	1.34
10	100761	5932.73	1.4
11	96727.6	5695.22	1.34
12	101170	5956.78	1.41
13	159727	9404.57	2.22
14	155317	9144.89	2.16
15	160202	9432.55	2.23
16	155725	9168.94	2.17
17	118141	6956.01	1.64
18	119574	7040.4	1.66
19	137183	8077.21	1.91

Relazione geotecnica

20	135941	8004.05	1.89
21	119725	7049.27	1.66
22	120936	7120.56	1.68
23	138767	8170.47	1.93
24	137302	8084.21	1.91
25	96479.1	5680.59	1.34
26	100956	5944.2	1.4
27	96954.3	5708.57	1.35
28	101365	5968.24	1.41
29	159954	9417.91	2.22
30	155512	9156.36	2.16
31	160429	9445.89	2.23
32	155920	9180.41	2.17
33	216373	12739.8	3.01
34	216491	12746.8	3.01
35	214075	12604.5	2.98
36	218790	12882.1	3.04
37	156118	9192.04	2.17
38	156235	9198.97	2.17
39	153819	9056.69	2.14
40	158534	9334.32	2.2
41	127901	7530.69	1.78
42	128019	7537.61	1.78
43	125602	7395.33	1.75
44	130318	7672.97	1.81
45	116615	6866.14	1.62
46	116732	6873.07	1.62
47	114316	6730.79	1.59
48	119031	7008.42	1.66

Travata 402
 B=0.40 <m> L=35.61 <m> D=1.00 <m> H=2.00 <m> E_r=750000.00 <daN/mq> v_r=0.40
 I_s=0.79 I_r=2.89 kw=489808.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	117449	8245.53	1.68
2	116448	8175.23	1.67
3	99942.8	7016.48	1.43
4	101401	7118.89	1.45
5	119389	8381.68	1.71
6	118115	8292.25	1.69
7	101882	7152.63	1.46
8	103068	7235.9	1.48
9	138552	9727.08	1.99
10	134586	9448.59	1.93
11	139134	9767.92	1.99
12	135086	9483.7	1.94
13	80197.2	5630.25	1.15
14	84430.5	5927.44	1.21
15	80779	5671.09	1.16
16	84930.5	5962.55	1.22
17	118764	8337.83	1.7
18	117578	8254.56	1.69
19	101257	7108.78	1.45
20	102531	7198.21	1.47
21	120703	8473.98	1.73
22	119245	8371.58	1.71
23	103197	7244.93	1.48
24	104198	7315.23	1.49
25	139867	9819.37	2
26	135716	9527.92	1.95
27	140449	9860.22	2.01
28	136216	9563.02	1.95
29	81511.9	5722.54	1.17
30	85560.4	6006.76	1.23
31	82093.6	5763.38	1.18
32	86060.4	6041.87	1.23
33	184646	12963.1	2.65
34	184790	12973.2	2.65
35	186886	13120.3	2.68
36	182550	12816	2.62
37	133368	9363.09	1.91
38	133512	9373.21	1.91
39	135608	9520.33	1.94
40	131272	9215.97	1.88
41	109692	7700.93	1.57
42	109836	7711.04	1.57
43	111932	7858.16	1.6

Relazione geotecnica

44	107596	7553.81	1.54
45	100222	7036.06	1.44
46	100366	7046.17	1.44
47	102461	7193.29	1.47
48	98126.1	6888.94	1.41

Travata 403
 B=0.40 <m> L=12.19 <m> D=1.00 <m> H=2.00 <m> E_r=750000.00 <daN/mq> v_r=0.40
 I_s=0.79 I_r=1.34 kw=1051260.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	67319.5	13806.3	1.31
2	68826.9	14115.4	1.34
3	67661.9	13876.5	1.32
4	69121.2	14175.8	1.35
5	88556.3	18161.7	1.73
6	87079.5	17858.8	1.7
7	88898.7	18231.9	1.73
8	87373.8	17919.2	1.7
9	74352.9	15248.8	1.45
10	74872	15355.2	1.46
11	80723.9	16555.4	1.57
12	80347.8	16478.2	1.57
13	75494.2	15482.8	1.47
14	75852.9	15556.4	1.48
15	81865.3	16789.4	1.6
16	81328.7	16679.4	1.59
17	67195.2	13780.8	1.31
18	68720.1	14093.5	1.34
19	67537.6	13851	1.32
20	69014.4	14153.9	1.35
21	88432	18136.2	1.73
22	86972.7	17836.9	1.7
23	88774.4	18206.4	1.73
24	87267	17897.3	1.7
25	74228.6	15223.3	1.45
26	74765.2	15333.3	1.46
27	80599.7	16529.9	1.57
28	80241	16456.3	1.57
29	75369.9	15457.3	1.47
30	75746.1	15534.5	1.48
31	81741	16763.9	1.59
32	81221.9	16657.5	1.58
33	129529	26564.5	2.53
34	131106	26888.1	2.56
35	130275	26717.6	2.54
36	130360	26735	2.54
37	93392.7	19153.6	1.82
38	94970.3	19477.1	1.85
39	94139.1	19306.6	1.84
40	94223.9	19324	1.84
41	76800	15750.6	1.5
42	78377.6	16074.2	1.53
43	77546.4	15903.7	1.51
44	77631.2	15921.1	1.51
45	70163	14389.5	1.37
46	71740.6	14713	1.4
47	70909.4	14542.5	1.38
48	70994.2	14559.9	1.39

Travata 404
 B=0.40 <m> L=12.19 <m> D=1.00 <m> H=2.00 <m> E_r=750000.00 <daN/mq> v_r=0.40
 I_s=0.79 I_r=1.34 kw=1051260.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	85237.7	17481.1	1.66
2	85635.3	17562.6	1.67
3	85551	17545.3	1.67
4	85904.5	17617.8	1.68
5	90683.5	18597.9	1.77
6	90315.8	18522.5	1.76
7	90996.8	18662.2	1.78
8	90585	18577.7	1.77
9	86778.3	17797	1.69
10	86959.4	17834.2	1.7
11	88412	18132.1	1.72
12	88363.5	18122.1	1.72

13	87822.5	18011.2	1.71
14	87856.8	18018.2	1.71
15	89456.2	18346.2	1.75
16	89260.9	18306.2	1.74
17	85136.7	17460.4	1.66
18	85548.4	17544.8	1.67
19	85449.9	17524.6	1.67
20	85817.6	17600	1.67
21	90582.5	18577.2	1.77
22	90229	18504.7	1.76
23	90895.7	18641.5	1.77
24	90498.2	18559.9	1.77
25	86677.3	17776.3	1.69
26	86872.5	17816.3	1.69
27	88311	18111.4	1.72
28	88276.7	18104.3	1.72
29	87721.4	17990.4	1.71
30	87769.9	18000.4	1.71
31	89355.1	18325.5	1.74
32	89174.1	18288.4	1.74
33	149736	30708.8	2.92
34	150140	30791.7	2.93
35	149900	30742.3	2.92
36	149977	30758.2	2.93
37	107834	22115.2	2.1
38	108238	22198.1	2.11
39	107997	22148.7	2.11
40	108075	22164.6	2.11
41	87851.4	18017.1	1.71
42	88255.8	18100	1.72
43	88014.8	18050.6	1.72
44	88092.3	18066.5	1.72
45	79858.5	16377.9	1.56
46	80262.9	16460.8	1.57
47	80021.9	16411.4	1.56
48	80099.4	16427.3	1.56

Travata 405
B=0.40 <m> L=12.19 <m> D=1.00 <m> H=2.00 <m> E_t=750000.00 <daN/mq> v_t=0.40
I_s=0.79 I_f=1.34 kw=1051260.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	91765.5	18819.8	1.79
2	91807.2	18828.4	1.79
3	92068.9	18882.1	1.8
4	92067.9	18881.9	1.8
5	92105.8	18889.6	1.8
6	92099.7	18888.4	1.8
7	92409.2	18951.8	1.8
8	92360.4	18941.8	1.8
9	91530.7	18771.7	1.79
10	91605.4	18787	1.79
11	91632.8	18792.6	1.79
12	91693.2	18805	1.79
13	92541.9	18979.1	1.81
14	92474.5	18965.2	1.8
15	92644	19000	1.81
16	92562.2	18983.2	1.81
17	91715.2	18809.5	1.79
18	91764	18819.5	1.79
19	92018.6	18871.7	1.8
20	92024.7	18873	1.8
21	92055.5	18879.3	1.8
22	92056.5	18879.5	1.8
23	92358.9	18941.5	1.8
24	92317.2	18933	1.8
25	91480.4	18761.4	1.78
26	91562.2	18778.1	1.79
27	91582.5	18782.3	1.79
28	91649.9	18796.1	1.79
29	92491.6	18968.7	1.8
30	92431.2	18956.4	1.8
31	92593.7	18989.7	1.81
32	92519	18974.4	1.8
33	157841	32371	3.08
34	157866	32376.2	3.08
35	157816	32365.9	3.08
36	157891	32381.3	3.08

Relazione geotecnica

37	113604	23298.5	2.22
38	113629	23303.7	2.22
39	113579	23293.4	2.22
40	113654	23308.8	2.22
41	92229.8	18915.1	1.8
42	92255.1	18920.2	1.8
43	92205.1	18910	1.8
44	92279.8	18925.3	1.8
45	83680.3	17161.7	1.63
46	83705.5	17166.8	1.63
47	83655.5	17156.6	1.63
48	83730.3	17171.9	1.63

Travata 406
 B=0.40 <m> L=12.19 <m> D=1.00 <m> H=2.00 <m> E_t=750000.00 <daN/mq> v_t=0.40
 I_s=0.79 I_f=1.34 kw=1051260.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	92112.3	18891	1.8
2	92131.5	18894.9	1.8
3	92471.3	18964.6	1.8
4	92440	18958.2	1.8
5	91985.8	18865	1.79
6	92022.8	18872.6	1.8
7	92344.9	18938.7	1.8
8	92331.4	18935.9	1.8
9	91649.2	18796	1.79
10	91733.5	18813.3	1.79
11	91611.3	18788.2	1.79
12	91700.9	18806.6	1.79
13	92845.9	19041.4	1.81
14	92762	19024.2	1.81
15	92807.9	19033.6	1.81
16	92729.4	19017.5	1.81
17	92153	18899.3	1.8
18	92166.5	18902.1	1.8
19	92512	18972.9	1.8
20	92475	18965.3	1.8
21	92026.5	18873.4	1.8
22	92057.8	18879.8	1.8
23	92385.5	18947	1.8
24	92366.3	18943.1	1.8
25	91689.9	18804.3	1.79
26	91768.4	18820.4	1.79
27	91652	18796.5	1.79
28	91735.8	18813.7	1.79
29	92886.6	19049.7	1.81
30	92797	19031.4	1.81
31	92848.6	19042	1.81
32	92764.4	19024.7	1.81
33	158277	32460.4	3.09
34	158267	32458.4	3.09
35	158227	32450.2	3.09
36	158317	32468.6	3.09
37	113911	23361.6	2.22
38	113902	23359.7	2.22
39	113862	23351.5	2.22
40	113951	23369.8	2.22
41	92451.4	18960.5	1.8
42	92441.8	18958.5	1.8
43	92402	18950.4	1.8
44	92491.3	18968.7	1.8
45	83867.4	17200.1	1.64
46	83857.9	17198.1	1.64
47	83818	17189.9	1.64
48	83907.3	17208.2	1.64

Travata 407
 B=0.40 <m> L=12.19 <m> D=1.00 <m> H=2.00 <m> E_t=750000.00 <daN/mq> v_t=0.40
 I_s=0.79 I_f=1.34 kw=1051260.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	88099.5	18068	1.72
2	88099.5	18068	1.72
3	88616.6	18174	1.73
4	88544	18159.1	1.73
5	87350.4	17914.4	1.7

Relazione geotecnica

6	87455.7	17936	1.71
7	87867.6	18020.4	1.71
8	87900.2	18027.1	1.71
9	87234	17890.5	1.7
10	87355.6	17915.4	1.7
11	87009.3	17844.4	1.7
12	87162.5	17875.8	1.7
13	88957.8	18244	1.74
14	88837.2	18219.3	1.73
15	88733.1	18197.9	1.73
16	88644.1	18179.7	1.73
17	88332.2	18115.7	1.72
18	88299.6	18109	1.72
19	88849.3	18221.8	1.73
20	88744	18200.2	1.73
21	87583.1	17962.1	1.71
22	87655.8	17977	1.71
23	88100.3	18068.1	1.72
24	88100.2	18068.1	1.72
25	87466.7	17938.2	1.71
26	87555.7	17956.5	1.71
27	87242	17892.1	1.7
28	87362.5	17916.8	1.7
29	89190.5	18291.7	1.74
30	89037.2	18260.3	1.74
31	88965.8	18245.6	1.74
32	88844.1	18220.7	1.73
33	150780	30922.9	2.94
34	150726	30911.7	2.94
35	150688	30904.1	2.94
36	150817	30930.5	2.94
37	108566	22265.4	2.12
38	108512	22254.3	2.12
39	108475	22246.6	2.12
40	108603	22273.1	2.12
41	88246.1	18098	1.72
42	88191.6	18086.9	1.72
43	88154.4	18079.3	1.72
44	88283.3	18105.7	1.72
45	80118	16431.1	1.56
46	80063.6	16419.9	1.56
47	80026.4	16412.3	1.56
48	80155.2	16438.7	1.56

Travata 408
 B=0.40 <m> L=12.19 <m> D=1.00 <m> H=2.00 <m> E_r=750000.00 <daN/mq> v_r=0.40
 I_s=0.79 I_r=1.34 kw=1051260.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	72460.9	14860.7	1.41
2	72182.1	14803.5	1.41
3	72950.8	14961.2	1.42
4	72603.1	14889.9	1.42
5	67622.8	13868.5	1.32
6	68023.9	13950.7	1.33
7	68112.7	13969	1.33
8	68444.9	14037.1	1.34
9	70196.1	14396.3	1.37
10	70235.5	14404.3	1.37
11	68744.7	14098.6	1.34
12	68988.1	14148.5	1.35
13	71828.9	14731.1	1.4
14	71638.9	14692.1	1.4
15	70377.5	14433.4	1.37
16	70391.4	14436.3	1.37
17	72840.6	14938.6	1.42
18	72508.5	14870.5	1.41
19	73330.5	15039.1	1.43
20	72929.5	14956.8	1.42
21	68002.6	13946.4	1.33
22	68350.2	14017.7	1.33
23	68492.4	14046.8	1.34
24	68771.2	14104	1.34
25	70575.8	14474.1	1.38
26	70561.9	14471.3	1.38
27	69124.4	14176.5	1.35
28	69314.4	14215.4	1.35
29	72208.6	14809	1.41

Relazione geotecnica

30	71965.2	14759.1	1.4
31	70757.2	14511.3	1.38
32	70717.8	14503.2	1.38
33	119500	24507.8	2.33
34	119140	24433.9	2.32
35	119259	24458.3	2.33
36	119382	24483.5	2.33
37	86228.8	17684.3	1.68
38	85868.5	17610.4	1.68
39	85987.2	17634.8	1.68
40	86110.1	17660	1.68
41	70529.6	14464.6	1.38
42	70169.2	14390.7	1.37
43	70288	14415.1	1.37
44	70410.8	14440.3	1.37
45	64249.9	13176.8	1.25
46	63889.5	13102.9	1.25
47	64008.3	13127.2	1.25
48	64131.1	13152.4	1.25

Travata 409

B=0.40 <m> L=3.54 <m> D=1.00 <m> H=2.00 <m> E_r=750000.00 <daN/mq> v_r=0.40
I_s=0.80 I_r=0.77 kw=1808450.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	27084.5	19117.3	1.06
2	26919.4	19000.7	1.05
3	31123	21967.8	1.21
4	30390.4	21450.7	1.19
5	19217.7	13564.6	0.75
6	20158	14228.3	0.79
7	23256.2	16415.1	0.91
8	23629	16678.2	0.92
9	19619.6	13848.2	0.77
10	20503.4	14472.1	0.8
11	17259.5	12182.4	0.67
12	18475	13040.3	0.72
13	33081.1	23349.9	1.29
14	32073.4	22638.6	1.25
15	30721.1	21684.1	1.2
16	30045	21206.9	1.17
17	28562.5	20160.5	1.11
18	28189.7	19897.3	1.1
19	32601	23011	1.27
20	31660.7	22347.3	1.24
21	20695.7	14607.8	0.81
22	21428.3	15124.9	0.84
23	24734.2	17458.3	0.97
24	24899.3	17574.9	0.97
25	21097.6	14891.5	0.82
26	21773.7	15368.7	0.85
27	18737.5	13225.7	0.73
28	19745.3	13937	0.77
29	34559.2	24393.1	1.35
30	33343.7	23535.2	1.3
31	32199.1	22727.3	1.26
32	31315.3	22103.5	1.22
33	43402.9	30635.4	1.69
34	42820.4	30224.2	1.67
35	42612.5	30077.5	1.66
36	43610.8	30782.1	1.7
37	31465.3	22209.4	1.23
38	30882.7	21798.2	1.21
39	30674.9	21651.5	1.2
40	31673.2	22356.1	1.24
41	26022.4	18367.6	1.02
42	25439.8	17956.4	0.99
43	25231.9	17809.7	0.98
44	26230.3	18514.3	1.02
45	23845.2	16830.9	0.93
46	23262.7	16419.6	0.91
47	23054.8	16272.9	0.9
48	24053.1	16977.6	0.94

Travata 411

B=0.40 <m> L=3.35 <m> D=1.00 <m> H=2.00 <m> E_r=750000.00 <daN/mq> v_r=0.40
I_s=0.80 I_r=0.75 kw=1840740.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	21122.9	15774.5	0.86
2	20703.1	15461	0.84
3	20957.4	15650.9	0.85
4	20560.9	15354.8	0.83
5	15613.6	11660.2	0.63
6	15968	11924.9	0.65
7	15448.1	11536.6	0.63
8	15825.8	11818.7	0.64
9	19387.7	14478.7	0.79
10	19211.8	14347.3	0.78
11	17734.9	13244.4	0.72
12	17791.2	13286.5	0.72
13	18836.1	14066.7	0.76
14	18737.6	13993.2	0.76
15	17183.3	12832.4	0.7
16	17317.1	12932.4	0.7
17	20823.2	15550.7	0.84
18	20445.6	15268.7	0.83
19	20657.7	15427.1	0.84
20	20303.3	15162.5	0.82
21	15314	11436.4	0.62
22	15710.5	11732.5	0.64
23	15148.5	11312.8	0.61
24	15568.2	11626.3	0.63
25	19088.1	14254.9	0.77
26	18954.2	14155	0.77
27	17435.3	13020.6	0.71
28	17533.7	13094.1	0.71
29	18536.4	13842.9	0.75
30	18480.1	13800.9	0.75
31	16883.6	12608.7	0.68
32	17059.6	12740	0.69
33	30233.5	22578.3	1.23
34	29825.2	22273.4	1.21
35	30051.6	22442.4	1.22
36	30007.2	22409.3	1.22
37	21935.1	16381.1	0.89
38	21526.8	16076.1	0.87
39	21753.1	16245.2	0.88
40	21708.7	16212	0.88
41	18189.4	13583.8	0.74
42	17781.1	13278.9	0.72
43	18007.4	13447.9	0.73
44	17963.1	13414.8	0.73
45	16691.1	12464.9	0.68
46	16282.8	12160	0.66
47	16509.2	12329	0.67
48	16464.8	12295.9	0.67

Travata 412
B=0.40 <m> L=35.17 <m> D=1.00 <m> H=2.00 <m> E_x=750000.00 <daN/mq> v_x=0.40
I_s=0.79 I_r=2.86 kw=494787.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	118304	8409.41	1.7
2	118560	8427.64	1.7
3	118565	8427.97	1.7
4	118784	8443.59	1.71
5	121634	8646.16	1.75
6	121423	8631.12	1.74
7	121895	8664.72	1.75
8	121647	8647.07	1.75
9	119165	8470.62	1.71
10	119300	8480.25	1.71
11	120164	8541.64	1.73
12	120159	8541.29	1.73
13	120035	8532.48	1.72
14	120048	8533.42	1.72
15	121034	8603.51	1.74
16	120907	8594.46	1.74
17	118363	8413.61	1.7
18	118611	8431.25	1.7
19	118624	8432.17	1.7
20	118835	8447.2	1.71
21	121693	8650.36	1.75
22	121473	8634.73	1.75

Relazione geotecnica

23	121954	8668.92	1.75
24	121698	8650.68	1.75
25	119224	8474.82	1.71
26	119351	8483.86	1.71
27	120223	8545.84	1.73
28	120210	8544.91	1.73
29	120094	8536.68	1.73
30	120099	8537.03	1.73
31	121093	8607.71	1.74
32	120958	8598.08	1.74
33	206667	14690.6	2.97
34	206915	14708.2	2.97
35	206759	14697.1	2.97
36	206823	14701.7	2.97
37	148626	10564.9	2.14
38	148874	10582.4	2.14
39	148718	10571.3	2.14
40	148782	10575.9	2.14
41	120382	8557.16	1.73
42	120630	8574.75	1.73
43	120473	8563.65	1.73
44	120538	8568.25	1.73
45	109084	7754.08	1.57
46	109332	7771.67	1.57
47	109176	7760.58	1.57
48	109240	7765.18	1.57

Travata 412

B=0.40 <m> L=7.44 <m> D=1.00 <m> H=2.00 <m> E_r=750000.00 <daN/mq> v_r=0.40
I_s=0.80 I_r=1.03 k_w=1363970.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	44600.7	14986.3	1.1
2	44076.5	14810.2	1.09
3	43573.9	14641.3	1.07
4	43194	14513.7	1.06
5	38706.2	13005.7	0.95
6	39010.3	13107.9	0.96
7	37679.4	12660.7	0.93
8	38127.8	12811.4	0.94
9	43735.6	14695.6	1.08
10	43332.9	14560.4	1.07
11	41967.2	14101.5	1.03
12	41813.1	14049.7	1.03
13	40312.9	13545.6	0.99
14	40391.2	13571.9	1
15	38544.5	12951.4	0.95
16	38871.4	13061.2	0.96
17	44061.5	14805.1	1.09
18	43613.1	14654.5	1.07
19	43034.7	14460.1	1.06
20	42730.5	14357.9	1.05
21	38167	12824.5	0.94
22	38546.9	12952.2	0.95
23	37140.2	12479.5	0.91
24	37664.4	12655.6	0.93
25	43196.3	14514.5	1.06
26	42869.5	14404.6	1.06
27	41428	13920.3	1.02
28	41349.6	13893.9	1.02
29	39773.7	13364.4	0.98
30	39927.8	13416.2	0.98
31	38005.3	12770.2	0.94
32	38407.9	12905.5	0.95
33	69128.4	23227.9	1.7
34	68690.8	23080.9	1.69
35	69036.7	23197.1	1.7
36	68782.5	23111.7	1.69
37	49945.2	16782.2	1.23
38	49507.6	16635.1	1.22
39	49853.5	16751.3	1.23
40	49599.3	16665.9	1.22
41	40965.6	13764.9	1.01
42	40528	13617.8	1
43	40873.9	13734.1	1.01
44	40619.7	13648.7	1
45	37373.8	12558	0.92
46	36936.1	12410.9	0.91

Relazione geotecnica

47	37282	12527.2	0.92
48	37027.8	12441.8	0.91

Travata 413

B=0.40 <m> L=8.96 <m> D=1.00 <m> H=2.00 <m> E_r=750000.00 <daN/mq> v_r=0.40

I_s=0.80 I_r=1.13 kw=1245730.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	46384.4	12938	1.04
2	45169.5	12599.1	1.01
3	39743.5	11085.7	0.89
4	39461.8	11007.1	0.88
5	38234.2	10664.7	0.86
6	38164.6	10645.3	0.85
7	31593.4	8812.35	0.71
8	32456.9	9053.21	0.73
9	51279.5	14303.4	1.15
10	49376.7	13772.7	1.11
11	48834.4	13621.4	1.09
12	47275.3	13186.5	1.06
13	29143.3	8128.95	0.65
14	30351.1	8465.84	0.68
15	26698.3	7446.96	0.6
16	28249.7	7879.68	0.63
17	43884	12240.6	0.98
18	43020.5	11999.7	0.96
19	37243.2	10388.2	0.83
20	37312.8	10407.7	0.84
21	35733.9	9967.25	0.8
22	36015.6	10045.8	0.81
23	29093	8114.92	0.65
24	30307.9	8453.79	0.68
25	48779.1	13606	1.09
26	47227.7	13173.2	1.06
27	46334.1	12924	1.04
28	45126.2	12587.1	1.01
29	26643	7431.53	0.6
30	28202.1	7866.42	0.63
31	24197.9	6749.53	0.54
32	26100.7	7280.26	0.58
33	62260.4	17366.3	1.39
34	61654.8	17197.4	1.38
35	62779.5	17511.1	1.41
36	61135.7	17052.6	1.37
37	45199	12607.4	1.01
38	44593.4	12438.4	1
39	45718.1	12752.2	1.02
40	44074.3	12293.6	0.99
41	37635.9	10497.8	0.84
42	37030.3	10328.9	0.83
43	38155	10642.6	0.85
44	36511.2	10184.1	0.82
45	34610.7	9653.96	0.77
46	34005.1	9485.05	0.76
47	35129.8	9798.76	0.79
48	33486	9340.25	0.75

Fondazioni profonde

Simbologia

D_p = Diametro pali
 L_p = Lunghezza pali
 W_p = Peso del palo
 D = Profondità della testa del palo
 Q_{S_{lim}} = Resistenza laterale di progetto per compressione
 q_p = Pressione limite alla base del palo
 Q_{P_{lim}} = Resistenza di progetto alla base del palo
 k_p = Risposta elastica alla base del palo
 Palo = Numero del palo
 X_p = Coordinata X del palo
 Y_p = Coordinata Y del palo
 Z_p = Profondità del tratto di integrazione
 τ_s = Attrito laterale limite per compressione
 k_s = Risposta elastica laterale per compressione
 σ_h = Pressione limite per carichi orizzontali
 k_h = Risposta elastica per carichi orizzontali

Relazione geotecnica

Caso =Caso di verifica
 CC =Numero della combinazione delle condizioni di carico elementari
 N =Sforzo normale
 Ced =Cedimento calcolato
 Sic.V=Sicurezza a rottura verticale
 T =Taglio in testa
 M =Momento flettente
 Sps =Spostamento
 Sic.O=Sicurezza a rottura orizzontale

Verifiche capacità portante e cedimenti

Plinto n. 9

Tipo palo=Trivellato
 Rotazione testa libera
 Coefficiente di efficienza=1.00
 Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>
 Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	0	1.2
2	0	-1.2

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{lim}=252333.00 <daN>
 q_p=28.63 <daN/cm²>
 QP_{lim}=143893.00 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>
 q_p=16.60 <daN/cm²>
 QP_{lim}=83431.40 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-11259.9	0.16	17.03	2377.96	2139.49	0.11	>1
2	1	1	-9530.06	0.13	20.12	2377.96	2139.49	0.11	>1
1	3	2	-11135.8	0.15	--	1882.31	1659.2	0.09	--
2	3	2	-9654.24	0.13	--	1882.31	1659.2	0.09	--
1	5	3	-8442.62	0.12	22.71	3141.24	2092.47	0.14	>1
2	5	3	-12347.4	0.17	15.53	3141.24	2092.47	0.14	>1
1	7	4	-8714.33	0.12	--	2586.11	1618.78	0.11	--
2	7	4	-12075.7	0.17	--	2586.11	1618.78	0.11	--
1	9	5	-11218	0.15	17.09	4775.44	4672.2	0.22	>1
2	9	5	-9572.01	0.13	20.03	4775.44	4672.2	0.22	>1
1	11	6	-11099.7	0.15	--	4279.71	4195.33	0.2	--
2	11	6	-9690.29	0.13	--	4279.71	4195.33	0.2	--
1	13	7	-8400.68	0.12	22.83	5291.35	4719.22	0.24	>1
2	13	7	-12389.3	0.17	15.48	5291.35	4719.22	0.24	>1
1	15	8	-8678.28	0.12	--	4710.13	4235.74	0.21	--
2	15	8	-12111.7	0.17	--	4710.13	4235.74	0.21	--
1	17	9	-14532.1	0.2	13.2	4968.17	189.74	0.18	>1
2	17	9	-6257.88	0.09	30.64	4968.17	189.74	0.18	>1
1	19	10	-13948.1	0.19	--	4277.53	342.74	0.16	--
2	19	10	-6841.86	0.09	--	4277.53	342.74	0.16	--
1	21	11	-14519.5	0.2	13.21	5429.96	2233.25	0.22	>1
2	21	11	-6270.46	0.09	30.58	5429.96	2233.25	0.22	>1

Relazione geotecnica

1	23	12	-13937.3	0.19	--	4740.83	2099.09	0.19	--
2	23	12	-6852.67	0.09	--	4740.83	2099.09	0.19	--
1	25	13	-5141.08	0.07	37.3	6314.22	346.48	0.23	>1
2	25	13	-15648.9	0.22	12.25	6314.22	346.48	0.23	>1
1	27	14	-5876.71	0.08	--	5442.93	477.45	0.2	--
2	27	14	-14913.3	0.21	--	5442.93	477.45	0.2	--
1	29	15	-5128.49	0.07	37.39	6756.63	2389.98	0.27	>1
2	29	15	-15661.5	0.22	12.24	6756.63	2389.98	0.27	>1
1	31	16	-5865.9	0.08	--	5876.08	2233.8	0.24	--
2	31	16	-14924.1	0.21	--	5876.08	2233.8	0.24	--
1	33	17	-12351.8	0.17	15.53	3191.99	2162.16	0.14	>1
2	33	17	-8438.2	0.12	22.73	3191.99	2162.16	0.14	>1
1	35	18	-12074.2	0.17	--	2622.66	1678.68	0.11	--
2	35	18	-8715.8	0.12	--	2622.66	1678.68	0.11	--
1	37	19	-9534.49	0.13	20.11	2353.75	2115.14	0.11	>1
2	37	19	-11255.5	0.16	17.04	2353.75	2115.14	0.11	>1
1	39	20	-9652.77	0.13	--	1864.73	1638.27	0.08	--
2	39	20	-11137.2	0.15	--	1864.73	1638.27	0.08	--
1	41	21	-12309.9	0.17	15.58	5186.34	4649.53	0.24	>1
2	41	21	-8480.15	0.12	22.61	5186.34	4649.53	0.24	>1
1	43	22	-12038.1	0.17	--	4617.96	4175.84	0.21	--
2	43	22	-8751.86	0.12	--	4617.96	4175.84	0.21	--
1	45	23	-9492.54	0.13	20.2	4819.79	4696.55	0.22	>1
2	45	23	-11297.5	0.16	16.97	4819.79	4696.55	0.22	>1
1	47	24	-9616.72	0.13	--	4318.46	4216.25	0.2	--
2	47	24	-11173.3	0.15	--	4318.46	4216.25	0.2	--
1	49	25	-15624	0.22	12.27	6277.01	167.07	0.23	>1
2	49	25	-5166.01	0.07	37.12	6277.01	167.07	0.23	>1
1	51	26	-14886.6	0.21	--	5399.58	323.25	0.2	--
2	51	26	-5903.42	0.08	--	5399.58	323.25	0.2	--
1	53	27	-15611.4	0.22	12.28	6638.55	2210.58	0.27	>1
2	53	27	-5178.6	0.07	37.03	6638.55	2210.58	0.27	>1
1	55	28	-14875.8	0.21	--	5765.07	2079.61	0.23	--
2	55	28	-5914.24	0.08	--	5765.07	2079.61	0.23	--
1	57	29	-6232.94	0.09	30.77	5004.96	323.81	0.19	>1
2	57	29	-14557.1	0.2	13.17	5004.96	323.81	0.19	>1
1	59	30	-6815.15	0.09	--	4320.17	457.96	0.16	--
2	59	30	-13974.9	0.19	--	4320.17	457.96	0.16	--
1	61	31	-6220.35	0.09	30.83	5540.76	2367.31	0.23	>1
2	61	31	-14569.6	0.2	13.16	5540.76	2367.31	0.23	>1
1	63	32	-6804.33	0.09	--	4844.48	2214.32	0.2	--
2	63	32	-13985.7	0.19	--	4844.48	2214.32	0.2	--
1	65	33	-9427.89	0.13	20.34	2148.73	2148.57	0.1	>1
2	65	33	-9472.11	0.13	20.25	2148.73	2148.57	0.1	>1
1	67	34	-9424.77	0.13	20.35	2654.75	2654.58	0.12	>1
2	67	34	-9475.23	0.13	20.24	2654.75	2654.58	0.12	>1
1	69	35	-9775.14	0.13	19.62	2427.31	2395.75	0.11	>1
2	69	35	-9124.86	0.13	21.02	2427.31	2395.75	0.11	>1
1	71	36	-9077.52	0.13	21.13	2448.54	2407.39	0.11	>1
2	71	36	-9822.48	0.14	19.52	2448.54	2407.39	0.11	>1
1	73	37	-9433.59	0.13	--	1452.7	1452.57	0.07	--
2	73	37	-9466.41	0.13	--	1452.7	1452.57	0.07	--
1	75	38	-9430.47	0.13	--	1958.72	1958.58	0.09	--
2	75	38	-9469.53	0.13	--	1958.72	1958.58	0.09	--
1	77	39	-9780.84	0.13	--	1745.5	1699.75	0.08	--
2	77	39	-9119.16	0.13	--	1745.5	1699.75	0.08	--
1	79	40	-9083.22	0.13	--	1767.09	1711.4	0.08	--
2	79	40	-9816.78	0.14	--	1767.09	1711.4	0.08	--
1	81	41	-9434.24	0.13	--	1064.68	1064.51	0.05	--
2	81	41	-9465.76	0.13	--	1064.68	1064.51	0.05	--
1	83	42	-9431.13	0.13	--	1570.69	1570.53	0.07	--
2	83	42	-9468.88	0.13	--	1570.69	1570.53	0.07	--
1	85	43	-9781.5	0.13	--	1370.69	1311.7	0.06	--
2	85	43	-9118.51	0.13	--	1370.69	1311.7	0.06	--
1	87	44	-9083.87	0.13	--	1394.37	1323.34	0.06	--
2	87	44	-9816.13	0.14	--	1394.37	1323.34	0.06	--
1	89	45	-9434.5	0.13	--	909.48	909.29	0.04	--
2	89	45	-9465.5	0.13	--	909.48	909.29	0.04	--
1	91	46	-9431.39	0.13	--	1415.48	1415.31	0.07	--
2	91	46	-9468.62	0.13	--	1415.48	1415.31	0.07	--
1	93	47	-9781.76	0.13	--	1223.08	1156.48	0.06	--
2	93	47	-9118.25	0.13	--	1223.08	1156.48	0.06	--
1	95	48	-9084.13	0.13	--	1247.9	1168.12	0.06	--
2	95	48	-9815.87	0.14	--	1247.9	1168.12	0.06	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N	Ced	Sic.V	T	M	Sps	Sic.O
------	------	----	---	-----	-------	---	---	-----	-------

			<daN>	<cm>		<daN>	<daNm>	<cm>	
1	2	1	-11259.9	0.16	17.84	2377.96	2139.49	0.11	>1
2	2	1	-9530.06	0.13	21.08	2377.96	2139.49	0.11	>1
1	4	2	-11135.8	0.15	--	1882.31	1659.2	0.09	--
2	4	2	-9654.24	0.13	--	1882.31	1659.2	0.09	--
1	6	3	-8442.62	0.12	23.8	3141.24	2092.47	0.14	>1
2	6	3	-12347.4	0.17	16.27	3141.24	2092.47	0.14	>1
1	8	4	-8714.33	0.12	--	2586.11	1618.78	0.11	--
2	8	4	-12075.7	0.17	--	2586.11	1618.78	0.11	--
1	10	5	-11218	0.15	17.91	4775.44	4672.2	0.22	>1
2	10	5	-9572.01	0.13	20.99	4775.44	4672.2	0.22	>1
1	12	6	-11099.7	0.15	--	4279.71	4195.33	0.2	--
2	12	6	-9690.29	0.13	--	4279.71	4195.33	0.2	--
1	14	7	-8400.68	0.12	23.92	5291.35	4719.22	0.24	>1
2	14	7	-12389.3	0.17	16.22	5291.35	4719.22	0.24	>1
1	16	8	-8678.28	0.12	--	4710.13	4235.74	0.21	--
2	16	8	-12111.7	0.17	--	4710.13	4235.74	0.21	--
1	18	9	-14532.1	0.2	13.82	4968.17	189.74	0.18	>1
2	18	9	-6257.88	0.09	32.1	4968.17	189.74	0.18	>1
1	20	10	-13948.1	0.19	--	4277.53	342.74	0.16	--
2	20	10	-6841.86	0.09	--	4277.53	342.74	0.16	--
1	22	11	-14519.5	0.2	13.84	5429.96	2233.25	0.22	>1
2	22	11	-6270.46	0.09	32.04	5429.96	2233.25	0.22	>1
1	24	12	-13937.3	0.19	--	4740.83	2099.09	0.19	--
2	24	12	-6852.67	0.09	--	4740.83	2099.09	0.19	--
1	26	13	-5141.08	0.07	39.08	6314.22	346.48	0.23	>1
2	26	13	-15648.9	0.22	12.84	6314.22	346.48	0.23	>1
1	28	14	-5876.71	0.08	--	5442.93	477.45	0.2	--
2	28	14	-14913.3	0.21	--	5442.93	477.45	0.2	--
1	30	15	-5128.49	0.07	39.17	6756.63	2389.98	0.27	>1
2	30	15	-15661.5	0.22	12.83	6756.63	2389.98	0.27	>1
1	32	16	-5865.9	0.08	--	5876.08	2233.8	0.24	--
2	32	16	-14924.1	0.21	--	5876.08	2233.8	0.24	--
1	34	17	-12351.8	0.17	16.27	3191.99	2162.16	0.14	>1
2	34	17	-8438.2	0.12	23.81	3191.99	2162.16	0.14	>1
1	36	18	-12074.2	0.17	--	2622.66	1678.68	0.11	--
2	36	18	-8715.8	0.12	--	2622.66	1678.68	0.11	--
1	38	19	-9534.49	0.13	21.07	2353.75	2115.14	0.11	>1
2	38	19	-11255.5	0.16	17.85	2353.75	2115.14	0.11	>1
1	40	20	-9652.77	0.13	--	1864.73	1638.27	0.08	--
2	40	20	-11137.2	0.15	--	1864.73	1638.27	0.08	--
1	42	21	-12309.9	0.17	16.32	5186.34	4649.53	0.24	>1
2	42	21	-8480.15	0.12	23.69	5186.34	4649.53	0.24	>1
1	44	22	-12038.1	0.17	--	4617.96	4175.84	0.21	--
2	44	22	-8751.86	0.12	--	4617.96	4175.84	0.21	--
1	46	23	-9492.54	0.13	21.16	4819.79	4696.55	0.22	>1
2	46	23	-11297.5	0.16	17.78	4819.79	4696.55	0.22	>1
1	48	24	-9616.72	0.13	--	4318.46	4216.25	0.2	--
2	48	24	-11173.3	0.15	--	4318.46	4216.25	0.2	--
1	50	25	-15624	0.22	12.86	6277.01	167.07	0.23	>1
2	50	25	-5166.01	0.07	38.89	6277.01	167.07	0.23	>1
1	52	26	-14886.6	0.21	--	5399.58	323.25	0.2	--
2	52	26	-5903.42	0.08	--	5399.58	323.25	0.2	--
1	54	27	-15611.4	0.22	12.87	6638.55	2210.58	0.27	>1
2	54	27	-5178.6	0.07	38.79	6638.55	2210.58	0.27	>1
1	56	28	-14875.8	0.21	--	5765.07	2079.61	0.23	--
2	56	28	-5914.24	0.08	--	5765.07	2079.61	0.23	--
1	58	29	-6232.94	0.09	32.23	5004.96	323.81	0.19	>1
2	58	29	-14557.1	0.2	13.8	5004.96	323.81	0.19	>1
1	60	30	-6815.15	0.09	--	4320.17	457.96	0.16	--
2	60	30	-13974.9	0.19	--	4320.17	457.96	0.16	--
1	62	31	-6220.35	0.09	32.3	5540.76	2367.31	0.23	>1
2	62	31	-14569.6	0.2	13.79	5540.76	2367.31	0.23	>1
1	64	32	-6804.33	0.09	--	4844.48	2214.32	0.2	--
2	64	32	-13985.7	0.19	--	4844.48	2214.32	0.2	--
1	66	33	-9427.89	0.13	21.31	2148.73	2148.57	0.1	>1
2	66	33	-9472.11	0.13	21.21	2148.73	2148.57	0.1	>1
1	68	34	-9424.77	0.13	21.32	2654.75	2654.58	0.12	>1
2	68	34	-9475.23	0.13	21.2	2654.75	2654.58	0.12	>1
1	70	35	-9775.14	0.13	20.55	2427.31	2395.75	0.11	>1
2	70	35	-9124.86	0.13	22.02	2427.31	2395.75	0.11	>1
1	72	36	-9077.52	0.13	22.13	2448.54	2407.39	0.11	>1
2	72	36	-9822.48	0.14	20.45	2448.54	2407.39	0.11	>1
1	74	37	-9433.59	0.13	--	1452.7	1452.57	0.07	--
2	74	37	-9466.41	0.13	--	1452.7	1452.57	0.07	--
1	76	38	-9430.47	0.13	--	1958.72	1958.58	0.09	--
2	76	38	-9469.53	0.13	--	1958.72	1958.58	0.09	--
1	78	39	-9780.84	0.13	--	1745.5	1699.75	0.08	--
2	78	39	-9119.16	0.13	--	1745.5	1699.75	0.08	--

Relazione geotecnica

1	80	40	-9083.22	0.13	--	1767.09	1711.4	0.08	--
2	80	40	-9816.78	0.14	--	1767.09	1711.4	0.08	--
1	82	41	-9434.24	0.13	--	1064.68	1064.51	0.05	--
2	82	41	-9465.76	0.13	--	1064.68	1064.51	0.05	--
1	84	42	-9431.13	0.13	--	1570.69	1570.53	0.07	--
2	84	42	-9468.88	0.13	--	1570.69	1570.53	0.07	--
1	86	43	-9781.5	0.13	--	1370.69	1311.7	0.06	--
2	86	43	-9118.51	0.13	--	1370.69	1311.7	0.06	--
1	88	44	-9083.87	0.13	--	1394.37	1323.34	0.06	--
2	88	44	-9816.13	0.14	--	1394.37	1323.34	0.06	--
1	90	45	-9434.5	0.13	--	909.48	909.29	0.04	--
2	90	45	-9465.5	0.13	--	909.48	909.29	0.04	--
1	92	46	-9431.39	0.13	--	1415.48	1415.31	0.07	--
2	92	46	-9468.62	0.13	--	1415.48	1415.31	0.07	--
1	94	47	-9781.76	0.13	--	1223.08	1156.48	0.06	--
2	94	47	-9118.25	0.13	--	1223.08	1156.48	0.06	--
1	96	48	-9084.13	0.13	--	1247.9	1168.12	0.06	--
2	96	48	-9815.87	0.14	--	1247.9	1168.12	0.06	--

Plinto n. 10

Tipo palo=Trivellato

Rotazione testa libera

Coefficiente di efficienza=1.00

Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>

Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	0	1.2
2	0	-1.2

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{lim}=252333.00 <daN>

q_p=28.63 <daN/cm²>

QP_{lim}=143893.00 <daN>

k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>

q_p=16.60 <daN/cm²>

QP_{lim}=83431.40 <daN>

k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-11465	0.16	16.73	3464.13	3217.39	0.16	>1
2	1	1	-9325.02	0.13	20.57	3464.13	3217.39	0.16	>1
1	3	2	-11292.8	0.16	--	2872.18	2662.46	0.13	--
2	3	2	-9497.18	0.13	--	2872.18	2662.46	0.13	--
1	5	3	-8588.91	0.12	22.33	3836.56	3165.75	0.17	>1
2	5	3	-12201.1	0.17	15.72	3836.56	3165.75	0.17	>1
1	7	4	-8820.89	0.12	--	3228.38	2618.08	0.14	--
2	7	4	-11969.1	0.17	--	3228.38	2618.08	0.14	--
1	9	5	-11392.8	0.16	16.83	4803.47	4651.86	0.22	>1
2	9	5	-9397.25	0.13	20.41	4803.47	4651.86	0.22	>1
1	11	6	-11230.7	0.15	--	4221.86	4101.02	0.2	--
2	11	6	-9559.26	0.13	--	4221.86	4101.02	0.2	--
1	13	7	-8516.67	0.12	22.52	5215.69	4703.5	0.24	>1
2	13	7	-12273.3	0.17	15.62	5215.69	4703.5	0.24	>1
1	15	8	-8758.8	0.12	--	4586.87	4145.4	0.21	--
2	15	8	-12031.2	0.17	--	4586.87	4145.4	0.21	--
1	17	9	-14795.1	0.2	12.96	5306.02	523.4	0.2	>1

Relazione geotecnica

2	17	9	-5994.88	0.08	31.99	5306.02	523.4	0.2	>1
1	19	10	-14155	0.2	--	4525.34	347.02	0.17	--
2	19	10	-6634.99	0.09	--	4525.34	347.02	0.17	--
1	21	11	-14773.5	0.2	12.98	5566.14	1837.38	0.22	>1
2	21	11	-6016.55	0.08	31.87	5566.14	1837.38	0.22	>1
1	23	12	-14136.4	0.19	--	4794.4	1682.02	0.19	--
2	23	12	-6653.61	0.09	--	4794.4	1682.02	0.19	--
1	25	13	-5208.2	0.07	36.82	6234.06	351.27	0.23	>1
2	25	13	-15581.8	0.21	12.31	6234.06	351.27	0.23	>1
1	27	14	-5915.24	0.08	--	5379.4	199.08	0.2	--
2	27	14	-14874.8	0.21	--	5379.4	199.08	0.2	--
1	29	15	-5186.54	0.07	36.97	6565.26	2009.5	0.26	>1
2	29	15	-15603.5	0.22	12.29	6565.26	2009.5	0.26	>1
1	31	16	-5896.61	0.08	--	5699.82	1829.96	0.23	--
2	31	16	-14893.4	0.21	--	5699.82	1829.96	0.23	--
1	33	17	-11962.9	0.16	16.03	3746.61	3239.93	0.17	>1
2	33	17	-8827.1	0.12	21.73	3746.61	3239.93	0.17	>1
1	35	18	-11720.8	0.16	--	3118.21	2681.83	0.14	--
2	35	18	-9069.23	0.13	--	3118.21	2681.83	0.14	--
1	37	19	-9086.83	0.13	21.1	3553.8	3188.29	0.16	>1
2	37	19	-11703.2	0.16	16.39	3553.8	3188.29	0.16	>1
1	39	20	-9248.84	0.13	--	2974.53	2637.44	0.14	--
2	39	20	-11541.2	0.16	--	2974.53	2637.44	0.14	--
1	41	21	-11890.7	0.16	16.13	4965.07	4629.32	0.23	>1
2	41	21	-8899.33	0.12	21.55	4965.07	4629.32	0.23	>1
1	43	22	-11658.7	0.16	--	4354.24	4081.65	0.2	--
2	43	22	-9131.31	0.13	--	4354.24	4081.65	0.2	--
1	45	23	-9014.59	0.12	21.27	4965.42	4680.96	0.23	>1
2	45	23	-11775.4	0.16	16.29	4965.42	4680.96	0.23	>1
1	47	24	-9186.75	0.13	--	4373.37	4126.03	0.2	--
2	47	24	-11603.2	0.16	--	4373.37	4126.03	0.2	--
1	49	25	-15293	0.21	12.54	5902.95	545.93	0.22	>1
2	49	25	-5496.96	0.08	34.89	5902.95	545.93	0.22	>1
1	51	26	-14583	0.2	--	5038.89	366.39	0.19	--
2	51	26	-6207.04	0.09	--	5038.89	366.39	0.19	--
1	53	27	-15271.4	0.21	12.56	6126.61	1814.84	0.24	>1
2	53	27	-5518.63	0.08	34.75	6126.61	1814.84	0.24	>1
1	55	28	-14564.3	0.2	--	5272.24	1662.65	0.21	--
2	55	28	-6225.66	0.09	--	5272.24	1662.65	0.21	--
1	57	29	-5706.12	0.08	33.61	5639.06	373.81	0.21	>1
2	57	29	-15083.9	0.21	12.71	5639.06	373.81	0.21	>1
1	59	30	-6343.19	0.09	--	4867.08	218.45	0.18	--
2	59	30	-14446.8	0.2	--	4867.08	218.45	0.18	--
1	61	31	-5684.45	0.08	33.74	5991.71	1986.97	0.24	>1
2	61	31	-15105.6	0.21	12.7	5991.71	1986.97	0.24	>1
1	63	32	-6324.56	0.09	--	5209.31	1810.59	0.21	--
2	63	32	-14465.4	0.2	--	5209.31	1810.59	0.21	--
1	65	33	-9186.03	0.13	20.88	1039.05	989.59	0.05	>1
2	65	33	-9713.97	0.13	19.74	1039.05	989.59	0.05	>1
1	67	34	-9180.66	0.13	20.89	1607.01	1574.17	0.07	>1
2	67	34	-9719.34	0.13	19.73	1607.01	1574.17	0.07	>1
1	69	35	-9539.43	0.13	20.1	1279.99	1275.49	0.06	>1
2	69	35	-9360.57	0.13	20.49	1279.99	1275.49	0.06	>1
1	71	36	-8827.26	0.12	21.72	1489.33	1288.27	0.07	>1
2	71	36	-10072.7	0.14	19.04	1489.33	1288.27	0.07	>1
1	73	37	-9260.81	0.13	--	667.19	627.38	0.03	--
2	73	37	-9639.19	0.13	--	667.19	627.38	0.03	--
1	75	38	-9255.45	0.13	--	1234.23	1211.95	0.06	--
2	75	38	-9644.55	0.13	--	1234.23	1211.95	0.06	--
1	77	39	-9614.22	0.13	--	934.29	913.27	0.04	--
2	77	39	-9285.78	0.13	--	934.29	913.27	0.04	--
1	79	40	-8902.04	0.12	--	1135.76	926.06	0.05	--
2	79	40	-9997.96	0.14	--	1135.76	926.06	0.05	--
1	81	41	-9297.08	0.13	--	481.96	445.66	0.02	--
2	81	41	-9602.93	0.13	--	481.96	445.66	0.02	--
1	83	42	-9291.71	0.13	--	1047.6	1030.23	0.05	--
2	83	42	-9608.29	0.13	--	1047.6	1030.23	0.05	--
1	85	43	-9650.48	0.13	--	770.1	731.55	0.04	--
2	85	43	-9249.52	0.13	--	770.1	731.55	0.04	--
1	87	44	-8938.31	0.12	--	964.92	744.34	0.04	--
2	87	44	-9961.7	0.14	--	964.92	744.34	0.04	--
1	89	45	-9311.58	0.13	--	408.29	372.97	0.02	--
2	89	45	-9588.42	0.13	--	408.29	372.97	0.02	--
1	91	46	-9306.21	0.13	--	972.97	957.55	0.05	--
2	91	46	-9593.79	0.13	--	972.97	957.55	0.05	--
1	93	47	-9664.98	0.13	--	707.57	658.87	0.03	--
2	93	47	-9235.02	0.13	--	707.57	658.87	0.03	--
1	95	48	-8952.81	0.12	--	898.38	671.65	0.04	--
2	95	48	-9947.19	0.14	--	898.38	671.65	0.04	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-11465	0.16	17.52	3464.13	3217.39	0.16	>1
2	2	1	-9325.02	0.13	21.54	3464.13	3217.39	0.16	>1
1	4	2	-11292.8	0.16	--	2872.18	2662.46	0.13	--
2	4	2	-9497.18	0.13	--	2872.18	2662.46	0.13	--
1	6	3	-8588.91	0.12	23.39	3836.56	3165.75	0.17	>1
2	6	3	-12201.1	0.17	16.47	3836.56	3165.75	0.17	>1
1	8	4	-8820.89	0.12	--	3228.38	2618.08	0.14	--
2	8	4	-11969.1	0.17	--	3228.38	2618.08	0.14	--
1	10	5	-11392.8	0.16	17.63	4803.47	4651.86	0.22	>1
2	10	5	-9397.25	0.13	21.38	4803.47	4651.86	0.22	>1
1	12	6	-11230.7	0.15	--	4221.86	4101.02	0.2	--
2	12	6	-9559.26	0.13	--	4221.86	4101.02	0.2	--
1	14	7	-8516.67	0.12	23.59	5215.69	4703.5	0.24	>1
2	14	7	-12273.3	0.17	16.37	5215.69	4703.5	0.24	>1
1	16	8	-8758.8	0.12	--	4586.87	4145.4	0.21	--
2	16	8	-12031.2	0.17	--	4586.87	4145.4	0.21	--
1	18	9	-14795.1	0.2	13.58	5306.02	523.4	0.2	>1
2	18	9	-5994.88	0.08	33.51	5306.02	523.4	0.2	>1
1	20	10	-14155	0.2	--	4525.34	347.02	0.17	--
2	20	10	-6634.99	0.09	--	4525.34	347.02	0.17	--
1	22	11	-14773.5	0.2	13.6	5566.14	1837.38	0.22	>1
2	22	11	-6016.55	0.08	33.39	5566.14	1837.38	0.22	>1
1	24	12	-14136.4	0.19	--	4794.4	1682.02	0.19	--
2	24	12	-6653.61	0.09	--	4794.4	1682.02	0.19	--
1	26	13	-5208.2	0.07	38.57	6234.06	351.27	0.23	>1
2	26	13	-15581.8	0.21	12.89	6234.06	351.27	0.23	>1
1	28	14	-5915.24	0.08	--	5379.4	199.08	0.2	--
2	28	14	-14874.8	0.21	--	5379.4	199.08	0.2	--
1	30	15	-5186.54	0.07	38.74	6565.26	2009.5	0.26	>1
2	30	15	-15603.5	0.22	12.88	6565.26	2009.5	0.26	>1
1	32	16	-5896.61	0.08	--	5699.82	1829.96	0.23	--
2	32	16	-14893.4	0.21	--	5699.82	1829.96	0.23	--
1	34	17	-11962.9	0.16	16.79	3746.61	3239.93	0.17	>1
2	34	17	-8827.1	0.12	22.76	3746.61	3239.93	0.17	>1
1	36	18	-11720.8	0.16	--	3118.21	2681.83	0.14	--
2	36	18	-9069.23	0.13	--	3118.21	2681.83	0.14	--
1	38	19	-9086.83	0.13	22.11	3553.8	3188.29	0.16	>1
2	38	19	-11703.2	0.16	17.17	3553.8	3188.29	0.16	>1
1	40	20	-9248.84	0.13	--	2974.53	2637.44	0.14	--
2	40	20	-11541.2	0.16	--	2974.53	2637.44	0.14	--
1	42	21	-11890.7	0.16	16.9	4965.07	4629.32	0.23	>1
2	42	21	-8899.33	0.12	22.57	4965.07	4629.32	0.23	>1
1	44	22	-11658.7	0.16	--	4354.24	4081.65	0.2	--
2	44	22	-9131.31	0.13	--	4354.24	4081.65	0.2	--
1	46	23	-9014.59	0.12	22.29	4965.42	4680.96	0.23	>1
2	46	23	-11775.4	0.16	17.06	4965.42	4680.96	0.23	>1
1	48	24	-9186.75	0.13	--	4373.37	4126.03	0.2	--
2	48	24	-11603.2	0.16	--	4373.37	4126.03	0.2	--
1	50	25	-15293	0.21	13.14	5902.95	545.93	0.22	>1
2	50	25	-5496.96	0.08	36.55	5902.95	545.93	0.22	>1
1	52	26	-14583	0.2	--	5038.89	366.39	0.19	--
2	52	26	-6207.04	0.09	--	5038.89	366.39	0.19	--
1	54	27	-15271.4	0.21	13.16	6126.61	1814.84	0.24	>1
2	54	27	-5518.63	0.08	36.4	6126.61	1814.84	0.24	>1
1	56	28	-14564.3	0.2	--	5272.24	1662.65	0.21	--
2	56	28	-6225.66	0.09	--	5272.24	1662.65	0.21	--
1	58	29	-5706.12	0.08	35.21	5639.06	373.81	0.21	>1
2	58	29	-15083.9	0.21	13.32	5639.06	373.81	0.21	>1
1	60	30	-6343.19	0.09	--	4867.08	218.45	0.18	--
2	60	30	-14446.8	0.2	--	4867.08	218.45	0.18	--
1	62	31	-5684.45	0.08	35.34	5991.71	1986.97	0.24	>1
2	62	31	-15105.6	0.21	13.3	5991.71	1986.97	0.24	>1
1	64	32	-6324.56	0.09	--	5209.31	1810.59	0.21	--
2	64	32	-14465.4	0.2	--	5209.31	1810.59	0.21	--
1	66	33	-9186.03	0.13	21.87	1039.05	989.59	0.05	>1
2	66	33	-9713.97	0.13	20.68	1039.05	989.59	0.05	>1
1	68	34	-9180.66	0.13	21.88	1607.01	1574.17	0.07	>1
2	68	34	-9719.34	0.13	20.67	1607.01	1574.17	0.07	>1
1	70	35	-9539.43	0.13	21.06	1279.99	1275.49	0.06	>1
2	70	35	-9360.57	0.13	21.46	1279.99	1275.49	0.06	>1
1	72	36	-8827.26	0.12	22.76	1489.33	1288.27	0.07	>1
2	72	36	-10072.7	0.14	19.95	1489.33	1288.27	0.07	>1
1	74	37	-9260.81	0.13	--	667.19	627.38	0.03	--
2	74	37	-9639.19	0.13	--	667.19	627.38	0.03	--

Relazione geotecnica

1	76	38	-9255.45	0.13	--	1234.23	1211.95	0.06	--
2	76	38	-9644.55	0.13	--	1234.23	1211.95	0.06	--
1	78	39	-9614.22	0.13	--	934.29	913.27	0.04	--
2	78	39	-9285.78	0.13	--	934.29	913.27	0.04	--
1	80	40	-8902.04	0.12	--	1135.76	926.06	0.05	--
2	80	40	-9997.96	0.14	--	1135.76	926.06	0.05	--
1	82	41	-9297.08	0.13	--	481.96	445.66	0.02	--
2	82	41	-9602.93	0.13	--	481.96	445.66	0.02	--
1	84	42	-9291.71	0.13	--	1047.6	1030.23	0.05	--
2	84	42	-9608.29	0.13	--	1047.6	1030.23	0.05	--
1	86	43	-9650.48	0.13	--	770.1	731.55	0.04	--
2	86	43	-9249.52	0.13	--	770.1	731.55	0.04	--
1	88	44	-8938.31	0.12	--	964.92	744.34	0.04	--
2	88	44	-9961.7	0.14	--	964.92	744.34	0.04	--
1	90	45	-9311.58	0.13	--	408.29	372.97	0.02	--
2	90	45	-9588.42	0.13	--	408.29	372.97	0.02	--
1	92	46	-9306.21	0.13	--	972.97	957.55	0.05	--
2	92	46	-9593.79	0.13	--	972.97	957.55	0.05	--
1	94	47	-9664.98	0.13	--	707.57	658.87	0.03	--
2	94	47	-9235.02	0.13	--	707.57	658.87	0.03	--
1	96	48	-8952.81	0.12	--	898.38	671.65	0.04	--
2	96	48	-9947.19	0.14	--	898.38	671.65	0.04	--

Plinto n. 11

Tipo palo=Trivellato

Rotazione testa libera

Coefficiente di efficienza=1.00

Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>

Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	0	1.2
2	0	-1.2

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{lim}=252333.00 <daN>

q_p=28.63 <daN/cm²>

QP_{lim}=143893.00 <daN>

k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>

q_p=16.60 <daN/cm²>

QP_{lim}=83431.40 <daN>

k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-11663.8	0.16	16.44	3936.06	3629.66	0.18	>1
2	1	1	-9126.22	0.13	21.01	3936.06	3629.66	0.18	>1
1	3	2	-11449.5	0.16	--	3311.48	3060.18	0.15	--
2	3	2	-9340.5	0.13	--	3311.48	3060.18	0.15	--
1	5	3	-8758.33	0.12	21.9	4074.18	3569.53	0.18	>1
2	5	3	-12031.7	0.17	15.94	4074.18	3569.53	0.18	>1
1	7	4	-8952.32	0.12	--	3471.05	3008.5	0.16	--
2	7	4	-11837.7	0.16	--	3471.05	3008.5	0.16	--
1	9	5	-11580.4	0.16	16.56	4654.21	4431.48	0.21	>1
2	9	5	-9209.57	0.13	20.82	4654.21	4431.48	0.21	>1
1	11	6	-11377.9	0.16	--	4044.04	3868.23	0.19	--
2	11	6	-9412.13	0.13	--	4044.04	3868.23	0.19	--
1	13	7	-8674.98	0.12	22.11	4943.15	4491.61	0.23	>1

Relazione geotecnica

2	13	7	-12115	0.17	15.83	4943.15	4491.61	0.23	>1
1	15	8	-8880.68	0.12	--	4320.63	3919.91	0.2	--
2	15	8	-11909.3	0.16	--	4320.63	3919.91	0.2	--
1	17	9	-15024.3	0.21	12.76	5624.19	878.41	0.21	>1
2	17	9	-5765.69	0.08	33.26	5624.19	878.41	0.21	>1
1	19	10	-14337.8	0.2	--	4782.23	695.52	0.18	--
2	19	10	-6452.18	0.09	--	4782.23	695.52	0.18	--
1	21	11	-14999.3	0.21	12.79	5735.76	1539.94	0.23	>1
2	21	11	-5790.69	0.08	33.12	5735.76	1539.94	0.23	>1
1	23	12	-14316.3	0.2	--	4904.62	1383	0.19	--
2	23	12	-6473.67	0.09	--	4904.62	1383	0.19	--
1	25	13	-5339.45	0.07	35.92	6104.42	677.99	0.23	>1
2	25	13	-15450.5	0.21	12.41	6104.42	677.99	0.23	>1
1	27	14	-6013.86	0.08	--	5283.34	523.27	0.2	--
2	27	14	-14776.1	0.2	--	5283.34	523.27	0.2	--
1	29	15	-5314.45	0.07	36.08	6340.2	1740.36	0.25	>1
2	29	15	-15475.6	0.21	12.39	6340.2	1740.36	0.25	>1
1	31	16	-5992.37	0.08	--	5507.32	1555.25	0.22	--
2	31	16	-14797.6	0.2	--	5507.32	1555.25	0.22	--
1	33	17	-11602.8	0.16	16.53	3923.01	3645.46	0.18	>1
2	33	17	-9187.22	0.13	20.87	3923.01	3645.46	0.18	>1
1	35	18	-11397.1	0.16	--	3300.6	3073.76	0.15	--
2	35	18	-9392.93	0.13	--	3300.6	3073.76	0.15	--
1	37	19	-8697.32	0.12	22.05	4123.7	3585.34	0.19	>1
2	37	19	-12092.7	0.17	15.86	4123.7	3585.34	0.19	>1
1	39	20	-8899.89	0.12	--	3514.53	3022.08	0.16	--
2	39	20	-11890.1	0.16	--	3514.53	3022.08	0.16	--
1	41	21	-11519.4	0.16	16.65	4617.24	4415.68	0.21	>1
2	41	21	-9270.57	0.13	20.69	4617.24	4415.68	0.21	>1
1	43	22	-11325.4	0.16	--	4013.1	3854.65	0.19	--
2	43	22	-9464.56	0.13	--	4013.1	3854.65	0.19	--
1	45	23	-8613.98	0.12	22.26	4959.9	4475.81	0.23	>1
2	45	23	-12176	0.17	15.75	4959.9	4475.81	0.23	>1
1	47	24	-8828.25	0.12	--	4335.22	3906.32	0.2	--
2	47	24	-11961.7	0.16	--	4335.22	3906.32	0.2	--
1	49	25	-14963.3	0.21	12.82	5554.42	894.21	0.21	>1
2	49	25	-5826.69	0.08	32.91	5554.42	894.21	0.21	>1
1	51	26	-14285.4	0.2	--	4722.01	709.11	0.18	--
2	51	26	-6504.61	0.09	--	4722.01	709.11	0.18	--
1	53	27	-14938.3	0.21	12.84	5661	1524.13	0.22	>1
2	53	27	-5851.7	0.08	32.77	5661	1524.13	0.22	>1
1	55	28	-14263.9	0.2	--	4840.43	1369.42	0.19	--
2	55	28	-6526.1	0.09	--	4840.43	1369.42	0.19	--
1	57	29	-5278.45	0.07	36.33	6178.93	693.79	0.23	>1
2	57	29	-15511.6	0.21	12.36	6178.93	693.79	0.23	>1
1	59	30	-5961.43	0.08	--	5347.3	536.85	0.2	--
2	59	30	-14828.6	0.2	--	5347.3	536.85	0.2	--
1	61	31	-5253.45	0.07	36.5	6406.35	1724.56	0.25	>1
2	61	31	-15536.6	0.21	12.34	6406.35	1724.56	0.25	>1
1	63	32	-5939.94	0.08	--	5563.92	1541.67	0.22	--
2	63	32	-14850.1	0.2	--	5563.92	1541.67	0.22	--
1	65	33	-9009.22	0.12	21.29	657.42	390.43	0.03	>1
2	65	33	-9890.78	0.14	19.39	657.42	390.43	0.03	>1
1	67	34	-9003.03	0.12	21.3	1125.31	989.25	0.05	>1
2	67	34	-9896.97	0.14	19.38	1125.31	989.25	0.05	>1
1	69	35	-9365.85	0.13	20.48	689.83	682.4	0.03	>1
2	69	35	-9534.15	0.13	20.11	689.83	682.4	0.03	>1
1	71	36	-8646.4	0.12	22.18	1190.01	697.28	0.05	>1
2	71	36	-10253.6	0.14	18.7	1190.01	697.28	0.05	>1
1	73	37	-9134.13	0.13	--	429.04	201.01	0.02	--
2	73	37	-9765.87	0.13	--	429.04	201.01	0.02	--
1	75	38	-9127.94	0.13	--	888.31	799.84	0.04	--
2	75	38	-9772.06	0.13	--	888.31	799.84	0.04	--
1	77	39	-9490.76	0.13	--	495.4	492.98	0.02	--
2	77	39	-9409.24	0.13	--	495.4	492.98	0.02	--
1	79	40	-8771.31	0.12	--	959.8	507.87	0.04	--
2	79	40	-10128.7	0.14	--	959.8	507.87	0.04	--
1	81	41	-9195.65	0.13	--	327.34	118.29	0.01	--
2	81	41	-9704.35	0.13	--	327.34	118.29	0.01	--
1	83	42	-9189.46	0.13	--	782.31	717.12	0.04	--
2	83	42	-9710.54	0.13	--	782.31	717.12	0.04	--
1	85	43	-9552.28	0.13	--	428.22	410.26	0.02	--
2	85	43	-9347.72	0.13	--	428.22	410.26	0.02	--
1	87	44	-8832.83	0.12	--	853.96	425.14	0.04	--
2	87	44	-10067.2	0.14	--	853.96	425.14	0.04	--
1	89	45	-9220.26	0.13	--	288.55	85.2	0.01	--
2	89	45	-9679.74	0.13	--	288.55	85.2	0.01	--
1	91	46	-9214.07	0.13	--	740.3	684.03	0.03	--
2	91	46	-9685.93	0.13	--	740.3	684.03	0.03	--

Relazione geotecnica

1	93	47	-9576.89	0.13	--	406.74	377.17	0.02	--
2	93	47	-9323.11	0.13	--	406.74	377.17	0.02	--
1	95	48	-8857.44	0.12	--	812	392.06	0.03	--
2	95	48	-10042.6	0.14	--	812	392.06	0.03	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-11663.8	0.16	17.22	3936.06	3629.66	0.18	>1
2	2	1	-9126.22	0.13	22.01	3936.06	3629.66	0.18	>1
1	4	2	-11449.5	0.16	--	3311.48	3060.18	0.15	--
2	4	2	-9340.5	0.13	--	3311.48	3060.18	0.15	--
1	6	3	-8758.33	0.12	22.94	4074.18	3569.53	0.18	>1
2	6	3	-12031.7	0.17	16.7	4074.18	3569.53	0.18	>1
1	8	4	-8952.32	0.12	--	3471.05	3008.5	0.16	--
2	8	4	-11837.7	0.16	--	3471.05	3008.5	0.16	--
1	10	5	-11580.4	0.16	17.35	4654.21	4431.48	0.21	>1
2	10	5	-9209.57	0.13	21.81	4654.21	4431.48	0.21	>1
1	12	6	-11377.9	0.16	--	4044.04	3868.23	0.19	--
2	12	6	-9412.13	0.13	--	4044.04	3868.23	0.19	--
1	14	7	-8674.98	0.12	23.16	4943.15	4491.61	0.23	>1
2	14	7	-12115	0.17	16.58	4943.15	4491.61	0.23	>1
1	16	8	-8880.68	0.12	--	4320.63	3919.91	0.2	--
2	16	8	-11909.3	0.16	--	4320.63	3919.91	0.2	--
1	18	9	-15024.3	0.21	13.37	5624.19	878.41	0.21	>1
2	18	9	-5765.69	0.08	34.84	5624.19	878.41	0.21	>1
1	20	10	-14337.8	0.2	--	4782.23	695.52	0.18	--
2	20	10	-6452.18	0.09	--	4782.23	695.52	0.18	--
1	22	11	-14999.3	0.21	13.39	5735.76	1539.94	0.23	>1
2	22	11	-5790.69	0.08	34.69	5735.76	1539.94	0.23	>1
1	24	12	-14316.3	0.2	--	4904.62	1383	0.19	--
2	24	12	-6473.67	0.09	--	4904.62	1383	0.19	--
1	26	13	-5339.45	0.07	37.63	6104.42	677.99	0.23	>1
2	26	13	-15450.5	0.21	13	6104.42	677.99	0.23	>1
1	28	14	-6013.86	0.08	--	5283.34	523.27	0.2	--
2	28	14	-14776.1	0.2	--	5283.34	523.27	0.2	--
1	30	15	-5314.45	0.07	37.8	6340.2	1740.36	0.25	>1
2	30	15	-15475.6	0.21	12.98	6340.2	1740.36	0.25	>1
1	32	16	-5992.37	0.08	--	5507.32	1555.25	0.22	--
2	32	16	-14797.6	0.2	--	5507.32	1555.25	0.22	--
1	34	17	-11602.8	0.16	17.32	3923.01	3645.46	0.18	>1
2	34	17	-9187.22	0.13	21.87	3923.01	3645.46	0.18	>1
1	36	18	-11397.1	0.16	--	3300.6	3073.76	0.15	--
2	36	18	-9392.93	0.13	--	3300.6	3073.76	0.15	--
1	38	19	-8697.32	0.12	23.1	4123.7	3585.34	0.19	>1
2	38	19	-12092.7	0.17	16.61	4123.7	3585.34	0.19	>1
1	40	20	-8899.89	0.12	--	3514.53	3022.08	0.16	--
2	40	20	-11890.1	0.16	--	3514.53	3022.08	0.16	--
1	42	21	-11519.4	0.16	17.44	4617.24	4415.68	0.21	>1
2	42	21	-9270.57	0.13	21.67	4617.24	4415.68	0.21	>1
1	44	22	-11325.4	0.16	--	4013.1	3854.65	0.19	--
2	44	22	-9464.56	0.13	--	4013.1	3854.65	0.19	--
1	46	23	-8613.98	0.12	23.32	4959.9	4475.81	0.23	>1
2	46	23	-12176	0.17	16.5	4959.9	4475.81	0.23	>1
1	48	24	-8828.25	0.12	--	4335.22	3906.32	0.2	--
2	48	24	-11961.7	0.16	--	4335.22	3906.32	0.2	--
1	50	25	-14963.3	0.21	13.43	5554.42	894.21	0.21	>1
2	50	25	-5826.69	0.08	34.48	5554.42	894.21	0.21	>1
1	52	26	-14285.4	0.2	--	4722.01	709.11	0.18	--
2	52	26	-6504.61	0.09	--	4722.01	709.11	0.18	--
1	54	27	-14938.3	0.21	13.45	5661	1524.13	0.22	>1
2	54	27	-5851.7	0.08	34.33	5661	1524.13	0.22	>1
1	56	28	-14263.9	0.2	--	4840.43	1369.42	0.19	--
2	56	28	-6526.1	0.09	--	4840.43	1369.42	0.19	--
1	58	29	-5278.45	0.07	38.06	6178.93	693.79	0.23	>1
2	58	29	-15511.6	0.21	12.95	6178.93	693.79	0.23	>1
1	60	30	-5961.43	0.08	--	5347.3	536.85	0.2	--
2	60	30	-14828.6	0.2	--	5347.3	536.85	0.2	--
1	62	31	-5253.45	0.07	38.24	6406.35	1724.56	0.25	>1
2	62	31	-15536.6	0.21	12.93	6406.35	1724.56	0.25	>1
1	64	32	-5939.94	0.08	--	5563.92	1541.67	0.22	--
2	64	32	-14850.1	0.2	--	5563.92	1541.67	0.22	--
1	66	33	-9009.22	0.12	22.3	657.42	390.43	0.03	>1
2	66	33	-9890.78	0.14	20.31	657.42	390.43	0.03	>1
1	68	34	-9003.03	0.12	22.32	1125.31	989.25	0.05	>1
2	68	34	-9896.97	0.14	20.3	1125.31	989.25	0.05	>1
1	70	35	-9365.85	0.13	21.45	689.83	682.4	0.03	>1

Relazione geotecnica

2	70	35	-9534.15	0.13	21.07	689.83	682.4	0.03	>1
1	72	36	-8646.4	0.12	23.24	1190.01	697.28	0.05	>1
2	72	36	-10253.6	0.14	19.59	1190.01	697.28	0.05	>1
1	74	37	-9134.13	0.13	--	429.04	201.01	0.02	--
2	74	37	-9765.87	0.13	--	429.04	201.01	0.02	--
1	76	38	-9127.94	0.13	--	888.31	799.84	0.04	--
2	76	38	-9772.06	0.13	--	888.31	799.84	0.04	--
1	78	39	-9490.76	0.13	--	495.4	492.98	0.02	--
2	78	39	-9409.24	0.13	--	495.4	492.98	0.02	--
1	80	40	-8771.31	0.12	--	959.8	507.87	0.04	--
2	80	40	-10128.7	0.14	--	959.8	507.87	0.04	--
1	82	41	-9195.65	0.13	--	327.34	118.29	0.01	--
2	82	41	-9704.35	0.13	--	327.34	118.29	0.01	--
1	84	42	-9189.46	0.13	--	782.31	717.12	0.04	--
2	84	42	-9710.54	0.13	--	782.31	717.12	0.04	--
1	86	43	-9552.28	0.13	--	428.22	410.26	0.02	--
2	86	43	-9347.72	0.13	--	428.22	410.26	0.02	--
1	88	44	-8832.83	0.12	--	853.96	425.14	0.04	--
2	88	44	-10067.2	0.14	--	853.96	425.14	0.04	--
1	90	45	-9220.26	0.13	--	288.55	85.2	0.01	--
2	90	45	-9679.74	0.13	--	288.55	85.2	0.01	--
1	92	46	-9214.07	0.13	--	740.3	684.03	0.03	--
2	92	46	-9685.93	0.13	--	740.3	684.03	0.03	--
1	94	47	-9576.89	0.13	--	406.74	377.17	0.02	--
2	94	47	-9323.11	0.13	--	406.74	377.17	0.02	--
1	96	48	-8857.44	0.12	--	812	392.06	0.03	--
2	96	48	-10042.6	0.14	--	812	392.06	0.03	--

Plinto n. 12

Tipo palo=Trivellato
 Rotazione testa libera
 Coefficiente di efficienza=1.00
 Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>
 Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	0	1.2
2	0	-1.2

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{lim}=252333.00 <daN>
 q_p=28.63 <daN/cm²>
 QP_{lim}=143893.00 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>
 q_p=16.60 <daN/cm²>
 QP_{lim}=83431.40 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-12022.5	0.17	15.95	5022.49	4627.19	0.23	>1
2	1	1	-8767.45	0.12	21.87	5022.49	4627.19	0.23	>1
1	3	2	-11768.5	0.16	--	4387.01	4065.6	0.2	--
2	3	2	-9021.47	0.12	--	4387.01	4065.6	0.2	--
1	5	3	-9078.72	0.13	21.12	4820.64	4554.52	0.22	>1
2	5	3	-11711.3	0.16	16.37	4820.64	4554.52	0.22	>1
1	7	4	-9238.36	0.13	--	4236.93	4003.14	0.2	--
2	7	4	-11551.6	0.16	--	4236.93	4003.14	0.2	--

Relazione geotecnica

1	9	5	-11988.7	0.17	16	3814.08	3299.95	0.17	>1
2	9	5	-8801.27	0.12	21.79	3814.08	3299.95	0.17	>1
1	11	6	-11739.5	0.16	--	3186.28	2747.63	0.14	--
2	11	6	-9050.54	0.12	--	3186.28	2747.63	0.14	--
1	13	7	-9044.9	0.12	21.2	3741.58	3372.63	0.17	>1
2	13	7	-11745.1	0.16	16.33	3741.58	3372.63	0.17	>1
1	15	8	-9209.3	0.13	--	3149.78	2810.1	0.14	--
2	15	8	-11580.7	0.16	--	3149.78	2810.1	0.14	--
1	17	9	-15445.2	0.21	12.42	6362.39	1937.48	0.25	>1
2	17	9	-5344.82	0.07	35.88	6362.39	1937.48	0.25	>1
1	19	10	-14710.2	0.2	--	5467.21	1753.85	0.22	--
2	19	10	-6079.78	0.08	--	5467.21	1753.85	0.22	--
1	21	11	-15435	0.21	12.42	6064.07	440.66	0.23	>1
2	21	11	-5354.97	0.07	35.81	6064.07	440.66	0.23	>1
1	23	12	-14701.5	0.2	--	5175.94	290.13	0.19	--
2	23	12	-6088.5	0.08	--	5175.94	290.13	0.19	--
1	25	13	-5632.41	0.08	34.05	5961.23	1695.23	0.24	>1
2	25	13	-15157.6	0.21	12.65	5961.23	1695.23	0.24	>1
1	27	14	-6276.33	0.09	--	5178.45	1545.63	0.2	--
2	27	14	-14513.7	0.2	--	5178.45	1545.63	0.2	--
1	29	15	-5622.26	0.08	34.11	5767.86	682.92	0.22	>1
2	29	15	-15167.7	0.21	12.64	5767.86	682.92	0.22	>1
1	31	16	-6267.61	0.09	--	4977.88	498.34	0.19	--
2	31	16	-14522.4	0.2	--	4977.88	498.34	0.19	--
1	33	17	-11384.8	0.16	16.84	4783.68	4633.88	0.22	>1
2	33	17	-9405.21	0.13	20.39	4783.68	4633.88	0.22	>1
1	35	18	-11220.4	0.15	--	4190.1	4071.35	0.19	--
2	35	18	-9569.61	0.13	--	4190.1	4071.35	0.19	--
1	37	19	-8440.96	0.12	22.72	5128.63	4561.2	0.23	>1
2	37	19	-12349	0.17	15.53	5128.63	4561.2	0.23	>1
1	39	20	-8690.22	0.12	--	4500.68	4008.88	0.2	--
2	39	20	-12099.8	0.17	--	4500.68	4008.88	0.2	--
1	41	21	-11351	0.16	16.89	3487.35	3293.27	0.16	>1
2	41	21	-9439.03	0.13	20.32	3487.35	3293.27	0.16	>1
1	43	22	-11191.3	0.15	--	2903.64	2741.89	0.13	--
2	43	22	-9598.68	0.13	--	2903.64	2741.89	0.13	--
1	45	23	-8407.14	0.12	22.81	4125.51	3365.94	0.18	>1
2	45	23	-12382.9	0.17	15.49	4125.51	3365.94	0.18	>1
1	47	24	-8661.16	0.12	--	3491.9	2804.35	0.16	--
2	47	24	-12128.8	0.17	--	3491.9	2804.35	0.16	--
1	49	25	-14807.4	0.2	12.95	5640.55	1944.17	0.23	>1
2	49	25	-5982.58	0.08	32.05	5640.55	1944.17	0.23	>1
1	51	26	-14162.1	0.2	--	4850.88	1759.59	0.2	--
2	51	26	-6627.92	0.09	--	4850.88	1759.59	0.2	--
1	53	27	-14797.3	0.2	12.96	5300.53	433.98	0.2	>1
2	53	27	-5992.72	0.08	32	5300.53	433.98	0.2	>1
1	55	28	-14153.4	0.2	--	4518.99	284.38	0.17	--
2	55	28	-6636.64	0.09	--	4518.99	284.38	0.17	--
1	57	29	-4994.65	0.07	38.39	6700.17	1701.91	0.26	>1
2	57	29	-15795.3	0.22	12.14	6700.17	1701.91	0.26	>1
1	59	30	-5728.19	0.08	--	5811.09	1551.38	0.23	--
2	59	30	-15061.8	0.21	--	5811.09	1551.38	0.23	--
1	61	31	-4984.51	0.07	38.47	6527.71	676.23	0.25	>1
2	61	31	-15805.5	0.22	12.13	6527.71	676.23	0.25	>1
1	63	32	-5719.47	0.08	--	5632.22	492.6	0.21	--
2	63	32	-15070.5	0.21	--	5632.22	492.6	0.21	--
1	65	33	-9155.76	0.13	20.95	1537.91	1496.83	0.07	>1
2	65	33	-9744.25	0.13	19.68	1537.91	1496.83	0.07	>1
1	67	34	-9153.24	0.13	20.95	975.29	907.95	0.04	>1
2	67	34	-9746.76	0.13	19.68	975.29	907.95	0.04	>1
1	69	35	-9518.98	0.13	20.15	1214.21	1211.39	0.06	>1
2	69	35	-9381.03	0.13	20.44	1214.21	1211.39	0.06	>1
1	71	36	-8790.02	0.12	21.82	1432.27	1193.39	0.06	>1
2	71	36	-10110	0.14	18.97	1432.27	1193.39	0.06	>1
1	73	37	-9237.1	0.13	--	1174.7	1146.58	0.05	--
2	73	37	-9662.9	0.13	--	1174.7	1146.58	0.05	--
1	75	38	-9234.58	0.13	--	614.7	557.7	0.03	--
2	75	38	-9665.42	0.13	--	614.7	557.7	0.03	--
1	77	39	-9600.32	0.13	--	879.83	861.14	0.04	--
2	77	39	-9299.68	0.13	--	879.83	861.14	0.04	--
1	79	40	-8871.37	0.12	--	1092.26	843.14	0.05	--
2	79	40	-10028.6	0.14	--	1092.26	843.14	0.05	--
1	81	41	-9273.08	0.13	--	970.9	947.4	0.05	--
2	81	41	-9626.92	0.13	--	970.9	947.4	0.05	--
1	83	42	-9270.57	0.13	--	418.21	358.53	0.02	--
2	83	42	-9629.43	0.13	--	418.21	358.53	0.02	--
1	85	43	-9636.3	0.13	--	698.7	661.96	0.03	--
2	85	43	-9263.7	0.13	--	698.7	661.96	0.03	--
1	87	44	-8907.35	0.12	--	915.82	643.97	0.04	--

Relazione geotecnica

2	87	44	-9992.65	0.14	--	915.82	643.97	0.04	--
1	89	45	-9287.48	0.13	--	889.38	867.73	0.04	--
2	89	45	-9612.52	0.13	--	889.38	867.73	0.04	--
1	91	46	-9284.97	0.13	--	342.03	278.86	0.02	--
2	91	46	-9615.04	0.13	--	342.03	278.86	0.02	--
1	93	47	-9650.7	0.13	--	630.13	582.29	0.03	--
2	93	47	-9249.3	0.13	--	630.13	582.29	0.03	--
1	95	48	-8921.75	0.12	--	848.69	564.3	0.04	--
2	95	48	-9978.26	0.14	--	848.69	564.3	0.04	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-12022.5	0.17	16.71	5022.49	4627.19	0.23	>1
2	2	1	-8767.45	0.12	22.91	5022.49	4627.19	0.23	>1
1	4	2	-11768.5	0.16	--	4387.01	4065.6	0.2	--
2	4	2	-9021.47	0.12	--	4387.01	4065.6	0.2	--
1	6	3	-9078.72	0.13	22.13	4820.64	4554.52	0.22	>1
2	6	3	-11711.3	0.16	17.15	4820.64	4554.52	0.22	>1
1	8	4	-9238.36	0.13	--	4236.93	4003.14	0.2	--
2	8	4	-11551.6	0.16	--	4236.93	4003.14	0.2	--
1	10	5	-11988.7	0.17	16.76	3814.08	3299.95	0.17	>1
2	10	5	-8801.27	0.12	22.83	3814.08	3299.95	0.17	>1
1	12	6	-11739.5	0.16	--	3186.28	2747.63	0.14	--
2	12	6	-9050.54	0.12	--	3186.28	2747.63	0.14	--
1	14	7	-9044.9	0.12	22.21	3741.58	3372.63	0.17	>1
2	14	7	-11745.1	0.16	17.11	3741.58	3372.63	0.17	>1
1	16	8	-9209.3	0.13	--	3149.78	2810.1	0.14	--
2	16	8	-11580.7	0.16	--	3149.78	2810.1	0.14	--
1	18	9	-15445.2	0.21	13.01	6362.39	1937.48	0.25	>1
2	18	9	-5344.82	0.07	37.59	6362.39	1937.48	0.25	>1
1	20	10	-14710.2	0.2	--	5467.21	1753.85	0.22	--
2	20	10	-6079.78	0.08	--	5467.21	1753.85	0.22	--
1	22	11	-15435	0.21	13.02	6064.07	440.66	0.23	>1
2	22	11	-5354.97	0.07	37.52	6064.07	440.66	0.23	>1
1	24	12	-14701.5	0.2	--	5175.94	290.13	0.19	--
2	24	12	-6088.5	0.08	--	5175.94	290.13	0.19	--
1	26	13	-5632.41	0.08	35.67	5961.23	1695.23	0.24	>1
2	26	13	-15157.6	0.21	13.25	5961.23	1695.23	0.24	>1
1	28	14	-6276.33	0.09	--	5178.45	1545.63	0.2	--
2	28	14	-14513.7	0.2	--	5178.45	1545.63	0.2	--
1	30	15	-5622.26	0.08	35.73	5767.86	682.92	0.22	>1
2	30	15	-15167.7	0.21	13.25	5767.86	682.92	0.22	>1
1	32	16	-6267.61	0.09	--	4977.88	498.34	0.19	--
2	32	16	-14522.4	0.2	--	4977.88	498.34	0.19	--
1	34	17	-11384.8	0.16	17.65	4783.68	4633.88	0.22	>1
2	34	17	-9405.21	0.13	21.36	4783.68	4633.88	0.22	>1
1	36	18	-11220.4	0.15	--	4190.1	4071.35	0.19	--
2	36	18	-9569.61	0.13	--	4190.1	4071.35	0.19	--
1	38	19	-8440.96	0.12	23.8	5128.63	4561.2	0.23	>1
2	38	19	-12349	0.17	16.27	5128.63	4561.2	0.23	>1
1	40	20	-8690.22	0.12	--	4500.68	4008.88	0.2	--
2	40	20	-12099.8	0.17	--	4500.68	4008.88	0.2	--
1	42	21	-11351	0.16	17.7	3487.35	3293.27	0.16	>1
2	42	21	-9439.03	0.13	21.28	3487.35	3293.27	0.16	>1
1	44	22	-11191.3	0.15	--	2903.64	2741.89	0.13	--
2	44	22	-9598.68	0.13	--	2903.64	2741.89	0.13	--
1	46	23	-8407.14	0.12	23.9	4125.51	3365.94	0.18	>1
2	46	23	-12382.9	0.17	16.22	4125.51	3365.94	0.18	>1
1	48	24	-8661.16	0.12	--	3491.9	2804.35	0.16	--
2	48	24	-12128.8	0.17	--	3491.9	2804.35	0.16	--
1	50	25	-14807.4	0.2	13.57	5640.55	1944.17	0.23	>1
2	50	25	-5982.58	0.08	33.58	5640.55	1944.17	0.23	>1
1	52	26	-14162.1	0.2	--	4850.88	1759.59	0.2	--
2	52	26	-6627.92	0.09	--	4850.88	1759.59	0.2	--
1	54	27	-14797.3	0.2	13.58	5300.53	433.98	0.2	>1
2	54	27	-5992.72	0.08	33.52	5300.53	433.98	0.2	>1
1	56	28	-14153.4	0.2	--	4518.99	284.38	0.17	--
2	56	28	-6636.64	0.09	--	4518.99	284.38	0.17	--
1	58	29	-4994.65	0.07	40.22	6700.17	1701.91	0.26	>1
2	58	29	-15795.3	0.22	12.72	6700.17	1701.91	0.26	>1
1	60	30	-5728.19	0.08	--	5811.09	1551.38	0.23	--
2	60	30	-15061.8	0.21	--	5811.09	1551.38	0.23	--
1	62	31	-4984.51	0.07	40.31	6527.71	676.23	0.25	>1
2	62	31	-15805.5	0.22	12.71	6527.71	676.23	0.25	>1
1	64	32	-5719.47	0.08	--	5632.22	492.6	0.21	--
2	64	32	-15070.5	0.21	--	5632.22	492.6	0.21	--

Relazione geotecnica

1	66	33	-9155.76	0.13	21.94	1537.91	1496.83	0.07	>1
2	66	33	-9744.25	0.13	20.62	1537.91	1496.83	0.07	>1
1	68	34	-9153.24	0.13	21.95	975.29	907.95	0.04	>1
2	68	34	-9746.76	0.13	20.61	975.29	907.95	0.04	>1
1	70	35	-9518.98	0.13	21.11	1214.21	1211.39	0.06	>1
2	70	35	-9381.03	0.13	21.42	1214.21	1211.39	0.06	>1
1	72	36	-8790.02	0.12	22.86	1432.27	1193.39	0.06	>1
2	72	36	-10110	0.14	19.87	1432.27	1193.39	0.06	>1
1	74	37	-9237.1	0.13	--	1174.7	1146.58	0.05	--
2	74	37	-9662.9	0.13	--	1174.7	1146.58	0.05	--
1	76	38	-9234.58	0.13	--	614.7	557.7	0.03	--
2	76	38	-9665.42	0.13	--	614.7	557.7	0.03	--
1	78	39	-9600.32	0.13	--	879.83	861.14	0.04	--
2	78	39	-9299.68	0.13	--	879.83	861.14	0.04	--
1	80	40	-8871.37	0.12	--	1092.26	843.14	0.05	--
2	80	40	-10028.6	0.14	--	1092.26	843.14	0.05	--
1	82	41	-9273.08	0.13	--	970.9	947.4	0.05	--
2	82	41	-9626.92	0.13	--	970.9	947.4	0.05	--
1	84	42	-9270.57	0.13	--	418.21	358.53	0.02	--
2	84	42	-9629.43	0.13	--	418.21	358.53	0.02	--
1	86	43	-9636.3	0.13	--	698.7	661.96	0.03	--
2	86	43	-9263.7	0.13	--	698.7	661.96	0.03	--
1	88	44	-8907.35	0.12	--	915.82	643.97	0.04	--
2	88	44	-9992.65	0.14	--	915.82	643.97	0.04	--
1	90	45	-9287.48	0.13	--	889.38	867.73	0.04	--
2	90	45	-9612.52	0.13	--	889.38	867.73	0.04	--
1	92	46	-9284.97	0.13	--	342.03	278.86	0.02	--
2	92	46	-9615.04	0.13	--	342.03	278.86	0.02	--
1	94	47	-9650.7	0.13	--	630.13	582.29	0.03	--
2	94	47	-9249.3	0.13	--	630.13	582.29	0.03	--
1	96	48	-8921.75	0.12	--	848.69	564.3	0.04	--
2	96	48	-9978.26	0.14	--	848.69	564.3	0.04	--

Plinto n. 13

Tipo palo=Trivellato
 Rotazione testa libera
 Coefficiente di efficienza=1.00
 Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>
 Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp	Yp
	<m>	<m>
1	0	1.2
2	0	-1.2

Verifiche in condizioni drenate

Zp	τ_s	k_s	σ_h	k_h
<m>	<daN/cm ² >	<daN/cm ² >	<daN/cm ² >	<daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{lim}=252333.00 <daN>
 q_p=28.63 <daN/cm²>
 QP_{lim}=143893.00 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp	τ_s	k_s	σ_h	k_h
<m>	<daN/cm ² >	<daN/cm ² >	<daN/cm ² >	<daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>
 q_p=16.60 <daN/cm²>
 QP_{lim}=83431.40 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N	Ced	Sic.V	T	M	Sps	Sic.O
			<daN>	<cm>		<daN>	<daNm>	<cm>	
1	1	1	-12975.5	0.18	14.78	6398.54	5599.29	0.29	>1
2	1	1	-7814.47	0.11	24.54	6398.54	5599.29	0.29	>1
1	3	2	-12676.2	0.17	--	5794.45	5107.07	0.26	--

Relazione geotecnica

2	3	2	-8113.82	0.11	--	5794.45	5107.07	0.26	--
1	5	3	-10008.3	0.14	19.16	5666.9	5647.86	0.26	>1
2	5	3	-10781.7	0.15	17.79	5666.9	5647.86	0.26	>1
1	7	4	-10125.9	0.14	--	5158.94	5148.82	0.24	--
2	7	4	-10664.1	0.15	--	5158.94	5148.82	0.24	--
1	9	5	-12941.3	0.18	14.82	3417.96	1531.62	0.14	>1
2	9	5	-7848.68	0.11	24.43	3417.96	1531.62	0.14	>1
1	11	6	-12646.8	0.17	--	2888.88	1021.82	0.12	--
2	11	6	-8143.22	0.11	--	2888.88	1021.82	0.12	--
1	13	7	-9974.05	0.14	19.23	1566.72	1483.05	0.07	>1
2	13	7	-10816	0.15	17.73	1566.72	1483.05	0.07	>1
1	15	8	-10096.5	0.14	--	1043.49	980.07	0.05	--
2	15	8	-10693.5	0.15	--	1043.49	980.07	0.05	--
1	17	9	-16425.4	0.23	11.68	7851.71	3046.81	0.32	>1
2	17	9	-4364.62	0.06	43.94	7851.71	3046.81	0.32	>1
1	19	10	-15641.3	0.22	--	6936.9	2913.26	0.28	--
2	19	10	-5148.74	0.07	--	6936.9	2913.26	0.28	--
1	21	11	-16415.1	0.23	11.68	7280.93	907.53	0.28	>1
2	21	11	-4374.88	0.06	43.83	7280.93	907.53	0.28	>1
1	23	12	-15632.4	0.22	--	6376.13	1074.59	0.24	--
2	23	12	-5157.56	0.07	--	6376.13	1074.59	0.24	--
1	25	13	-6534.46	0.09	29.35	5635.35	3208.71	0.24	>1
2	25	13	-14255.5	0.2	13.45	5635.35	3208.71	0.24	>1
1	27	14	-7140.2	0.1	--	4957.03	3052.41	0.21	--
2	27	14	-13649.8	0.19	--	4957.03	3052.41	0.21	--
1	29	15	-6524.2	0.09	29.39	4766.48	1069.44	0.19	>1
2	29	15	-14265.8	0.2	13.44	4766.48	1069.44	0.19	>1
1	31	16	-7131.38	0.1	--	4100.12	1213.74	0.16	--
2	31	16	-13658.6	0.19	--	4100.12	1213.74	0.16	--
1	33	17	-11716.3	0.16	16.37	5893.17	5675.86	0.27	>1
2	33	17	-9073.68	0.13	21.13	5893.17	5675.86	0.27	>1
1	35	18	-11593.9	0.16	--	5369.22	5172.88	0.25	--
2	35	18	-9196.09	0.13	--	5369.22	5172.88	0.25	--
1	37	19	-8749.05	0.12	21.92	6055.6	5724.43	0.28	>1
2	37	19	-12041	0.17	15.93	6055.6	5724.43	0.28	>1
1	39	20	-9043.59	0.12	--	5460.97	5214.62	0.25	--
2	39	20	-11746.4	0.16	--	5460.97	5214.62	0.25	--
1	41	21	-11682.1	0.16	16.42	2121.97	1455.06	0.09	>1
2	41	21	-9107.89	0.13	21.06	2121.97	1455.06	0.09	>1
1	43	22	-11564.5	0.16	--	1698.09	956.01	0.07	--
2	43	22	-9225.5	0.13	--	1698.09	956.01	0.07	--
1	45	23	-8714.83	0.12	22	2458.3	1406.48	0.1	>1
2	45	23	-12075.2	0.17	15.88	2458.3	1406.48	0.1	>1
1	47	24	-9014.19	0.12	--	1892.47	914.26	0.08	--
2	47	24	-11775.8	0.16	--	1892.47	914.26	0.08	--
1	49	25	-15166.2	0.21	12.64	6521.94	3123.37	0.27	>1
2	49	25	-5623.83	0.08	34.1	6521.94	3123.37	0.27	>1
1	51	26	-14559	0.2	--	5817.45	2979.06	0.24	--
2	51	26	-6231.01	0.09	--	5817.45	2979.06	0.24	--
1	53	27	-15155.9	0.21	12.65	5797.22	984.1	0.22	>1
2	53	27	-5634.09	0.08	34.04	5797.22	984.1	0.22	>1
1	55	28	-14550.2	0.2	--	5114.95	1140.4	0.2	--
2	55	28	-6239.83	0.09	--	5114.95	1140.4	0.2	--
1	57	29	-5275.25	0.07	36.35	6966.93	3285.27	0.29	>1
2	57	29	-15514.8	0.21	12.36	6966.93	3285.27	0.29	>1
1	59	30	-6057.93	0.08	--	6067.12	3118.22	0.25	--
2	59	30	-14732.1	0.2	--	6067.12	3118.22	0.25	--
1	61	31	-5264.99	0.07	36.42	6261.78	1146	0.24	>1
2	61	31	-15525	0.21	12.35	6261.78	1146	0.24	>1
1	63	32	-6049.11	0.08	--	5369.75	1279.55	0.21	--
2	63	32	-14740.9	0.2	--	5369.75	1279.55	0.21	--
1	65	33	-10365	0.14	18.5	4176.37	4029.44	0.19	>1
2	65	33	-8534.95	0.12	22.47	4176.37	4029.44	0.19	>1
1	67	34	-10362.5	0.14	18.51	3667.02	3499.71	0.17	>1
2	67	34	-8537.49	0.12	22.46	3667.02	3499.71	0.17	>1
1	69	35	-10731.2	0.15	17.87	4060.83	3758.56	0.19	>1
2	69	35	-8168.84	0.11	23.48	4060.83	3758.56	0.19	>1
1	71	36	-9996.4	0.14	19.18	3827.17	3770.59	0.18	>1
2	71	36	-8903.6	0.12	21.54	3827.17	3770.59	0.18	>1
1	73	37	-10093.4	0.14	--	3054.96	2955.79	0.14	--
2	73	37	-8806.6	0.12	--	3054.96	2955.79	0.14	--
1	75	38	-10090.9	0.14	--	2545.03	2426.06	0.12	--
2	75	38	-8809.14	0.12	--	2545.03	2426.06	0.12	--
1	77	39	-10459.5	0.14	--	2945.55	2684.91	0.13	--
2	77	39	-8440.49	0.12	--	2945.55	2684.91	0.13	--
1	79	40	-9724.75	0.13	--	2717.02	2696.94	0.13	--
2	79	40	-9175.25	0.13	--	2717.02	2696.94	0.13	--
1	81	41	-9927.06	0.14	--	2462.47	2395	0.11	--
2	81	41	-8972.94	0.12	--	2462.47	2395	0.11	--

Relazione geotecnica

1	83	42	-9924.52	0.14	--	1950.25	1865.27	0.09	--
2	83	42	-8975.48	0.12	--	1950.25	1865.27	0.09	--
1	85	43	-10293.2	0.14	--	2352.8	2124.12	0.11	--
2	85	43	-8606.83	0.12	--	2352.8	2124.12	0.11	--
1	87	44	-9558.42	0.13	--	2140.11	2136.15	0.1	--
2	87	44	-9341.59	0.13	--	2140.11	2136.15	0.1	--
1	89	45	-9860.53	0.14	--	2225.88	2170.68	0.1	--
2	89	45	-9039.47	0.12	--	2225.88	2170.68	0.1	--
1	91	46	-9857.99	0.14	--	1712.44	1640.96	0.08	--
2	91	46	-9042.01	0.12	--	1712.44	1640.96	0.08	--
1	93	47	-10226.6	0.14	--	2116.09	1899.81	0.1	--
2	93	47	-8673.36	0.12	--	2116.09	1899.81	0.1	--
1	95	48	-9491.88	0.13	--	1912.49	1911.83	0.09	--
2	95	48	-9408.12	0.13	--	1912.49	1911.83	0.09	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-12975.5	0.18	15.48	6398.54	5599.29	0.29	>1
2	2	1	-7814.47	0.11	25.71	6398.54	5599.29	0.29	>1
1	4	2	-12676.2	0.17	--	5794.45	5107.07	0.26	--
2	4	2	-8113.82	0.11	--	5794.45	5107.07	0.26	--
1	6	3	-10008.3	0.14	20.07	5666.9	5647.86	0.26	>1
2	6	3	-10781.7	0.15	18.63	5666.9	5647.86	0.26	>1
1	8	4	-10125.9	0.14	--	5158.94	5148.82	0.24	--
2	8	4	-10664.1	0.15	--	5158.94	5148.82	0.24	--
1	10	5	-12941.3	0.18	15.52	3417.96	1531.62	0.14	>1
2	10	5	-7848.68	0.11	25.6	3417.96	1531.62	0.14	>1
1	12	6	-12646.8	0.17	--	2888.88	1021.82	0.12	--
2	12	6	-8143.22	0.11	--	2888.88	1021.82	0.12	--
1	14	7	-9974.05	0.14	20.14	1566.72	1483.05	0.07	>1
2	14	7	-10816	0.15	18.57	1566.72	1483.05	0.07	>1
1	16	8	-10096.5	0.14	--	1043.49	980.07	0.05	--
2	16	8	-10693.5	0.15	--	1043.49	980.07	0.05	--
1	18	9	-16425.4	0.23	12.23	7851.71	3046.81	0.32	>1
2	18	9	-4364.62	0.06	46.03	7851.71	3046.81	0.32	>1
1	20	10	-15641.3	0.22	--	6936.9	2913.26	0.28	--
2	20	10	-5148.74	0.07	--	6936.9	2913.26	0.28	--
1	22	11	-16415.1	0.23	12.24	7280.93	907.53	0.28	>1
2	22	11	-4374.88	0.06	45.92	7280.93	907.53	0.28	>1
1	24	12	-15632.4	0.22	--	6376.13	1074.59	0.24	--
2	24	12	-5157.56	0.07	--	6376.13	1074.59	0.24	--
1	26	13	-6534.46	0.09	30.75	5635.35	3208.71	0.24	>1
2	26	13	-14255.5	0.2	14.09	5635.35	3208.71	0.24	>1
1	28	14	-7140.2	0.1	--	4957.03	3052.41	0.21	--
2	28	14	-13649.8	0.19	--	4957.03	3052.41	0.21	--
1	30	15	-6524.2	0.09	30.79	4766.48	1069.44	0.19	>1
2	30	15	-14265.8	0.2	14.08	4766.48	1069.44	0.19	>1
1	32	16	-7131.38	0.1	--	4100.12	1213.74	0.16	--
2	32	16	-13658.6	0.19	--	4100.12	1213.74	0.16	--
1	34	17	-11716.3	0.16	17.15	5893.17	5675.86	0.27	>1
2	34	17	-9073.68	0.13	22.14	5893.17	5675.86	0.27	>1
1	36	18	-11593.9	0.16	--	5369.22	5172.88	0.25	--
2	36	18	-9196.09	0.13	--	5369.22	5172.88	0.25	--
1	38	19	-8749.05	0.12	22.96	6055.6	5724.43	0.28	>1
2	38	19	-12041	0.17	16.68	6055.6	5724.43	0.28	>1
1	40	20	-9043.59	0.12	--	5460.97	5214.62	0.25	--
2	40	20	-11746.4	0.16	--	5460.97	5214.62	0.25	--
1	42	21	-11682.1	0.16	17.2	2121.97	1455.06	0.09	>1
2	42	21	-9107.89	0.13	22.06	2121.97	1455.06	0.09	>1
1	44	22	-11564.5	0.16	--	1698.09	956.01	0.07	--
2	44	22	-9225.5	0.13	--	1698.09	956.01	0.07	--
1	46	23	-8714.83	0.12	23.05	2458.3	1406.48	0.1	>1
2	46	23	-12075.2	0.17	16.64	2458.3	1406.48	0.1	>1
1	48	24	-9014.19	0.12	--	1892.47	914.26	0.08	--
2	48	24	-11775.8	0.16	--	1892.47	914.26	0.08	--
1	50	25	-15166.2	0.21	13.25	6521.94	3123.37	0.27	>1
2	50	25	-5623.83	0.08	35.72	6521.94	3123.37	0.27	>1
1	52	26	-14559	0.2	--	5817.45	2979.06	0.24	--
2	52	26	-6231.01	0.09	--	5817.45	2979.06	0.24	--
1	54	27	-15155.9	0.21	13.26	5797.22	984.1	0.22	>1
2	54	27	-5634.09	0.08	35.66	5797.22	984.1	0.22	>1
1	56	28	-14550.2	0.2	--	5114.95	1140.4	0.2	--
2	56	28	-6239.83	0.09	--	5114.95	1140.4	0.2	--
1	58	29	-5275.25	0.07	38.08	6966.93	3285.27	0.29	>1
2	58	29	-15514.8	0.21	12.95	6966.93	3285.27	0.29	>1
1	60	30	-6057.93	0.08	--	6067.12	3118.22	0.25	--

Relazione geotecnica

2	60	30	-14732.1	0.2	--	6067.12	3118.22	0.25	--
1	62	31	-5264.99	0.07	38.16	6261.78	1146	0.24	>1
2	62	31	-15525	0.21	12.94	6261.78	1146	0.24	>1
1	64	32	-6049.11	0.08	--	5369.75	1279.55	0.21	--
2	64	32	-14740.9	0.2	--	5369.75	1279.55	0.21	--
1	66	33	-10365	0.14	19.38	4176.37	4029.44	0.19	>1
2	66	33	-8534.95	0.12	23.54	4176.37	4029.44	0.19	>1
1	68	34	-10362.5	0.14	19.39	3667.02	3499.71	0.17	>1
2	68	34	-8537.49	0.12	23.53	3667.02	3499.71	0.17	>1
1	70	35	-10731.2	0.15	18.72	4060.83	3758.56	0.19	>1
2	70	35	-8168.84	0.11	24.59	4060.83	3758.56	0.19	>1
1	72	36	-9996.4	0.14	20.1	3827.17	3770.59	0.18	>1
2	72	36	-8903.6	0.12	22.56	3827.17	3770.59	0.18	>1
1	74	37	-10093.4	0.14	--	3054.96	2955.79	0.14	--
2	74	37	-8806.6	0.12	--	3054.96	2955.79	0.14	--
1	76	38	-10090.9	0.14	--	2545.03	2426.06	0.12	--
2	76	38	-8809.14	0.12	--	2545.03	2426.06	0.12	--
1	78	39	-10459.5	0.14	--	2945.55	2684.91	0.13	--
2	78	39	-8440.49	0.12	--	2945.55	2684.91	0.13	--
1	80	40	-9724.75	0.13	--	2717.02	2696.94	0.13	--
2	80	40	-9175.25	0.13	--	2717.02	2696.94	0.13	--
1	82	41	-9927.06	0.14	--	2462.47	2395	0.11	--
2	82	41	-8972.94	0.12	--	2462.47	2395	0.11	--
1	84	42	-9924.52	0.14	--	1950.25	1865.27	0.09	--
2	84	42	-8975.48	0.12	--	1950.25	1865.27	0.09	--
1	86	43	-10293.2	0.14	--	2352.8	2124.12	0.11	--
2	86	43	-8606.83	0.12	--	2352.8	2124.12	0.11	--
1	88	44	-9558.42	0.13	--	2140.11	2136.15	0.1	--
2	88	44	-9341.59	0.13	--	2140.11	2136.15	0.1	--
1	90	45	-9860.53	0.14	--	2225.88	2170.68	0.1	--
2	90	45	-9039.47	0.12	--	2225.88	2170.68	0.1	--
1	92	46	-9857.99	0.14	--	1712.44	1640.96	0.08	--
2	92	46	-9042.01	0.12	--	1712.44	1640.96	0.08	--
1	94	47	-10226.6	0.14	--	2116.09	1899.81	0.1	--
2	94	47	-8673.36	0.12	--	2116.09	1899.81	0.1	--
1	96	48	-9491.88	0.13	--	1912.49	1911.83	0.09	--
2	96	48	-9408.12	0.13	--	1912.49	1911.83	0.09	--

Plinto n. 8

Tipo palo=Trivellato
 Rotazione testa libera
 Coefficiente di efficienza=1.00
 Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>
 Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	0	1.2
2	0	-1.2

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{lim}=252333.00 <daN>
 q_p=28.63 <daN/cm²>
 QP_{lim}=143893.00 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>
 q_p=16.60 <daN/cm²>
 QP_{lim}=83431.40 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-10824.7	0.15	17.72	544.06	173.6	0.02	>1
2	1	1	-9965.32	0.14	19.24	544.06	173.6	0.02	>1
1	3	2	-10776.9	0.15	--	462.04	59.06	0.02	--
2	3	2	-10013.1	0.14	--	462.04	59.06	0.02	--
1	5	3	-8613.72	0.12	22.26	2143.59	161.01	0.08	>1
2	5	3	-12176.3	0.17	15.75	2143.59	161.01	0.08	>1
1	7	4	-8876.59	0.12	--	1822.73	48.23	0.07	--
2	7	4	-11913.4	0.16	--	1822.73	48.23	0.07	--
1	9	5	-10803.2	0.15	17.75	1530.56	1450.06	0.07	>1
2	9	5	-9986.81	0.14	19.2	1530.56	1450.06	0.07	>1
1	11	6	-10758.4	0.15	--	1405.8	1336.45	0.06	--
2	11	6	-10031.6	0.14	--	1405.8	1336.45	0.06	--
1	13	7	-8592.23	0.12	22.32	2611.38	1462.65	0.11	>1
2	13	7	-12197.8	0.17	15.72	2611.38	1462.65	0.11	>1
1	15	8	-8858.13	0.12	--	2283.95	1347.27	0.1	--
2	15	8	-11931.9	0.16	--	2283.95	1347.27	0.1	--
1	17	9	-13396.6	0.18	14.31	3621.93	379.99	0.14	>1
2	17	9	-7393.38	0.1	25.94	3621.93	379.99	0.14	>1
1	19	10	-12987.4	0.18	--	3138.67	416.75	0.12	--
2	19	10	-7802.6	0.11	--	3138.67	416.75	0.12	--
1	21	11	-13390.2	0.18	14.32	3697.32	867.09	0.14	>1
2	21	11	-7399.83	0.1	25.92	3697.32	867.09	0.14	>1
1	23	12	-12981.9	0.18	--	3214.68	835.4	0.13	--
2	23	12	-7808.14	0.11	--	3214.68	835.4	0.13	--
1	25	13	-6026.75	0.08	31.82	5258.86	421.96	0.2	>1
2	25	13	-14763.3	0.2	12.99	5258.86	421.96	0.2	>1
1	27	14	-6653.14	0.09	--	4513.01	452.82	0.17	--
2	27	14	-14136.9	0.19	--	4513.01	452.82	0.17	--
1	29	15	-6020.3	0.08	31.85	5327.77	909.06	0.2	>1
2	29	15	-14769.7	0.2	12.98	5327.77	909.06	0.2	>1
1	31	16	-6647.59	0.09	--	4580.55	871.47	0.18	--
2	31	16	-14142.4	0.19	--	4580.55	871.47	0.18	--
1	33	17	-12376.7	0.17	15.49	2384.76	179.53	0.09	>1
2	33	17	-8413.34	0.12	22.79	2384.76	179.53	0.09	>1
1	35	18	-12110.8	0.17	--	2059.92	64.15	0.08	--
2	35	18	-8679.23	0.12	--	2059.92	64.15	0.08	--
1	37	19	-10165.7	0.14	18.86	321.84	166.94	0.01	>1
2	37	19	-10624.3	0.15	18.05	321.84	166.94	0.01	>1
1	39	20	-10210.5	0.14	--	227.75	53.33	0.01	--
2	39	20	-10579.5	0.15	--	227.75	53.33	0.01	--
1	41	21	-12355.2	0.17	15.52	2760.15	1444.13	0.12	>1
2	41	21	-8434.83	0.12	22.74	2760.15	1444.13	0.12	>1
1	43	22	-12092.3	0.17	--	2433.29	1331.36	0.1	--
2	43	22	-8697.7	0.12	--	2433.29	1331.36	0.1	--
1	45	23	-10144.2	0.14	18.9	1487.49	1456.73	0.07	>1
2	45	23	-10645.8	0.15	18.01	1487.49	1456.73	0.07	>1
1	47	24	-10192	0.14	--	1364.1	1342.18	0.06	--
2	47	24	-10598	0.15	--	1364.1	1342.18	0.06	--
1	49	25	-14948.6	0.21	12.83	5477.1	374.06	0.2	>1
2	49	25	-5841.41	0.08	32.83	5477.1	374.06	0.2	>1
1	51	26	-14321.3	0.2	--	4729.51	411.65	0.18	--
2	51	26	-6468.7	0.09	--	4729.51	411.65	0.18	--
1	53	27	-14942.2	0.21	12.83	5524.12	861.16	0.21	>1
2	53	27	-5847.85	0.08	32.79	5524.12	861.16	0.21	>1
1	55	28	-14315.8	0.2	--	4777.61	830.3	0.18	--
2	55	28	-6474.24	0.09	--	4777.61	830.3	0.18	--
1	57	29	-7578.72	0.1	25.3	3405.04	416.04	0.13	>1
2	57	29	-13211.3	0.18	14.52	3405.04	416.04	0.13	>1
1	59	30	-7987.03	0.11	--	2924.04	447.73	0.11	--
2	59	30	-12803	0.18	--	2924.04	447.73	0.11	--
1	61	31	-7572.28	0.1	25.33	3505.6	903.13	0.14	>1
2	61	31	-13217.7	0.18	14.51	3505.6	903.13	0.14	>1
1	63	32	-7981.49	0.11	--	3023.02	866.38	0.12	--
2	63	32	-12808.5	0.18	--	3023.02	866.38	0.12	--
1	65	33	-9613.65	0.13	19.95	1128.46	1111.24	0.05	>1
2	65	33	-9286.35	0.13	20.65	1128.46	1111.24	0.05	>1
1	67	34	-9612.05	0.13	19.95	1247.11	1231.86	0.06	>1
2	67	34	-9287.95	0.13	20.65	1247.11	1231.86	0.06	>1
1	69	35	-9886.59	0.14	19.4	1281.93	1169.99	0.06	>1
2	69	35	-9013.41	0.12	21.28	1281.93	1169.99	0.06	>1
1	71	36	-9339.11	0.13	20.53	1180.63	1173.11	0.05	>1
2	71	36	-9560.89	0.13	20.06	1180.63	1173.11	0.05	>1
1	73	37	-9566.97	0.13	--	787.68	775.08	0.04	--
2	73	37	-9333.03	0.13	--	787.68	775.08	0.04	--
1	75	38	-9565.37	0.13	--	906.33	895.69	0.04	--
2	75	38	-9334.63	0.13	--	906.33	895.69	0.04	--
1	77	39	-9839.91	0.14	--	956.13	833.82	0.04	--

Relazione geotecnica

2	77	39	-9060.09	0.12	--	956.13	833.82	0.04	--
1	79	40	-9292.43	0.13	--	858.03	836.94	0.04	--
2	79	40	-9607.57	0.13	--	858.03	836.94	0.04	--
1	81	41	-9542.07	0.13	--	605.14	594.97	0.03	--
2	81	41	-9357.93	0.13	--	605.14	594.97	0.03	--
1	83	42	-9540.48	0.13	--	723.78	715.59	0.03	--
2	83	42	-9359.53	0.13	--	723.78	715.59	0.03	--
1	85	43	-9815.01	0.14	--	786.9	653.72	0.04	--
2	85	43	-9084.99	0.13	--	786.9	653.72	0.04	--
1	87	44	-9267.54	0.13	--	692.37	656.84	0.03	--
2	87	44	-9632.47	0.13	--	692.37	656.84	0.03	--
1	89	45	-9532.11	0.13	--	532.13	522.93	0.02	--
2	89	45	-9367.89	0.13	--	532.13	522.93	0.02	--
1	91	46	-9530.52	0.13	--	650.76	643.55	0.03	--
2	91	46	-9369.48	0.13	--	650.76	643.55	0.03	--
1	93	47	-9805.06	0.14	--	721.03	581.68	0.03	--
2	93	47	-9094.95	0.13	--	721.03	581.68	0.03	--
1	95	48	-9257.58	0.13	--	628.73	584.8	0.03	--
2	95	48	-9642.42	0.13	--	628.73	584.8	0.03	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-10824.7	0.15	18.56	544.06	173.6	0.02	>1
2	2	1	-9965.32	0.14	20.16	544.06	173.6	0.02	>1
1	4	2	-10776.9	0.15	--	462.04	59.06	0.02	--
2	4	2	-10013.1	0.14	--	462.04	59.06	0.02	--
1	6	3	-8613.72	0.12	23.32	2143.59	161.01	0.08	>1
2	6	3	-12176.3	0.17	16.5	2143.59	161.01	0.08	>1
1	8	4	-8876.59	0.12	--	1822.73	48.23	0.07	--
2	8	4	-11913.4	0.16	--	1822.73	48.23	0.07	--
1	10	5	-10803.2	0.15	18.6	1530.56	1450.06	0.07	>1
2	10	5	-9986.81	0.14	20.12	1530.56	1450.06	0.07	>1
1	12	6	-10758.4	0.15	--	1405.8	1336.45	0.06	--
2	12	6	-10031.6	0.14	--	1405.8	1336.45	0.06	--
1	14	7	-8592.23	0.12	23.38	2611.38	1462.65	0.11	>1
2	14	7	-12197.8	0.17	16.47	2611.38	1462.65	0.11	>1
1	16	8	-8858.13	0.12	--	2283.95	1347.27	0.1	--
2	16	8	-11931.9	0.16	--	2283.95	1347.27	0.1	--
1	18	9	-13396.6	0.18	15	3621.93	379.99	0.14	>1
2	18	9	-7393.38	0.1	27.17	3621.93	379.99	0.14	>1
1	20	10	-12987.4	0.18	--	3138.67	416.75	0.12	--
2	20	10	-7802.6	0.11	--	3138.67	416.75	0.12	--
1	22	11	-13390.2	0.18	15	3697.32	867.09	0.14	>1
2	22	11	-7399.83	0.1	27.15	3697.32	867.09	0.14	>1
1	24	12	-12981.9	0.18	--	3214.68	835.4	0.13	--
2	24	12	-7808.14	0.11	--	3214.68	835.4	0.13	--
1	26	13	-6026.75	0.08	33.34	5258.86	421.96	0.2	>1
2	26	13	-14763.3	0.2	13.61	5258.86	421.96	0.2	>1
1	28	14	-6653.14	0.09	--	4513.01	452.82	0.17	--
2	28	14	-14136.9	0.19	--	4513.01	452.82	0.17	--
1	30	15	-6020.3	0.08	33.37	5327.77	909.06	0.2	>1
2	30	15	-14769.7	0.2	13.6	5327.77	909.06	0.2	>1
1	32	16	-6647.59	0.09	--	4580.55	871.47	0.18	--
2	32	16	-14142.4	0.19	--	4580.55	871.47	0.18	--
1	34	17	-12376.7	0.17	16.23	2384.76	179.53	0.09	>1
2	34	17	-8413.34	0.12	23.88	2384.76	179.53	0.09	>1
1	36	18	-12110.8	0.17	--	2059.92	64.15	0.08	--
2	36	18	-8679.23	0.12	--	2059.92	64.15	0.08	--
1	38	19	-10165.7	0.14	19.76	321.84	166.94	0.01	>1
2	38	19	-10624.3	0.15	18.91	321.84	166.94	0.01	>1
1	40	20	-10210.5	0.14	--	227.75	53.33	0.01	--
2	40	20	-10579.5	0.15	--	227.75	53.33	0.01	--
1	42	21	-12355.2	0.17	16.26	2760.15	1444.13	0.12	>1
2	42	21	-8434.83	0.12	23.82	2760.15	1444.13	0.12	>1
1	44	22	-12092.3	0.17	--	2433.29	1331.36	0.1	--
2	44	22	-8697.7	0.12	--	2433.29	1331.36	0.1	--
1	46	23	-10144.2	0.14	19.8	1487.49	1456.73	0.07	>1
2	46	23	-10645.8	0.15	18.87	1487.49	1456.73	0.07	>1
1	48	24	-10192	0.14	--	1364.1	1342.18	0.06	--
2	48	24	-10598	0.15	--	1364.1	1342.18	0.06	--
1	50	25	-14948.6	0.21	13.44	5477.1	374.06	0.2	>1
2	50	25	-5841.41	0.08	34.39	5477.1	374.06	0.2	>1
1	52	26	-14321.3	0.2	--	4729.51	411.65	0.18	--
2	52	26	-6468.7	0.09	--	4729.51	411.65	0.18	--
1	54	27	-14942.2	0.21	13.45	5524.12	861.16	0.21	>1
2	54	27	-5847.85	0.08	34.35	5524.12	861.16	0.21	>1

1	56	28	-14315.8	0.2	--	4777.61	830.3	0.18	--
2	56	28	-6474.24	0.09	--	4777.61	830.3	0.18	--
1	58	29	-7578.72	0.1	26.51	3405.04	416.04	0.13	>1
2	58	29	-13211.3	0.18	15.21	3405.04	416.04	0.13	>1
1	60	30	-7987.03	0.11	--	2924.04	447.73	0.11	--
2	60	30	-12803	0.18	--	2924.04	447.73	0.11	--
1	62	31	-7572.28	0.1	26.53	3505.6	903.13	0.14	>1
2	62	31	-13217.7	0.18	15.2	3505.6	903.13	0.14	>1
1	64	32	-7981.49	0.11	--	3023.02	866.38	0.12	--
2	64	32	-12808.5	0.18	--	3023.02	866.38	0.12	--
1	66	33	-9613.65	0.13	20.9	1128.46	1111.24	0.05	>1
2	66	33	-9286.35	0.13	21.63	1128.46	1111.24	0.05	>1
1	68	34	-9612.05	0.13	20.9	1247.11	1231.86	0.06	>1
2	68	34	-9287.95	0.13	21.63	1247.11	1231.86	0.06	>1
1	70	35	-9886.59	0.14	20.32	1281.93	1169.99	0.06	>1
2	70	35	-9013.41	0.12	22.29	1281.93	1169.99	0.06	>1
1	72	36	-9339.11	0.13	21.51	1180.63	1173.11	0.05	>1
2	72	36	-9560.89	0.13	21.01	1180.63	1173.11	0.05	>1
1	74	37	-9566.97	0.13	--	787.68	775.08	0.04	--
2	74	37	-9333.03	0.13	--	787.68	775.08	0.04	--
1	76	38	-9565.37	0.13	--	906.33	895.69	0.04	--
2	76	38	-9334.63	0.13	--	906.33	895.69	0.04	--
1	78	39	-9839.91	0.14	--	956.13	833.82	0.04	--
2	78	39	-9060.09	0.12	--	956.13	833.82	0.04	--
1	80	40	-9292.43	0.13	--	858.03	836.94	0.04	--
2	80	40	-9607.57	0.13	--	858.03	836.94	0.04	--
1	82	41	-9542.07	0.13	--	605.14	594.97	0.03	--
2	82	41	-9357.93	0.13	--	605.14	594.97	0.03	--
1	84	42	-9540.48	0.13	--	723.78	715.59	0.03	--
2	84	42	-9359.53	0.13	--	723.78	715.59	0.03	--
1	86	43	-9815.01	0.14	--	786.9	653.72	0.04	--
2	86	43	-9084.99	0.13	--	786.9	653.72	0.04	--
1	88	44	-9267.54	0.13	--	692.37	656.84	0.03	--
2	88	44	-9632.47	0.13	--	692.37	656.84	0.03	--
1	90	45	-9532.11	0.13	--	532.13	522.93	0.02	--
2	90	45	-9367.89	0.13	--	532.13	522.93	0.02	--
1	92	46	-9530.52	0.13	--	650.76	643.55	0.03	--
2	92	46	-9369.48	0.13	--	650.76	643.55	0.03	--
1	94	47	-9805.06	0.14	--	721.03	581.68	0.03	--
2	94	47	-9094.95	0.13	--	721.03	581.68	0.03	--
1	96	48	-9257.58	0.13	--	628.73	584.8	0.03	--
2	96	48	-9642.42	0.13	--	628.73	584.8	0.03	--

Plinto n. 14

Tipo palo=Trivellato

Rotazione testa libera

Coefficiente di efficienza=1.00

Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>

Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	0	1.2
2	0	-1.2

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{lim}=252333.00 <daN>

q_p=28.63 <daN/cm²>

QP_{lim}=143893.00 <daN>

k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>

q_p=16.60 <daN/cm²>

QP_{lim}=83431.40 <daN>

Relazione geotecnica

k_p=1.42 <daN/cm<

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-11859.3	0.16	16.17	2842.97	2234.91	0.13	>1
2	1	1	-8930.7	0.12	21.47	2842.97	2234.91	0.13	>1
1	3	2	-11685.3	0.16	--	2601.62	2090.73	0.12	--
2	3	2	-9104.74	0.13	--	2601.62	2090.73	0.12	--
1	5	3	-9773.75	0.13	19.62	2303.57	2179.6	0.11	>1
2	5	3	-11016.3	0.15	17.41	2303.57	2179.6	0.11	>1
1	7	4	-9892.76	0.14	--	2130.22	2043.19	0.1	--
2	7	4	-10897.2	0.15	--	2130.22	2043.19	0.1	--
1	9	5	-12937.2	0.18	14.82	3060.91	250.29	0.11	>1
2	9	5	-7852.78	0.11	24.42	3060.91	250.29	0.11	>1
1	11	6	-12611.7	0.17	--	2687.76	384.98	0.1	--
2	11	6	-8178.29	0.11	--	2687.76	384.98	0.1	--
1	13	7	-10851.7	0.15	17.67	581.65	194.98	0.02	>1
2	13	7	-9938.34	0.14	19.3	581.65	194.98	0.02	>1
1	15	8	-10819.2	0.15	--	610.74	337.44	0.03	--
2	15	8	-9970.79	0.14	--	610.74	337.44	0.03	--
1	17	9	-14669.7	0.2	13.07	5374.85	1604.82	0.21	>1
2	17	9	-6120.27	0.08	31.33	5374.85	1604.82	0.21	>1
1	19	10	-14100.8	0.19	--	4709.04	1549.18	0.19	--
2	19	10	-6689.24	0.09	--	4709.04	1549.18	0.19	--
1	21	11	-14993.1	0.21	12.79	5609.3	1009.44	0.22	>1
2	21	11	-5796.9	0.08	33.08	5609.3	1009.44	0.22	>1
1	23	12	-14378.7	0.2	--	4891.72	1037.45	0.19	--
2	23	12	-6411.3	0.09	--	4891.72	1037.45	0.19	--
1	25	13	-7717.86	0.11	24.85	3512.59	1420.46	0.14	>1
2	25	13	-13072.1	0.18	14.67	3512.59	1420.46	0.14	>1
1	27	14	-8125.77	0.11	--	3057.66	1390.72	0.13	--
2	27	14	-12664.2	0.17	--	3057.66	1390.72	0.13	--
1	29	15	-8041.24	0.11	23.85	2942.55	825.07	0.12	>1
2	29	15	-12748.8	0.18	15.04	2942.55	825.07	0.12	>1
1	31	16	-8403.7	0.12	--	2546.1	878.99	0.1	--
2	31	16	-12386.3	0.17	--	2546.1	878.99	0.1	--
1	33	17	-10389.8	0.14	18.46	2222.68	2222.67	0.1	>1
2	33	17	-10400.3	0.14	18.44	2222.68	2222.67	0.1	>1
1	35	18	-10422.2	0.14	--	2080.46	2080.21	0.1	--
2	35	18	-10367.8	0.14	--	2080.46	2080.21	0.1	--
1	37	19	-8304.19	0.11	23.09	3315.48	2167.36	0.14	>1
2	37	19	-12485.8	0.17	15.36	3315.48	2167.36	0.14	>1
1	39	20	-8629.7	0.12	--	2935.84	2032.67	0.13	--
2	39	20	-12160.3	0.17	--	2935.84	2032.67	0.13	--
1	41	21	-11467.7	0.16	16.72	1309.03	238.05	0.05	>1
2	41	21	-9322.33	0.13	20.57	1309.03	238.05	0.05	>1
1	43	22	-11348.7	0.16	--	1204.09	374.46	0.05	--
2	43	22	-9441.35	0.13	--	1204.09	374.46	0.05	--
1	45	23	-9382.11	0.13	20.44	1229.13	182.74	0.05	>1
2	45	23	-11407.9	0.16	16.81	1229.13	182.74	0.05	>1
1	47	24	-9556.15	0.13	--	1058.38	326.93	0.04	--
2	47	24	-11233.8	0.15	--	1058.38	326.93	0.04	--
1	49	25	-13200.2	0.18	14.53	3723.93	1592.58	0.15	>1
2	49	25	-7589.83	0.1	25.27	3723.93	1592.58	0.15	>1
1	51	26	-12837.7	0.18	--	3310.55	1538.66	0.14	--
2	51	26	-7952.29	0.11	--	3310.55	1538.66	0.14	--
1	53	27	-13523.5	0.19	14.18	3884.44	997.2	0.15	>1
2	53	27	-7266.45	0.1	26.39	3884.44	997.2	0.15	>1
1	55	28	-13115.6	0.18	--	3422.48	1026.94	0.14	--
2	55	28	-7674.36	0.11	--	3422.48	1026.94	0.14	--
1	57	29	-6248.31	0.09	30.69	5171.46	1408.22	0.2	>1
2	57	29	-14541.7	0.2	13.19	5171.46	1408.22	0.2	>1
1	59	30	-6862.71	0.09	--	4457.79	1380.2	0.18	--
2	59	30	-13927.3	0.19	--	4457.79	1380.2	0.18	--
1	61	31	-6571.68	0.09	29.18	4659.43	812.83	0.18	>1
2	61	31	-14218.3	0.2	13.49	4659.43	812.83	0.18	>1
1	63	32	-7140.65	0.1	--	4000.63	868.48	0.16	--
2	63	32	-13649.4	0.19	--	4000.63	868.48	0.16	--
1	65	33	-10005.2	0.14	19.17	2337.93	2241	0.11	>1
2	65	33	-8894.81	0.12	21.56	2337.93	2241	0.11	>1
1	67	34	-10085.3	0.14	19.01	2228.04	2093.57	0.1	>1
2	67	34	-8814.73	0.12	21.76	2228.04	2093.57	0.1	>1
1	69	35	-10303.4	0.14	18.61	2403.27	2174.13	0.11	>1
2	69	35	-8596.56	0.12	22.31	2403.27	2174.13	0.11	>1
1	71	36	-9787.02	0.13	19.59	2197.96	2160.43	0.1	>1
2	71	36	-9112.98	0.13	21.04	2197.96	2160.43	0.1	>1
1	73	37	-9815.54	0.14	--	1681.47	1623.25	0.08	--

Relazione geotecnica

2	73	37	-9084.47	0.13	--	1681.47	1623.25	0.08	--
1	75	38	-9895.61	0.14	--	1569.71	1475.82	0.07	--
2	75	38	-9004.39	0.12	--	1569.71	1475.82	0.07	--
1	77	39	-10113.8	0.14	--	1748.38	1556.39	0.08	--
2	77	39	-8786.22	0.12	--	1748.38	1556.39	0.08	--
1	79	40	-9597.36	0.13	--	1552.79	1542.69	0.07	--
2	79	40	-9302.64	0.13	--	1552.79	1542.69	0.07	--
1	81	41	-9672.4	0.13	--	1328.48	1301.39	0.06	--
2	81	41	-9227.6	0.13	--	1328.48	1301.39	0.06	--
1	83	42	-9752.48	0.13	--	1209.7	1153.96	0.06	--
2	83	42	-9147.52	0.13	--	1209.7	1153.96	0.06	--
1	85	43	-9970.65	0.14	--	1383.62	1234.53	0.06	--
2	85	43	-8929.35	0.12	--	1383.62	1234.53	0.06	--
1	87	44	-9454.23	0.13	--	1220.84	1220.83	0.06	--
2	87	44	-9445.77	0.13	--	1220.84	1220.83	0.06	--
1	89	45	-9615.15	0.13	--	1189.28	1172.65	0.06	--
2	89	45	-9284.85	0.13	--	1189.28	1172.65	0.06	--
1	91	46	-9695.22	0.13	--	1066.61	1025.22	0.05	--
2	91	46	-9204.78	0.13	--	1066.61	1025.22	0.05	--
1	93	47	-9913.4	0.14	--	1237.73	1105.78	0.06	--
2	93	47	-8986.6	0.12	--	1237.73	1105.78	0.06	--
1	95	48	-9396.97	0.13	--	1093.94	1092.09	0.05	--
2	95	48	-9503.03	0.13	--	1093.94	1092.09	0.05	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-11859.3	0.16	16.94	2842.97	2234.91	0.13	>1
2	2	1	-8930.7	0.12	22.5	2842.97	2234.91	0.13	>1
1	4	2	-11685.3	0.16	--	2601.62	2090.73	0.12	--
2	4	2	-9104.74	0.13	--	2601.62	2090.73	0.12	--
1	6	3	-9773.75	0.13	20.56	2303.57	2179.6	0.11	>1
2	6	3	-11016.3	0.15	18.24	2303.57	2179.6	0.11	>1
1	8	4	-9892.76	0.14	--	2130.22	2043.19	0.1	--
2	8	4	-10897.2	0.15	--	2130.22	2043.19	0.1	--
1	10	5	-12937.2	0.18	15.53	3060.91	250.29	0.11	>1
2	10	5	-7852.78	0.11	25.58	3060.91	250.29	0.11	>1
1	12	6	-12611.7	0.17	--	2687.76	384.98	0.1	--
2	12	6	-8178.29	0.11	--	2687.76	384.98	0.1	--
1	14	7	-10851.7	0.15	18.51	581.65	194.98	0.02	>1
2	14	7	-9938.34	0.14	20.21	581.65	194.98	0.02	>1
1	16	8	-10819.2	0.15	--	610.74	337.44	0.03	--
2	16	8	-9970.79	0.14	--	610.74	337.44	0.03	--
1	18	9	-14669.7	0.2	13.7	5374.85	1604.82	0.21	>1
2	18	9	-6120.27	0.08	32.83	5374.85	1604.82	0.21	>1
1	20	10	-14100.8	0.19	--	4709.04	1549.18	0.19	--
2	20	10	-6689.24	0.09	--	4709.04	1549.18	0.19	--
1	22	11	-14993.1	0.21	13.4	5609.3	1009.44	0.22	>1
2	22	11	-5796.9	0.08	34.66	5609.3	1009.44	0.22	>1
1	24	12	-14378.7	0.2	--	4891.72	1037.45	0.19	--
2	24	12	-6411.3	0.09	--	4891.72	1037.45	0.19	--
1	26	13	-7717.86	0.11	26.03	3512.59	1420.46	0.14	>1
2	26	13	-13072.1	0.18	15.37	3512.59	1420.46	0.14	>1
1	28	14	-8125.77	0.11	--	3057.66	1390.72	0.13	--
2	28	14	-12664.2	0.17	--	3057.66	1390.72	0.13	--
1	30	15	-8041.24	0.11	24.98	2942.55	825.07	0.12	>1
2	30	15	-12748.8	0.18	15.76	2942.55	825.07	0.12	>1
1	32	16	-8403.7	0.12	--	2546.1	878.99	0.1	--
2	32	16	-12386.3	0.17	--	2546.1	878.99	0.1	--
1	34	17	-10389.8	0.14	19.34	2222.68	2222.67	0.1	>1
2	34	17	-10400.3	0.14	19.32	2222.68	2222.67	0.1	>1
1	36	18	-10422.2	0.14	--	2080.46	2080.21	0.1	--
2	36	18	-10367.8	0.14	--	2080.46	2080.21	0.1	--
1	38	19	-8304.19	0.11	24.19	3315.48	2167.36	0.14	>1
2	38	19	-12485.8	0.17	16.09	3315.48	2167.36	0.14	>1
1	40	20	-8629.7	0.12	--	2935.84	2032.67	0.13	--
2	40	20	-12160.3	0.17	--	2935.84	2032.67	0.13	--
1	42	21	-11467.7	0.16	17.52	1309.03	238.05	0.05	>1
2	42	21	-9322.33	0.13	21.55	1309.03	238.05	0.05	>1
1	44	22	-11348.7	0.16	--	1204.09	374.46	0.05	--
2	44	22	-9441.35	0.13	--	1204.09	374.46	0.05	--
1	46	23	-9382.11	0.13	21.41	1229.13	182.74	0.05	>1
2	46	23	-11407.9	0.16	17.61	1229.13	182.74	0.05	>1
1	48	24	-9556.15	0.13	--	1058.38	326.93	0.04	--
2	48	24	-11233.8	0.15	--	1058.38	326.93	0.04	--
1	50	25	-13200.2	0.18	15.22	3723.93	1592.58	0.15	>1
2	50	25	-7589.83	0.1	26.47	3723.93	1592.58	0.15	>1

Relazione geotecnica

1	52	26	-12837.7	0.18	--	3310.55	1538.66	0.14	--
2	52	26	-7952.29	0.11	--	3310.55	1538.66	0.14	--
1	54	27	-13523.5	0.19	14.86	3884.44	997.2	0.15	>1
2	54	27	-7266.45	0.1	27.65	3884.44	997.2	0.15	>1
1	56	28	-13115.6	0.18	--	3422.48	1026.94	0.14	--
2	56	28	-7674.36	0.11	--	3422.48	1026.94	0.14	--
1	58	29	-6248.31	0.09	32.15	5171.46	1408.22	0.2	>1
2	58	29	-14541.7	0.2	13.82	5171.46	1408.22	0.2	>1
1	60	30	-6862.71	0.09	--	4457.79	1380.2	0.18	--
2	60	30	-13927.3	0.19	--	4457.79	1380.2	0.18	--
1	62	31	-6571.68	0.09	30.57	4659.43	812.83	0.18	>1
2	62	31	-14218.3	0.2	14.13	4659.43	812.83	0.18	>1
1	64	32	-7140.65	0.1	--	4000.63	868.48	0.16	--
2	64	32	-13649.4	0.19	--	4000.63	868.48	0.16	--
1	66	33	-10005.2	0.14	20.08	2337.93	2241	0.11	>1
2	66	33	-8894.81	0.12	22.59	2337.93	2241	0.11	>1
1	68	34	-10085.3	0.14	19.92	2228.04	2093.57	0.1	>1
2	68	34	-8814.73	0.12	22.79	2228.04	2093.57	0.1	>1
1	70	35	-10303.4	0.14	19.5	2403.27	2174.13	0.11	>1
2	70	35	-8596.56	0.12	23.37	2403.27	2174.13	0.11	>1
1	72	36	-9787.02	0.13	20.53	2197.96	2160.43	0.1	>1
2	72	36	-9112.98	0.13	22.05	2197.96	2160.43	0.1	>1
1	74	37	-9815.54	0.14	--	1681.47	1623.25	0.08	--
2	74	37	-9084.47	0.13	--	1681.47	1623.25	0.08	--
1	76	38	-9895.61	0.14	--	1569.71	1475.82	0.07	--
2	76	38	-9004.39	0.12	--	1569.71	1475.82	0.07	--
1	78	39	-10113.8	0.14	--	1748.38	1556.39	0.08	--
2	78	39	-8786.22	0.12	--	1748.38	1556.39	0.08	--
1	80	40	-9597.36	0.13	--	1552.79	1542.69	0.07	--
2	80	40	-9302.64	0.13	--	1552.79	1542.69	0.07	--
1	82	41	-9672.4	0.13	--	1328.48	1301.39	0.06	--
2	82	41	-9227.6	0.13	--	1328.48	1301.39	0.06	--
1	84	42	-9752.48	0.13	--	1209.7	1153.96	0.06	--
2	84	42	-9147.52	0.13	--	1209.7	1153.96	0.06	--
1	86	43	-9970.65	0.14	--	1383.62	1234.53	0.06	--
2	86	43	-8929.35	0.12	--	1383.62	1234.53	0.06	--
1	88	44	-9454.23	0.13	--	1220.84	1220.83	0.06	--
2	88	44	-9445.77	0.13	--	1220.84	1220.83	0.06	--
1	90	45	-9615.15	0.13	--	1189.28	1172.65	0.06	--
2	90	45	-9284.85	0.13	--	1189.28	1172.65	0.06	--
1	92	46	-9695.22	0.13	--	1066.61	1025.22	0.05	--
2	92	46	-9204.78	0.13	--	1066.61	1025.22	0.05	--
1	94	47	-9913.4	0.14	--	1237.73	1105.78	0.06	--
2	94	47	-8986.6	0.12	--	1237.73	1105.78	0.06	--
1	96	48	-9396.97	0.13	--	1093.94	1092.09	0.05	--
2	96	48	-9503.03	0.13	--	1093.94	1092.09	0.05	--

Plinto n. 16

Tipo palo=Trivellato
 Rotazione testa libera
 Coefficiente di efficienza=1.00
 Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>
 Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	-1.2	0
2	1.2	0

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{1im}=252333.00 <daN>
 q_p=28.63 <daN/cm²>
 QP_{1im}=143893.00 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{1m}=321694.00 <daN>
 q_p=16.60 <daN/cm²>
 QP_{1m}=83431.40 <daN>
 k_p=1.42 <daN/cm>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-8911.94	0.12	21.52	1883.19	615.76	0.08	>1
2	1	1	-11878.1	0.16	16.14	1883.19	615.76	0.08	>1
1	3	2	-9202.83	0.13	--	1541.66	574.54	0.06	--
2	3	2	-11587.2	0.16	--	1541.66	574.54	0.06	--
1	5	3	-8994.88	0.12	21.32	1710.35	319.99	0.07	>1
2	5	3	-11795.1	0.16	16.26	1710.35	319.99	0.07	>1
1	7	4	-9274.11	0.13	--	1364.54	229.72	0.05	--
2	7	4	-11515.9	0.16	--	1364.54	229.72	0.05	--
1	9	5	-13724.2	0.19	13.97	4039.8	599.58	0.15	>1
2	9	5	-7065.79	0.1	27.14	4039.8	599.58	0.15	>1
1	11	6	-13338.9	0.18	--	3576.88	560.63	0.14	--
2	11	6	-7451.11	0.1	--	3576.88	560.63	0.14	--
1	13	7	-13807.2	0.19	13.89	4108.36	336.16	0.15	>1
2	13	7	-6982.85	0.1	27.46	4108.36	336.16	0.15	>1
1	15	8	-13410.2	0.18	--	3626.4	243.62	0.14	--
2	15	8	-7379.83	0.1	--	3626.4	243.62	0.14	--
1	17	9	-10499.5	0.14	18.26	1706.41	1701.8	0.08	>1
2	17	9	-10290.5	0.14	18.64	1706.41	1701.8	0.08	>1
1	19	10	-10567.3	0.15	--	1522.08	1507.97	0.07	--
2	19	10	-10222.7	0.14	--	1522.08	1507.97	0.07	--
1	21	11	-11943.2	0.16	16.06	2516.15	1696.95	0.11	>1
2	21	11	-8846.85	0.12	21.68	2516.15	1696.95	0.11	>1
1	23	12	-11808.1	0.16	--	2266.47	1503.8	0.1	--
2	23	12	-8981.9	0.12	--	2266.47	1503.8	0.1	--
1	25	13	-10775.9	0.15	17.8	1489.24	1417.35	0.07	>1
2	25	13	-10014.1	0.14	19.15	1489.24	1417.35	0.07	>1
1	27	14	-10804.9	0.15	--	1271.85	1172.88	0.06	--
2	27	14	-9985.1	0.14	--	1271.85	1172.88	0.06	--
1	29	15	-12219.6	0.17	15.69	2610.89	1422.2	0.11	>1
2	29	15	-8570.38	0.12	22.38	2610.89	1422.2	0.11	>1
1	31	16	-12045.7	0.17	--	2304.18	1177.05	0.1	--
2	31	16	-8744.28	0.12	--	2304.18	1177.05	0.1	--
1	33	17	-8156.95	0.11	23.51	2859.22	981	0.11	>1
2	33	17	-12633.1	0.17	15.18	2859.22	981	0.11	>1
1	35	18	-8553.93	0.12	--	2381.24	888.45	0.1	--
2	35	18	-12236.1	0.17	--	2381.24	888.45	0.1	--
1	37	19	-8239.89	0.11	23.27	2586.53	45.25	0.1	>1
2	37	19	-12550.1	0.17	15.28	2586.53	45.25	0.1	>1
1	39	20	-8625.21	0.12	--	2125.41	84.2	0.08	--
2	39	20	-12164.8	0.17	--	2125.41	84.2	0.08	--
1	41	21	-12969.2	0.18	14.79	3236.24	964.82	0.13	>1
2	41	21	-7820.78	0.11	24.52	3236.24	964.82	0.13	>1
1	43	22	-12690	0.17	--	2889.51	874.55	0.11	--
2	43	22	-8100.01	0.11	--	2889.51	874.55	0.11	--
1	45	23	-13052.2	0.18	14.69	3188.73	29.07	0.12	>1
2	45	23	-7737.84	0.11	24.78	3188.73	29.07	0.12	>1
1	47	24	-12761.3	0.18	--	2840.4	70.29	0.1	--
2	47	24	-8028.73	0.11	--	2840.4	70.29	0.1	--
1	49	25	-9744.49	0.13	19.68	2209.53	2067.04	0.1	>1
2	49	25	-11045.5	0.15	17.36	2209.53	2067.04	0.1	>1
1	51	26	-9918.39	0.14	--	1909.55	1821.89	0.09	--
2	51	26	-10871.6	0.15	--	1909.55	1821.89	0.09	--
1	53	27	-11188.2	0.15	17.14	2271.24	2062.18	0.1	>1
2	53	27	-9601.83	0.13	19.97	2271.24	2062.18	0.1	>1
1	55	28	-11159.2	0.15	--	2035.94	1817.71	0.09	--
2	55	28	-9630.8	0.13	--	2035.94	1817.71	0.09	--
1	57	29	-10020.9	0.14	19.14	1143.86	1052.11	0.05	>1
2	57	29	-10769.1	0.15	17.81	1143.86	1052.11	0.05	>1
1	59	30	-10156	0.14	--	905.58	858.97	0.04	--
2	59	30	-10634	0.15	--	905.58	858.97	0.04	--
1	61	31	-11464.6	0.16	16.73	1662.74	1056.97	0.07	>1
2	61	31	-9325.37	0.13	20.56	1662.74	1056.97	0.07	>1
1	63	32	-11396.8	0.16	--	1479.95	863.14	0.06	--
2	63	32	-9393.18	0.13	--	1479.95	863.14	0.06	--
1	65	33	-10372.8	0.14	18.49	1387.34	835.81	0.06	>1
2	65	33	-8527.24	0.12	22.49	1387.34	835.81	0.06	>1
1	67	34	-10730.2	0.15	17.87	1748.36	834.6	0.07	>1
2	67	34	-8169.76	0.11	23.47	1748.36	834.6	0.07	>1
1	69	35	-10541.2	0.15	18.19	1618.41	951.06	0.07	>1

Relazione geotecnica

2	69	35	-8358.77	0.12	22.94	1618.41	951.06	0.07	>1
1	71	36	-10561.8	0.15	18.16	1515.7	719.35	0.06	>1
2	71	36	-8338.23	0.11	23	1515.7	719.35	0.06	>1
1	73	37	-10053.7	0.14	--	922.23	570.76	0.04	--
2	73	37	-8846.35	0.12	--	922.23	570.76	0.04	--
1	75	38	-10411.1	0.14	--	1286.33	569.56	0.05	--
2	75	38	-8488.86	0.12	--	1286.33	569.56	0.05	--
1	77	39	-10222.1	0.14	--	1152.87	686.01	0.05	--
2	77	39	-8677.87	0.12	--	1152.87	686.01	0.05	--
1	79	40	-10242.7	0.14	--	1054.12	454.3	0.04	--
2	79	40	-8657.34	0.12	--	1054.12	454.3	0.04	--
1	81	41	-9876	0.14	--	632.74	372.86	0.03	--
2	81	41	-9024	0.12	--	632.74	372.86	0.03	--
1	83	42	-10233.5	0.14	--	1010.98	371.66	0.04	--
2	83	42	-8666.51	0.12	--	1010.98	371.66	0.04	--
1	85	43	-10044.5	0.14	--	864.38	488.12	0.04	--
2	85	43	-8855.53	0.12	--	864.38	488.12	0.04	--
1	87	44	-10065	0.14	--	781.29	256.41	0.03	--
2	87	44	-8834.99	0.12	--	781.29	256.41	0.03	--
1	89	45	-9804.94	0.14	--	517.38	293.71	0.02	--
2	89	45	-9095.06	0.13	--	517.38	293.71	0.02	--
1	91	46	-10162.4	0.14	--	903.57	292.5	0.04	--
2	91	46	-8737.58	0.12	--	903.57	292.5	0.04	--
1	93	47	-9973.42	0.14	--	749.5	408.96	0.03	--
2	93	47	-8926.59	0.12	--	749.5	408.96	0.03	--
1	95	48	-9993.95	0.14	--	676.38	177.25	0.03	--
2	95	48	-8906.05	0.12	--	676.38	177.25	0.03	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-8911.94	0.12	22.54	1883.19	615.76	0.08	>1
2	2	1	-11878.1	0.16	16.91	1883.19	615.76	0.08	>1
1	4	2	-9202.83	0.13	--	1541.66	574.54	0.06	--
2	4	2	-11587.2	0.16	--	1541.66	574.54	0.06	--
1	6	3	-8994.88	0.12	22.34	1710.35	319.99	0.07	>1
2	6	3	-11795.1	0.16	17.03	1710.35	319.99	0.07	>1
1	8	4	-9274.11	0.13	--	1364.54	229.72	0.05	--
2	8	4	-11515.9	0.16	--	1364.54	229.72	0.05	--
1	10	5	-13724.2	0.19	14.64	4039.8	599.58	0.15	>1
2	10	5	-7065.79	0.1	28.43	4039.8	599.58	0.15	>1
1	12	6	-13338.9	0.18	--	3576.88	560.63	0.14	--
2	12	6	-7451.11	0.1	--	3576.88	560.63	0.14	--
1	14	7	-13807.2	0.19	14.55	4108.36	336.16	0.15	>1
2	14	7	-6982.85	0.1	28.77	4108.36	336.16	0.15	>1
1	16	8	-13410.2	0.18	--	3626.4	243.62	0.14	--
2	16	8	-7379.83	0.1	--	3626.4	243.62	0.14	--
1	18	9	-10499.5	0.14	19.13	1706.41	1701.8	0.08	>1
2	18	9	-10290.5	0.14	19.52	1706.41	1701.8	0.08	>1
1	20	10	-10567.3	0.15	--	1522.08	1507.97	0.07	--
2	20	10	-10222.7	0.14	--	1522.08	1507.97	0.07	--
1	22	11	-11943.2	0.16	16.82	2516.15	1696.95	0.11	>1
2	22	11	-8846.85	0.12	22.71	2516.15	1696.95	0.11	>1
1	24	12	-11808.1	0.16	--	2266.47	1503.8	0.1	--
2	24	12	-8981.9	0.12	--	2266.47	1503.8	0.1	--
1	26	13	-10775.9	0.15	18.64	1489.24	1417.35	0.07	>1
2	26	13	-10014.1	0.14	20.06	1489.24	1417.35	0.07	>1
1	28	14	-10804.9	0.15	--	1271.85	1172.88	0.06	--
2	28	14	-9985.1	0.14	--	1271.85	1172.88	0.06	--
1	30	15	-12219.6	0.17	16.44	2610.89	1422.2	0.11	>1
2	30	15	-8570.38	0.12	23.44	2610.89	1422.2	0.11	>1
1	32	16	-12045.7	0.17	--	2304.18	1177.05	0.1	--
2	32	16	-8744.28	0.12	--	2304.18	1177.05	0.1	--
1	34	17	-8156.95	0.11	24.63	2859.22	981	0.11	>1
2	34	17	-12633.1	0.17	15.9	2859.22	981	0.11	>1
1	36	18	-8553.93	0.12	--	2381.24	888.45	0.1	--
2	36	18	-12236.1	0.17	--	2381.24	888.45	0.1	--
1	38	19	-8239.89	0.11	24.38	2586.53	45.25	0.1	>1
2	38	19	-12550.1	0.17	16.01	2586.53	45.25	0.1	>1
1	40	20	-8625.21	0.12	--	2125.41	84.2	0.08	--
2	40	20	-12164.8	0.17	--	2125.41	84.2	0.08	--
1	42	21	-12969.2	0.18	15.49	3236.24	964.82	0.13	>1
2	42	21	-7820.78	0.11	25.69	3236.24	964.82	0.13	>1
1	44	22	-12690	0.17	--	2889.51	874.55	0.11	--
2	44	22	-8100.01	0.11	--	2889.51	874.55	0.11	--
1	46	23	-13052.2	0.18	15.39	3188.73	29.07	0.12	>1
2	46	23	-7737.84	0.11	25.96	3188.73	29.07	0.12	>1

Relazione geotecnica

1	48	24	-12761.3	0.18	--	2840.4	70.29	0.1	--
2	48	24	-8028.73	0.11	--	2840.4	70.29	0.1	--
1	50	25	-9744.49	0.13	20.62	2209.53	2067.04	0.1	>1
2	50	25	-11045.5	0.15	18.19	2209.53	2067.04	0.1	>1
1	52	26	-9918.39	0.14	--	1909.55	1821.89	0.09	--
2	52	26	-10871.6	0.15	--	1909.55	1821.89	0.09	--
1	54	27	-11188.2	0.15	17.96	2271.24	2062.18	0.1	>1
2	54	27	-9601.83	0.13	20.92	2271.24	2062.18	0.1	>1
1	56	28	-11159.2	0.15	--	2035.94	1817.71	0.09	--
2	56	28	-9630.8	0.13	--	2035.94	1817.71	0.09	--
1	58	29	-10020.9	0.14	20.05	1143.86	1052.11	0.05	>1
2	58	29	-10769.1	0.15	18.66	1143.86	1052.11	0.05	>1
1	60	30	-10156	0.14	--	905.58	858.97	0.04	--
2	60	30	-10634	0.15	--	905.58	858.97	0.04	--
1	62	31	-11464.6	0.16	17.52	1662.74	1056.97	0.07	>1
2	62	31	-9325.37	0.13	21.54	1662.74	1056.97	0.07	>1
1	64	32	-11396.8	0.16	--	1479.95	863.14	0.06	--
2	64	32	-9393.18	0.13	--	1479.95	863.14	0.06	--
1	66	33	-10372.8	0.14	19.37	1387.34	835.81	0.06	>1
2	66	33	-8527.24	0.12	23.56	1387.34	835.81	0.06	>1
1	68	34	-10730.2	0.15	18.72	1748.36	834.6	0.07	>1
2	68	34	-8169.76	0.11	24.59	1748.36	834.6	0.07	>1
1	70	35	-10541.2	0.15	19.06	1618.41	951.06	0.07	>1
2	70	35	-8358.77	0.12	24.04	1618.41	951.06	0.07	>1
1	72	36	-10561.8	0.15	19.02	1515.7	719.35	0.06	>1
2	72	36	-8338.23	0.11	24.09	1515.7	719.35	0.06	>1
1	74	37	-10053.7	0.14	--	922.23	570.76	0.04	--
2	74	37	-8846.35	0.12	--	922.23	570.76	0.04	--
1	76	38	-10411.1	0.14	--	1286.33	569.56	0.05	--
2	76	38	-8488.86	0.12	--	1286.33	569.56	0.05	--
1	78	39	-10222.1	0.14	--	1152.87	686.01	0.05	--
2	78	39	-8677.87	0.12	--	1152.87	686.01	0.05	--
1	80	40	-10242.7	0.14	--	1054.12	454.3	0.04	--
2	80	40	-8657.34	0.12	--	1054.12	454.3	0.04	--
1	82	41	-9876	0.14	--	632.74	372.86	0.03	--
2	82	41	-9024	0.12	--	632.74	372.86	0.03	--
1	84	42	-10233.5	0.14	--	1010.98	371.66	0.04	--
2	84	42	-8666.51	0.12	--	1010.98	371.66	0.04	--
1	86	43	-10044.5	0.14	--	864.38	488.12	0.04	--
2	86	43	-8855.53	0.12	--	864.38	488.12	0.04	--
1	88	44	-10065	0.14	--	781.29	256.41	0.03	--
2	88	44	-8834.99	0.12	--	781.29	256.41	0.03	--
1	90	45	-9804.94	0.14	--	517.38	293.71	0.02	--
2	90	45	-9095.06	0.13	--	517.38	293.71	0.02	--
1	92	46	-10162.4	0.14	--	903.57	292.5	0.04	--
2	92	46	-8737.58	0.12	--	903.57	292.5	0.04	--
1	94	47	-9973.42	0.14	--	749.5	408.96	0.03	--
2	94	47	-8926.59	0.12	--	749.5	408.96	0.03	--
1	96	48	-9993.95	0.14	--	676.38	177.25	0.03	--
2	96	48	-8906.05	0.12	--	676.38	177.25	0.03	--

Plinto n. 17

Tipo palo=Trivellato
 Rotazione testa libera
 Coefficiente di efficienza=1.00
 Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>
 Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	-1.2	0
2	1.2	0

Verifiche in condizioni drenate

zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{1im}=252333.00 <daN>
 q_p=28.63 <daN/cm²>
 QP_{1im}=143893.00 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Relazione geotecnica

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm>	σ_h <daN/cm ² >	k_h <daN/cm>
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

$Q_{S1im}=321694.00$ <daN>
 $q_p=16.60$ <daN/cm²>
 $Q_{P1im}=83431.40$ <daN>
 $k_p=1.42$ <daN/cm>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-8394.71	0.12	22.84	2497.69	690.5	0.1	>1
2	1	1	-12395.3	0.17	15.47	2497.69	690.5	0.1	>1
1	3	2	-8720.72	0.12	--	2106.54	633.15	0.08	--
2	3	2	-12069.3	0.17	--	2106.54	633.15	0.08	--
1	5	3	-8414.27	0.12	22.79	2392.05	269.03	0.09	>1
2	5	3	-12375.7	0.17	15.5	2392.05	269.03	0.09	>1
1	7	4	-8737.54	0.12	--	1998.16	191.55	0.08	--
2	7	4	-12052.5	0.17	--	1998.16	191.55	0.08	--
1	9	5	-13810.3	0.19	13.89	4152.4	667.41	0.16	>1
2	9	5	-6979.66	0.1	27.48	4152.4	667.41	0.16	>1
1	11	6	-13375.4	0.18	--	3628.64	613.3	0.14	--
2	11	6	-7414.64	0.1	--	3628.64	613.3	0.14	--
1	13	7	-13829.9	0.19	13.87	4132.23	292.12	0.15	>1
2	13	7	-6960.09	0.1	27.55	4132.23	292.12	0.15	>1
1	15	8	-13392.2	0.18	--	3602.82	211.39	0.13	--
2	15	8	-7397.83	0.1	--	3602.82	211.39	0.13	--
1	17	9	-10267.4	0.14	18.68	1808.37	1801.87	0.08	>1
2	17	9	-10522.6	0.15	18.22	1808.37	1801.87	0.08	>1
1	19	10	-10330.2	0.14	--	1590.26	1588.36	0.07	--
2	19	10	-10459.8	0.14	--	1590.26	1588.36	0.07	--
1	21	11	-11892	0.16	16.13	2539.5	1794.94	0.11	>1
2	21	11	-8897.96	0.12	21.55	2539.5	1794.94	0.11	>1
1	23	12	-11726.6	0.16	--	2248.87	1582.4	0.1	--
2	23	12	-9063.38	0.12	--	2248.87	1582.4	0.1	--
1	25	13	-10332.6	0.14	18.56	1398.57	1396.57	0.07	>1
2	25	13	-10457.4	0.14	18.34	1398.57	1396.57	0.07	>1
1	27	14	-10386.3	0.14	--	1160.69	1160.64	0.05	--
2	27	14	-10403.7	0.14	--	1160.69	1160.64	0.05	--
1	29	15	-11957.3	0.16	16.04	2341.87	1403.49	0.1	>1
2	29	15	-8832.74	0.12	21.71	2341.87	1403.49	0.1	>1
1	31	16	-11782.7	0.16	--	2033.19	1166.6	0.09	--
2	31	16	-9007.33	0.12	--	2033.19	1166.6	0.09	--
1	33	17	-7599.66	0.1	25.23	3462.13	856.89	0.14	>1
2	33	17	-13190.3	0.18	14.54	3462.13	856.89	0.14	>1
1	35	18	-8037.39	0.11	--	2933.67	776.16	0.12	--
2	35	18	-12752.6	0.18	--	2933.67	776.16	0.12	--
1	37	19	-7619.22	0.11	25.17	3332.52	102.64	0.12	>1
2	37	19	-13170.8	0.18	14.56	3332.52	102.64	0.12	>1
1	39	20	-8054.2	0.11	--	2809.38	48.54	0.1	--
2	39	20	-12735.8	0.18	--	2809.38	48.54	0.1	--
1	41	21	-13015.3	0.18	14.73	3253.02	833.8	0.13	>1
2	41	21	-7774.71	0.11	24.67	3253.02	833.8	0.13	>1
1	43	22	-12692	0.17	--	2858.31	756.31	0.11	--
2	43	22	-8097.98	0.11	--	2858.31	756.31	0.11	--
1	45	23	-13034.9	0.18	14.71	3170.32	125.73	0.12	>1
2	45	23	-7755.15	0.11	24.73	3170.32	125.73	0.12	>1
1	47	24	-12708.8	0.18	--	2777.45	68.39	0.1	--
2	47	24	-8081.16	0.11	--	2777.45	68.39	0.1	--
1	49	25	-9472.3	0.13	20.25	2258.32	1968.26	0.1	>1
2	49	25	-11317.7	0.16	16.94	2258.32	1968.26	0.1	>1
1	51	26	-9646.89	0.13	--	1950.26	1731.36	0.09	--
2	51	26	-11143.1	0.15	--	1950.26	1731.36	0.09	--
1	53	27	-11097	0.15	17.28	2134.58	1961.33	0.1	>1
2	53	27	-9693.01	0.13	19.78	2134.58	1961.33	0.1	>1
1	55	28	-11043.3	0.15	--	1892.68	1725.41	0.09	--
2	55	28	-9746.72	0.13	--	1892.68	1725.41	0.09	--
1	57	29	-9537.52	0.13	20.11	1603.79	1230.18	0.07	>1
2	57	29	-11252.5	0.16	17.04	1603.79	1230.18	0.07	>1
1	59	30	-9702.94	0.13	--	1313.49	1017.63	0.06	--
2	59	30	-11087.1	0.15	--	1313.49	1017.63	0.06	--
1	61	31	-11162.2	0.15	17.18	1542.08	1237.1	0.07	>1
2	61	31	-9627.79	0.13	19.92	1542.08	1237.1	0.07	>1
1	63	32	-11099.3	0.15	--	1327.44	1023.59	0.06	--
2	63	32	-9690.67	0.13	--	1327.44	1023.59	0.06	--

Relazione geotecnica

1	65	33	-9804.83	0.14	19.56	878.06	767.91	0.04	>1
2	65	33	-9095.17	0.13	21.08	878.06	767.91	0.04	>1
1	67	34	-10207.1	0.14	18.79	1188.51	766.19	0.05	>1
2	67	34	-8692.86	0.12	22.06	1188.51	766.19	0.05	>1
1	69	35	-10003.6	0.14	19.17	1107.25	885.85	0.05	>1
2	69	35	-8896.44	0.12	21.56	1107.25	885.85	0.05	>1
1	71	36	-10008.4	0.14	19.16	932.34	648.25	0.04	>1
2	71	36	-8891.59	0.12	21.57	932.34	648.25	0.04	>1
1	73	37	-9648.18	0.13	--	573.54	521.91	0.03	--
2	73	37	-9251.82	0.13	--	573.54	521.91	0.03	--
1	75	38	-10050.5	0.14	--	888.73	520.19	0.04	--
2	75	38	-8849.52	0.12	--	888.73	520.19	0.04	--
1	77	39	-9846.91	0.14	--	797.66	639.85	0.04	--
2	77	39	-9053.09	0.12	--	797.66	639.85	0.04	--
1	79	40	-9851.76	0.14	--	627.88	402.25	0.03	--
2	79	40	-9048.25	0.12	--	627.88	402.25	0.03	--
1	81	41	-9570.59	0.13	--	363.17	333.1	0.02	--
2	81	41	-9329.41	0.13	--	363.17	333.1	0.02	--
1	83	42	-9972.9	0.14	--	709.61	331.38	0.03	--
2	83	42	-8927.1	0.12	--	709.61	331.38	0.03	--
1	85	43	-9769.32	0.13	--	591.83	451.04	0.03	--
2	85	43	-9130.68	0.13	--	591.83	451.04	0.03	--
1	87	44	-9774.17	0.13	--	443.71	213.44	0.02	--
2	87	44	-9125.83	0.13	--	443.71	213.44	0.02	--
1	89	45	-9539.56	0.13	--	279.09	257.57	0.01	--
2	89	45	-9360.44	0.13	--	279.09	257.57	0.01	--
1	91	46	-9941.86	0.14	--	643.3	255.85	0.03	--
2	91	46	-8958.14	0.12	--	643.3	255.85	0.03	--
1	93	47	-9738.29	0.13	--	510.57	375.51	0.02	--
2	93	47	-9161.71	0.13	--	510.57	375.51	0.02	--
1	95	48	-9743.13	0.13	--	377.83	137.91	0.02	--
2	95	48	-9156.87	0.13	--	377.83	137.91	0.02	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-8394.71	0.12	23.93	2497.69	690.5	0.1	>1
2	2	1	-12395.3	0.17	16.21	2497.69	690.5	0.1	>1
1	4	2	-8720.72	0.12	--	2106.54	633.15	0.08	--
2	4	2	-12069.3	0.17	--	2106.54	633.15	0.08	--
1	6	3	-8414.27	0.12	23.88	2392.05	269.03	0.09	>1
2	6	3	-12375.7	0.17	16.23	2392.05	269.03	0.09	>1
1	8	4	-8737.54	0.12	--	1998.16	191.55	0.08	--
2	8	4	-12052.5	0.17	--	1998.16	191.55	0.08	--
1	10	5	-13810.3	0.19	14.55	4152.4	667.41	0.16	>1
2	10	5	-6979.66	0.1	28.78	4152.4	667.41	0.16	>1
1	12	6	-13375.4	0.18	--	3628.64	613.3	0.14	--
2	12	6	-7414.64	0.1	--	3628.64	613.3	0.14	--
1	14	7	-13829.9	0.19	14.53	4132.23	292.12	0.15	>1
2	14	7	-6960.09	0.1	28.86	4132.23	292.12	0.15	>1
1	16	8	-13392.2	0.18	--	3602.82	211.39	0.13	--
2	16	8	-7397.83	0.1	--	3602.82	211.39	0.13	--
1	18	9	-10267.4	0.14	19.57	1808.37	1801.87	0.08	>1
2	18	9	-10522.6	0.15	19.09	1808.37	1801.87	0.08	>1
1	20	10	-10330.2	0.14	--	1590.26	1588.36	0.07	--
2	20	10	-10459.8	0.14	--	1590.26	1588.36	0.07	--
1	22	11	-11892	0.16	16.89	2539.5	1794.94	0.11	>1
2	22	11	-8897.96	0.12	22.58	2539.5	1794.94	0.11	>1
1	24	12	-11726.6	0.16	--	2248.87	1582.4	0.1	--
2	24	12	-9063.38	0.12	--	2248.87	1582.4	0.1	--
1	26	13	-10332.6	0.14	19.44	1398.57	1396.57	0.07	>1
2	26	13	-10457.4	0.14	19.21	1398.57	1396.57	0.07	>1
1	28	14	-10386.3	0.14	--	1160.69	1160.64	0.05	--
2	28	14	-10403.7	0.14	--	1160.69	1160.64	0.05	--
1	30	15	-11957.3	0.16	16.8	2341.87	1403.49	0.1	>1
2	30	15	-8832.74	0.12	22.75	2341.87	1403.49	0.1	>1
1	32	16	-11782.7	0.16	--	2033.19	1166.6	0.09	--
2	32	16	-9007.33	0.12	--	2033.19	1166.6	0.09	--
1	34	17	-7599.66	0.1	26.44	3462.13	856.89	0.14	>1
2	34	17	-13190.3	0.18	15.23	3462.13	856.89	0.14	>1
1	36	18	-8037.39	0.11	--	2933.67	776.16	0.12	--
2	36	18	-12752.6	0.18	--	2933.67	776.16	0.12	--
1	38	19	-7619.22	0.11	26.37	3332.52	102.64	0.12	>1
2	38	19	-13170.8	0.18	15.25	3332.52	102.64	0.12	>1
1	40	20	-8054.2	0.11	--	2809.38	48.54	0.1	--
2	40	20	-12735.8	0.18	--	2809.38	48.54	0.1	--
1	42	21	-13015.3	0.18	15.44	3253.02	833.8	0.13	>1

Relazione geotecnica

2	42	21	-7774.71	0.11	25.84	3253.02	833.8	0.13	>1
1	44	22	-12692	0.17	--	2858.31	756.31	0.11	--
2	44	22	-8097.98	0.11	--	2858.31	756.31	0.11	--
1	46	23	-13034.9	0.18	15.41	3170.32	125.73	0.12	>1
2	46	23	-7755.15	0.11	25.91	3170.32	125.73	0.12	>1
1	48	24	-12708.8	0.18	--	2777.45	68.39	0.1	--
2	48	24	-8081.16	0.11	--	2777.45	68.39	0.1	--
1	50	25	-9472.3	0.13	21.21	2258.32	1968.26	0.1	>1
2	50	25	-11317.7	0.16	17.75	2258.32	1968.26	0.1	>1
1	52	26	-9646.89	0.13	--	1950.26	1731.36	0.09	--
2	52	26	-11143.1	0.15	--	1950.26	1731.36	0.09	--
1	54	27	-11097	0.15	18.1	2134.58	1961.33	0.1	>1
2	54	27	-9693.01	0.13	20.73	2134.58	1961.33	0.1	>1
1	56	28	-11043.3	0.15	--	1892.68	1725.41	0.09	--
2	56	28	-9746.72	0.13	--	1892.68	1725.41	0.09	--
1	58	29	-9537.52	0.13	21.06	1603.79	1230.18	0.07	>1
2	58	29	-11252.5	0.16	17.85	1603.79	1230.18	0.07	>1
1	60	30	-9702.94	0.13	--	1313.49	1017.63	0.06	--
2	60	30	-11087.1	0.15	--	1313.49	1017.63	0.06	--
1	62	31	-11162.2	0.15	18	1542.08	1237.1	0.07	>1
2	62	31	-9627.79	0.13	20.87	1542.08	1237.1	0.07	>1
1	64	32	-11099.3	0.15	--	1327.44	1023.59	0.06	--
2	64	32	-9690.67	0.13	--	1327.44	1023.59	0.06	--
1	66	33	-9804.83	0.14	20.49	878.06	767.91	0.04	>1
2	66	33	-9095.17	0.13	22.09	878.06	767.91	0.04	>1
1	68	34	-10207.1	0.14	19.68	1188.51	766.19	0.05	>1
2	68	34	-8692.86	0.12	23.11	1188.51	766.19	0.05	>1
1	70	35	-10003.6	0.14	20.08	1107.25	885.85	0.05	>1
2	70	35	-8896.44	0.12	22.58	1107.25	885.85	0.05	>1
1	72	36	-10008.4	0.14	20.07	932.34	648.25	0.04	>1
2	72	36	-8891.59	0.12	22.59	932.34	648.25	0.04	>1
1	74	37	-9648.18	0.13	--	573.54	521.91	0.03	--
2	74	37	-9251.82	0.13	--	573.54	521.91	0.03	--
1	76	38	-10050.5	0.14	--	888.73	520.19	0.04	--
2	76	38	-8849.52	0.12	--	888.73	520.19	0.04	--
1	78	39	-9846.91	0.14	--	797.66	639.85	0.04	--
2	78	39	-9053.09	0.12	--	797.66	639.85	0.04	--
1	80	40	-9851.76	0.14	--	627.88	402.25	0.03	--
2	80	40	-9048.25	0.12	--	627.88	402.25	0.03	--
1	82	41	-9570.59	0.13	--	363.17	333.1	0.02	--
2	82	41	-9329.41	0.13	--	363.17	333.1	0.02	--
1	84	42	-9972.9	0.14	--	709.61	331.38	0.03	--
2	84	42	-8927.1	0.12	--	709.61	331.38	0.03	--
1	86	43	-9769.32	0.13	--	591.83	451.04	0.03	--
2	86	43	-9130.68	0.13	--	591.83	451.04	0.03	--
1	88	44	-9774.17	0.13	--	443.71	213.44	0.02	--
2	88	44	-9125.83	0.13	--	443.71	213.44	0.02	--
1	90	45	-9539.56	0.13	--	279.09	257.57	0.01	--
2	90	45	-9360.44	0.13	--	279.09	257.57	0.01	--
1	92	46	-9941.86	0.14	--	643.3	255.85	0.03	--
2	92	46	-8958.14	0.12	--	643.3	255.85	0.03	--
1	94	47	-9738.29	0.13	--	510.57	375.51	0.02	--
2	94	47	-9161.71	0.13	--	510.57	375.51	0.02	--
1	96	48	-9743.13	0.13	--	377.83	137.91	0.02	--
2	96	48	-9156.87	0.13	--	377.83	137.91	0.02	--

Plinto n. 18

Tipo palo=Trivellato
 Rotazione testa libera
 Coefficiente di efficienza=1.00
 Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>
 Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	-1.2	0
2	1.2	0

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{1m}=252333.00 <daN>
 qp=28.63 <daN/cm²>

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QP_{lim}=143893.00 <daN>
 k_p=1.42 <daN/cmq>

Verifiche in condizioni non drenate

Zp <m>	τ _s <daN/cmq>	k _s <daN/cmc>	σ _h <daN/cmq>	k _h <daN/cmc>
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>
 q_p=16.60 <daN/cmq>
 QP_{lim}=83431.40 <daN>
 k_p=1.42 <daN/cmc>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-8020.85	0.11	23.91	2947.05	753.94	0.12	>1
2	1	1	-12769.1	0.18	15.02	2947.05	753.94	0.12	>1
1	3	2	-8353.87	0.12	--	2542.67	682.52	0.1	--
2	3	2	-12436.1	0.17	--	2542.67	682.52	0.1	--
1	5	3	-8044.88	0.11	23.84	2828.48	217.09	0.11	>1
2	5	3	-12745.1	0.18	15.05	2828.48	217.09	0.11	>1
1	7	4	-8374.53	0.12	--	2429.33	152.06	0.09	--
2	7	4	-12415.5	0.17	--	2429.33	152.06	0.09	--
1	9	5	-13530.4	0.19	14.17	3832.62	729.69	0.15	>1
2	9	5	-7259.57	0.1	26.42	3832.62	729.69	0.15	>1
1	11	6	-13089.3	0.18	--	3300.12	661.68	0.13	--
2	11	6	-7700.75	0.11	--	3300.12	661.68	0.13	--
1	13	7	-13554.5	0.19	14.15	3799.03	241.34	0.14	>1
2	13	7	-7235.54	0.1	26.5	3799.03	241.34	0.14	>1
1	15	8	-13109.9	0.18	--	3262.48	172.91	0.12	--
2	15	8	-7680.09	0.11	--	3262.48	172.91	0.12	--
1	17	9	-9921.17	0.14	19.33	1962.5	1878.32	0.09	>1
2	17	9	-10868.8	0.15	17.64	1962.5	1878.32	0.09	>1
1	19	10	-9987.16	0.14	--	1720	1648.9	0.08	--
2	19	10	-10802.8	0.15	--	1720	1648.9	0.08	--
1	21	11	-11574	0.16	16.57	2345.77	1871.05	0.1	>1
2	21	11	-9215.96	0.13	20.81	2345.77	1871.05	0.1	>1
1	23	12	-11407.8	0.16	--	2043.36	1642.65	0.09	--
2	23	12	-9382.23	0.13	--	2043.36	1642.65	0.09	--
1	25	13	-10001.3	0.14	19.17	1438.26	1358.44	0.07	>1
2	25	13	-10788.7	0.15	17.77	1438.26	1358.44	0.07	>1
1	27	14	-10056	0.14	--	1203.85	1133.04	0.06	--
2	27	14	-10734	0.15	--	1203.85	1133.04	0.06	--
1	29	15	-11654.2	0.16	16.45	2036.72	1365.72	0.09	>1
2	29	15	-9135.85	0.13	20.99	2036.72	1365.72	0.09	>1
1	31	16	-11476.6	0.16	--	1727.04	1139.29	0.07	--
2	31	16	-9313.38	0.13	--	1727.04	1139.29	0.07	--
1	33	17	-7227.13	0.1	26.53	3871.41	732.67	0.15	>1
2	33	17	-13562.9	0.19	14.14	3871.41	732.67	0.15	>1
1	35	18	-7671.68	0.11	--	3334.8	664.24	0.13	--
2	35	18	-13118.3	0.18	--	3334.8	664.24	0.13	--
1	37	19	-7251.16	0.1	26.45	3780.13	238.36	0.14	>1
2	37	19	-13538.8	0.19	14.16	3780.13	238.36	0.14	>1
1	39	20	-7692.34	0.11	--	3247.66	170.34	0.12	--
2	39	20	-13097.7	0.18	--	3247.66	170.34	0.12	--
1	41	21	-12736.7	0.18	15.06	2897.97	708.42	0.11	>1
2	41	21	-8053.29	0.11	23.81	2897.97	708.42	0.11	>1
1	43	22	-12407.1	0.17	--	2498.73	643.39	0.1	--
2	43	22	-8382.93	0.12	--	2498.73	643.39	0.1	--
1	45	23	-12760.7	0.18	15.03	2851.01	262.61	0.11	>1
2	45	23	-8029.26	0.11	23.88	2851.01	262.61	0.11	>1
1	47	24	-12427.7	0.17	--	2446.75	191.19	0.09	--
2	47	24	-8362.28	0.12	--	2446.75	191.19	0.09	--
1	49	25	-9127.45	0.13	21.01	2400.47	1857.05	0.11	>1
2	49	25	-11662.6	0.16	16.44	2400.47	1857.05	0.11	>1
1	51	26	-9304.97	0.13	--	2090.43	1630.62	0.09	--
2	51	26	-11485	0.16	--	2090.43	1630.62	0.09	--
1	53	27	-10780.3	0.15	17.79	1906.69	1849.77	0.09	>1
2	53	27	-10009.7	0.14	19.16	1906.69	1849.77	0.09	>1
1	55	28	-10725.6	0.15	--	1672.11	1624.37	0.08	--
2	55	28	-10064.4	0.14	--	1672.11	1624.37	0.08	--
1	57	29	-9207.55	0.13	20.83	1983.45	1379.72	0.09	>1
2	57	29	-11582.4	0.16	16.56	1983.45	1379.72	0.09	>1
1	59	30	-9373.82	0.13	--	1681.42	1151.32	0.07	--
2	59	30	-11416.2	0.16	--	1681.42	1151.32	0.07	--

Relazione geotecnica

1	61	31	-10860.4	0.15	17.66	1495.22	1386.99	0.07	>1
2	61	31	-9929.57	0.14	19.31	1495.22	1386.99	0.07	>1
1	63	32	-10794.4	0.15	--	1252.89	1157.57	0.06	--
2	63	32	-9995.56	0.14	--	1252.89	1157.57	0.06	--
1	65	33	-9188.34	0.13	20.87	768.52	701.44	0.04	>1
2	65	33	-9711.67	0.13	19.75	768.52	701.44	0.04	>1
1	67	34	-9597.62	0.13	19.98	721.72	699.64	0.03	>1
2	67	34	-9302.38	0.13	20.61	721.72	699.64	0.03	>1
1	69	35	-9390	0.13	20.42	823.92	820.76	0.04	>1
2	69	35	-9510	0.13	20.16	823.92	820.76	0.04	>1
1	71	36	-9395.96	0.13	20.41	583.93	580.32	0.03	>1
2	71	36	-9504.05	0.13	20.18	583.93	580.32	0.03	>1
1	73	37	-9209.78	0.13	--	555.17	474.47	0.03	--
2	73	37	-9690.22	0.13	--	555.17	474.47	0.03	--
1	75	38	-9619.07	0.13	--	514.37	472.67	0.02	--
2	75	38	-9280.93	0.13	--	514.37	472.67	0.02	--
1	77	39	-9411.45	0.13	--	595.59	593.79	0.03	--
2	77	39	-9488.55	0.13	--	595.59	593.79	0.03	--
1	79	40	-9417.4	0.13	--	355.5	353.35	0.02	--
2	79	40	-9482.6	0.13	--	355.5	353.35	0.02	--
1	81	41	-9232.46	0.13	--	394.46	295.73	0.02	--
2	81	41	-9667.54	0.13	--	394.46	295.73	0.02	--
1	83	42	-9641.75	0.13	--	373.28	293.93	0.02	--
2	83	42	-9258.25	0.13	--	373.28	293.93	0.02	--
1	85	43	-9434.13	0.13	--	415.49	415.05	0.02	--
2	85	43	-9465.87	0.13	--	415.49	415.05	0.02	--
1	87	44	-9440.08	0.13	--	175.01	174.61	0.01	--
2	87	44	-9459.92	0.13	--	175.01	174.61	0.01	--
1	89	45	-9241.54	0.13	--	335.94	224.23	0.01	--
2	89	45	-9658.46	0.13	--	335.94	224.23	0.01	--
1	91	46	-9650.82	0.13	--	327.95	222.43	0.01	--
2	91	46	-9249.18	0.13	--	327.95	222.43	0.01	--
1	93	47	-9443.21	0.13	--	343.65	343.56	0.02	--
2	93	47	-9456.8	0.13	--	343.65	343.56	0.02	--
1	95	48	-9449.16	0.13	--	103.11	103.11	0	--
2	95	48	-9450.85	0.13	--	103.11	103.11	0	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-8020.85	0.11	25.05	2947.05	753.94	0.12	>1
2	2	1	-12769.1	0.18	15.73	2947.05	753.94	0.12	>1
1	4	2	-8353.87	0.12	--	2542.67	682.52	0.1	--
2	4	2	-12436.1	0.17	--	2542.67	682.52	0.1	--
1	6	3	-8044.88	0.11	24.97	2828.48	217.09	0.11	>1
2	6	3	-12745.1	0.18	15.76	2828.48	217.09	0.11	>1
1	8	4	-8374.53	0.12	--	2429.33	152.06	0.09	--
2	8	4	-12415.5	0.17	--	2429.33	152.06	0.09	--
1	10	5	-13530.4	0.19	14.85	3832.62	729.69	0.15	>1
2	10	5	-7259.57	0.1	27.67	3832.62	729.69	0.15	>1
1	12	6	-13089.3	0.18	--	3300.12	661.68	0.13	--
2	12	6	-7700.75	0.11	--	3300.12	661.68	0.13	--
1	14	7	-13554.5	0.19	14.82	3799.03	241.34	0.14	>1
2	14	7	-7235.54	0.1	27.77	3799.03	241.34	0.14	>1
1	16	8	-13109.9	0.18	--	3262.48	172.91	0.12	--
2	16	8	-7680.09	0.11	--	3262.48	172.91	0.12	--
1	18	9	-9921.17	0.14	20.25	1962.5	1878.32	0.09	>1
2	18	9	-10868.8	0.15	18.48	1962.5	1878.32	0.09	>1
1	20	10	-9987.16	0.14	--	1720	1648.9	0.08	--
2	20	10	-10802.8	0.15	--	1720	1648.9	0.08	--
1	22	11	-11574	0.16	17.36	2345.77	1871.05	0.1	>1
2	22	11	-9215.96	0.13	21.8	2345.77	1871.05	0.1	>1
1	24	12	-11407.8	0.16	--	2043.36	1642.65	0.09	--
2	24	12	-9382.23	0.13	--	2043.36	1642.65	0.09	--
1	26	13	-10001.3	0.14	20.09	1438.26	1358.44	0.07	>1
2	26	13	-10788.7	0.15	18.62	1438.26	1358.44	0.07	>1
1	28	14	-10056	0.14	--	1203.85	1133.04	0.06	--
2	28	14	-10734	0.15	--	1203.85	1133.04	0.06	--
1	30	15	-11654.2	0.16	17.24	2036.72	1365.72	0.09	>1
2	30	15	-9135.85	0.13	21.99	2036.72	1365.72	0.09	>1
1	32	16	-11476.6	0.16	--	1727.04	1139.29	0.07	--
2	32	16	-9313.38	0.13	--	1727.04	1139.29	0.07	--
1	34	17	-7227.13	0.1	27.8	3871.41	732.67	0.15	>1
2	34	17	-13562.9	0.19	14.81	3871.41	732.67	0.15	>1
1	36	18	-7671.68	0.11	--	3334.8	664.24	0.13	--
2	36	18	-13118.3	0.18	--	3334.8	664.24	0.13	--
1	38	19	-7251.16	0.1	27.71	3780.13	238.36	0.14	>1

Relazione geotecnica

2	38	19	-13538.8	0.19	14.84	3780.13	238.36	0.14	>1
1	40	20	-7692.34	0.11	--	3247.66	170.34	0.12	--
2	40	20	-13097.7	0.18	--	3247.66	170.34	0.12	--
1	42	21	-12736.7	0.18	15.77	2897.97	708.42	0.11	>1
2	42	21	-8053.29	0.11	24.95	2897.97	708.42	0.11	>1
1	44	22	-12407.1	0.17	--	2498.73	643.39	0.1	--
2	44	22	-8382.93	0.12	--	2498.73	643.39	0.1	--
1	46	23	-12760.7	0.18	15.74	2851.01	262.61	0.11	>1
2	46	23	-8029.26	0.11	25.02	2851.01	262.61	0.11	>1
1	48	24	-12427.7	0.17	--	2446.75	191.19	0.09	--
2	48	24	-8362.28	0.12	--	2446.75	191.19	0.09	--
1	50	25	-9127.45	0.13	22.01	2400.47	1857.05	0.11	>1
2	50	25	-11662.6	0.16	17.23	2400.47	1857.05	0.11	>1
1	52	26	-9304.97	0.13	--	2090.43	1630.62	0.09	--
2	52	26	-11485	0.16	--	2090.43	1630.62	0.09	--
1	54	27	-10780.3	0.15	18.64	1906.69	1849.77	0.09	>1
2	54	27	-10009.7	0.14	20.07	1906.69	1849.77	0.09	>1
1	56	28	-10725.6	0.15	--	1672.11	1624.37	0.08	--
2	56	28	-10064.4	0.14	--	1672.11	1624.37	0.08	--
1	58	29	-9207.55	0.13	21.82	1983.45	1379.72	0.09	>1
2	58	29	-11582.4	0.16	17.35	1983.45	1379.72	0.09	>1
1	60	30	-9373.82	0.13	--	1681.42	1151.32	0.07	--
2	60	30	-11416.2	0.16	--	1681.42	1151.32	0.07	--
1	62	31	-10860.4	0.15	18.5	1495.22	1386.99	0.07	>1
2	62	31	-9929.57	0.14	20.23	1495.22	1386.99	0.07	>1
1	64	32	-10794.4	0.15	--	1252.89	1157.57	0.06	--
2	64	32	-9995.56	0.14	--	1252.89	1157.57	0.06	--
1	66	33	-9188.34	0.13	21.86	768.52	701.44	0.04	>1
2	66	33	-9711.67	0.13	20.69	768.52	701.44	0.04	>1
1	68	34	-9597.62	0.13	20.93	721.72	699.64	0.03	>1
2	68	34	-9302.38	0.13	21.6	721.72	699.64	0.03	>1
1	70	35	-9390	0.13	21.4	823.92	820.76	0.04	>1
2	70	35	-9510	0.13	21.13	823.92	820.76	0.04	>1
1	72	36	-9395.96	0.13	21.38	583.93	580.32	0.03	>1
2	72	36	-9504.05	0.13	21.14	583.93	580.32	0.03	>1
1	74	37	-9209.78	0.13	--	555.17	474.47	0.03	--
2	74	37	-9690.22	0.13	--	555.17	474.47	0.03	--
1	76	38	-9619.07	0.13	--	514.37	472.67	0.02	--
2	76	38	-9280.93	0.13	--	514.37	472.67	0.02	--
1	78	39	-9411.45	0.13	--	595.59	593.79	0.03	--
2	78	39	-9488.55	0.13	--	595.59	593.79	0.03	--
1	80	40	-9417.4	0.13	--	355.5	353.35	0.02	--
2	80	40	-9482.6	0.13	--	355.5	353.35	0.02	--
1	82	41	-9232.46	0.13	--	394.46	295.73	0.02	--
2	82	41	-9667.54	0.13	--	394.46	295.73	0.02	--
1	84	42	-9641.75	0.13	--	373.28	293.93	0.02	--
2	84	42	-9258.25	0.13	--	373.28	293.93	0.02	--
1	86	43	-9434.13	0.13	--	415.49	415.05	0.02	--
2	86	43	-9465.87	0.13	--	415.49	415.05	0.02	--
1	88	44	-9440.08	0.13	--	175.01	174.61	0.01	--
2	88	44	-9459.92	0.13	--	175.01	174.61	0.01	--
1	90	45	-9241.54	0.13	--	335.94	224.23	0.01	--
2	90	45	-9658.46	0.13	--	335.94	224.23	0.01	--
1	92	46	-9650.82	0.13	--	327.95	222.43	0.01	--
2	92	46	-9249.18	0.13	--	327.95	222.43	0.01	--
1	94	47	-9443.21	0.13	--	343.65	343.56	0.02	--
2	94	47	-9456.8	0.13	--	343.65	343.56	0.02	--
1	96	48	-9449.16	0.13	--	103.11	103.11	0	--
2	96	48	-9450.85	0.13	--	103.11	103.11	0	--

Plinto n. 19

Tipo palo=Trivellato
 Rotazione testa libera
 Coefficiente di efficienza=1.00
 Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>
 Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	-1.2	0
2	1.2	0

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88

Relazione geotecnica

17	1.01	0.17	22.05	1.88
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$Q_{S_{lim}}=252333.00$ <daN>
 $q_p=28.63$ <daN/cm²>
 $Q_{P_{lim}}=143893.00$ <daN>
 $k_p=1.42$ <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

$Q_{S_{lim}}=321694.00$ <daN>
 $q_p=16.60$ <daN/cm²>
 $Q_{P_{lim}}=83431.40$ <daN>
 $k_p=1.42$ <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-7196.47	0.1	26.65	3938.15	881.46	0.15	>1
2	1	1	-13593.5	0.19	14.11	3938.15	881.46	0.15	>1
1	3	2	-7521.42	0.1	--	3539.51	798.37	0.14	--
2	3	2	-13268.6	0.18	--	3539.51	798.37	0.14	--
1	5	3	-7256.18	0.1	26.43	3768.1	106.6	0.14	>1
2	5	3	-13533.8	0.19	14.17	3768.1	106.6	0.14	>1
1	7	4	-7572.74	0.1	--	3387.1	50.84	0.12	--
2	7	4	-13217.3	0.18	--	3387.1	50.84	0.12	--
1	9	5	-12506.4	0.17	15.33	2691.22	907.35	0.11	>1
2	9	5	-8283.62	0.11	23.15	2691.22	907.35	0.11	>1
1	11	6	-12085.2	0.17	--	2187.95	820.63	0.09	--
2	11	6	-8704.81	0.12	--	2187.95	820.63	0.09	--
1	13	7	-12566.1	0.17	15.26	2606.55	80.71	0.1	>1
2	13	7	-8223.92	0.11	23.32	2606.55	80.71	0.1	>1
1	15	8	-12136.5	0.17	--	2090	28.59	0.08	--
2	15	8	-8653.5	0.12	--	2090	28.59	0.08	--
1	17	9	-8985.29	0.12	21.34	2652.65	2043.25	0.12	>1
2	17	9	-11804.7	0.16	16.25	2652.65	2043.25	0.12	>1
1	19	10	-9058.88	0.12	--	2408.24	1796.92	0.11	--
2	19	10	-11731.1	0.16	--	2408.24	1796.92	0.11	--
1	21	11	-10578.3	0.15	18.13	2062.78	2051.02	0.1	>1
2	21	11	-10211.7	0.14	18.78	2062.78	2051.02	0.1	>1
1	23	12	-10428	0.14	--	1804.03	1803.59	0.08	--
2	23	12	-10362	0.14	--	1804.03	1803.59	0.08	--
1	25	13	-9184.3	0.13	20.88	1916.75	1250.27	0.08	>1
2	25	13	-11605.7	0.16	16.52	1916.75	1250.27	0.08	>1
1	27	14	-9229.92	0.13	--	1738.8	1033.81	0.07	--
2	27	14	-11560.1	0.16	--	1738.8	1033.81	0.07	--
1	29	15	-10777.3	0.15	17.79	1324.48	1242.5	0.06	>1
2	29	15	-10012.7	0.14	19.15	1324.48	1242.5	0.06	>1
1	31	16	-10599	0.15	--	1055.91	1027.13	0.05	--
2	31	16	-10191	0.14	--	1055.91	1027.13	0.05	--
1	33	17	-6451.86	0.09	29.72	4777.73	661.11	0.18	>1
2	33	17	-14338.1	0.2	13.37	4777.73	661.11	0.18	>1
1	35	18	-6881.44	0.09	--	4260.03	608.99	0.16	--
2	35	18	-13908.6	0.19	--	4260.03	608.99	0.16	--
1	37	19	-6511.56	0.09	29.45	4671.58	326.95	0.17	>1
2	37	19	-14278.4	0.2	13.43	4671.58	326.95	0.17	>1
1	39	20	-6932.75	0.1	--	4161.63	240.22	0.15	--
2	39	20	-13857.2	0.19	--	4161.63	240.22	0.15	--
1	41	21	-11761.8	0.16	16.3	1778.19	687.01	0.07	>1
2	41	21	-9028.24	0.12	21.24	1778.19	687.01	0.07	>1
1	43	22	-11445.2	0.16	--	1409.5	631.25	0.06	--
2	43	22	-9344.79	0.13	--	1409.5	631.25	0.06	--
1	45	23	-11821.5	0.16	16.22	1738.03	301.05	0.07	>1
2	45	23	-8968.53	0.12	21.38	1738.03	301.05	0.07	>1
1	47	24	-11496.5	0.16	--	1339.67	217.97	0.05	--
2	47	24	-9293.48	0.13	--	1339.67	217.97	0.05	--
1	49	25	-8240.67	0.11	23.27	3163.26	1822.91	0.13	>1
2	49	25	-12549.3	0.17	15.28	3163.26	1822.91	0.13	>1
1	51	26	-8418.89	0.12	--	2864.85	1607.53	0.12	--
2	51	26	-12371.1	0.17	--	2864.85	1607.53	0.12	--
1	53	27	-9833.65	0.14	19.5	1950.68	1830.68	0.09	>1
2	53	27	-10956.4	0.15	17.5	1950.68	1830.68	0.09	>1
1	55	28	-9788.02	0.13	--	1770.93	1614.21	0.08	--
2	55	28	-11002	0.15	--	1770.93	1614.21	0.08	--

Relazione geotecnica

1	57	29	-8439.68	0.12	22.72	2769.15	1470.61	0.12	>1
2	57	29	-12350.3	0.17	15.53	2769.15	1470.61	0.12	>1
1	59	30	-8589.94	0.12	--	2487.58	1223.19	0.1	--
2	59	30	-12200.1	0.17	--	2487.58	1223.19	0.1	--
1	61	31	-10032.7	0.14	19.11	1526.1	1462.85	0.07	>1
2	61	31	-10757.3	0.15	17.83	1526.1	1462.85	0.07	>1
1	63	32	-9959.07	0.14	--	1324.22	1216.51	0.06	--
2	63	32	-10830.9	0.15	--	1324.22	1216.51	0.06	--
1	65	33	-7618.21	0.11	25.17	2332.29	779.55	0.09	>1
2	65	33	-11281.8	0.16	17	2332.29	779.55	0.09	>1
1	67	34	-8012.66	0.11	23.93	1893.59	781.48	0.08	>1
2	67	34	-10887.3	0.15	17.61	1893.59	781.48	0.08	>1
1	69	35	-7808.04	0.11	24.56	2167.35	902.84	0.09	>1
2	69	35	-11092	0.15	17.29	2167.35	902.84	0.09	>1
1	71	36	-7822.83	0.11	24.51	2060.55	658.18	0.08	>1
2	71	36	-11077.2	0.15	17.31	2060.55	658.18	0.08	>1
1	73	37	-8088.94	0.11	--	1717.04	529.77	0.07	--
2	73	37	-10811.1	0.15	--	1717.04	529.77	0.07	--
1	75	38	-8483.39	0.12	--	1275.98	531.7	0.05	--
2	75	38	-10416.6	0.14	--	1275.98	531.7	0.05	--
1	77	39	-8278.78	0.11	--	1549.79	653.06	0.06	--
2	77	39	-10621.2	0.15	--	1549.79	653.06	0.06	--
1	79	40	-8293.56	0.11	--	1446.58	408.4	0.06	--
2	79	40	-10606.4	0.15	--	1446.58	408.4	0.06	--
1	81	41	-8344.91	0.12	--	1368.79	339.12	0.05	--
2	81	41	-10555.1	0.15	--	1368.79	339.12	0.05	--
1	83	42	-8739.36	0.12	--	918.44	341.04	0.04	--
2	83	42	-10160.6	0.14	--	918.44	341.04	0.04	--
1	85	43	-8534.74	0.12	--	1191.68	462.41	0.05	--
2	85	43	-10365.3	0.14	--	1191.68	462.41	0.05	--
1	87	44	-8549.53	0.12	--	1102.29	217.75	0.04	--
2	87	44	-10350.5	0.14	--	1102.29	217.75	0.04	--
1	89	45	-8447.29	0.12	--	1231.63	262.86	0.05	--
2	89	45	-10452.7	0.14	--	1231.63	262.86	0.05	--
1	91	46	-8841.75	0.12	--	776.45	264.78	0.03	--
2	91	46	-10058.3	0.14	--	776.45	264.78	0.03	--
1	93	47	-8637.13	0.12	--	1049.1	386.15	0.04	--
2	93	47	-10262.9	0.14	--	1049.1	386.15	0.04	--
1	95	48	-8651.91	0.12	--	968.1	141.49	0.04	--
2	95	48	-10248.1	0.14	--	968.1	141.49	0.04	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-7196.47	0.1	27.92	3938.15	881.46	0.15	>1
2	2	1	-13593.5	0.19	14.78	3938.15	881.46	0.15	>1
1	4	2	-7521.42	0.1	--	3539.51	798.37	0.14	--
2	4	2	-13268.6	0.18	--	3539.51	798.37	0.14	--
1	6	3	-7256.18	0.1	27.69	3768.1	106.6	0.14	>1
2	6	3	-13533.8	0.19	14.84	3768.1	106.6	0.14	>1
1	8	4	-7572.74	0.1	--	3387.1	50.84	0.12	--
2	8	4	-13217.3	0.18	--	3387.1	50.84	0.12	--
1	10	5	-12506.4	0.17	16.06	2691.22	907.35	0.11	>1
2	10	5	-8283.62	0.11	24.25	2691.22	907.35	0.11	>1
1	12	6	-12085.2	0.17	--	2187.95	820.63	0.09	--
2	12	6	-8704.81	0.12	--	2187.95	820.63	0.09	--
1	14	7	-12566.1	0.17	15.99	2606.55	80.71	0.1	>1
2	14	7	-8223.92	0.11	24.43	2606.55	80.71	0.1	>1
1	16	8	-12136.5	0.17	--	2090	28.59	0.08	--
2	16	8	-8653.5	0.12	--	2090	28.59	0.08	--
1	18	9	-8985.29	0.12	22.36	2652.65	2043.25	0.12	>1
2	18	9	-11804.7	0.16	17.02	2652.65	2043.25	0.12	>1
1	20	10	-9058.88	0.12	--	2408.24	1796.92	0.11	--
2	20	10	-11731.1	0.16	--	2408.24	1796.92	0.11	--
1	22	11	-10578.3	0.15	18.99	2062.78	2051.02	0.1	>1
2	22	11	-10211.7	0.14	19.67	2062.78	2051.02	0.1	>1
1	24	12	-10428	0.14	--	1804.03	1803.59	0.08	--
2	24	12	-10362	0.14	--	1804.03	1803.59	0.08	--
1	26	13	-9184.3	0.13	21.87	1916.75	1250.27	0.08	>1
2	26	13	-11605.7	0.16	17.31	1916.75	1250.27	0.08	>1
1	28	14	-9229.92	0.13	--	1738.8	1033.81	0.07	--
2	28	14	-11560.1	0.16	--	1738.8	1033.81	0.07	--
1	30	15	-10777.3	0.15	18.64	1324.48	1242.5	0.06	>1
2	30	15	-10012.7	0.14	20.06	1324.48	1242.5	0.06	>1
1	32	16	-10599	0.15	--	1055.91	1027.13	0.05	--
2	32	16	-10191	0.14	--	1055.91	1027.13	0.05	--
1	34	17	-6451.86	0.09	31.14	4777.73	661.11	0.18	>1

Relazione geotecnica

2	34	17	-14338.1	0.2	14.01	4777.73	661.11	0.18	>1
1	36	18	-6881.44	0.09	--	4260.03	608.99	0.16	--
2	36	18	-13908.6	0.19	--	4260.03	608.99	0.16	--
1	38	19	-6511.56	0.09	30.85	4671.58	326.95	0.17	>1
2	38	19	-14278.4	0.2	14.07	4671.58	326.95	0.17	>1
1	40	20	-6932.75	0.1	--	4161.63	240.22	0.15	--
2	40	20	-13857.2	0.19	--	4161.63	240.22	0.15	--
1	42	21	-11761.8	0.16	17.08	1778.19	687.01	0.07	>1
2	42	21	-9028.24	0.12	22.25	1778.19	687.01	0.07	>1
1	44	22	-11445.2	0.16	--	1409.5	631.25	0.06	--
2	44	22	-9344.79	0.13	--	1409.5	631.25	0.06	--
1	46	23	-11821.5	0.16	16.99	1738.03	301.05	0.07	>1
2	46	23	-8968.53	0.12	22.4	1738.03	301.05	0.07	>1
1	48	24	-11496.5	0.16	--	1339.67	217.97	0.05	--
2	48	24	-9293.48	0.13	--	1339.67	217.97	0.05	--
1	50	25	-8240.67	0.11	24.38	3163.26	1822.91	0.13	>1
2	50	25	-12549.3	0.17	16.01	3163.26	1822.91	0.13	>1
1	52	26	-8418.89	0.12	--	2864.85	1607.53	0.12	--
2	52	26	-12371.1	0.17	--	2864.85	1607.53	0.12	--
1	54	27	-9833.65	0.14	20.43	1950.68	1830.68	0.09	>1
2	54	27	-10956.4	0.15	18.34	1950.68	1830.68	0.09	>1
1	56	28	-9788.02	0.13	--	1770.93	1614.21	0.08	--
2	56	28	-11002	0.15	--	1770.93	1614.21	0.08	--
1	58	29	-8439.68	0.12	23.8	2769.15	1470.61	0.12	>1
2	58	29	-12350.3	0.17	16.27	2769.15	1470.61	0.12	>1
1	60	30	-8589.94	0.12	--	2487.58	1223.19	0.1	--
2	60	30	-12200.1	0.17	--	2487.58	1223.19	0.1	--
1	62	31	-10032.7	0.14	20.02	1526.1	1462.85	0.07	>1
2	62	31	-10757.3	0.15	18.68	1526.1	1462.85	0.07	>1
1	64	32	-9959.07	0.14	--	1324.22	1216.51	0.06	--
2	64	32	-10830.9	0.15	--	1324.22	1216.51	0.06	--
1	66	33	-7618.21	0.11	26.37	2332.29	779.55	0.09	>1
2	66	33	-11281.8	0.16	17.81	2332.29	779.55	0.09	>1
1	68	34	-8012.66	0.11	25.07	1893.59	781.48	0.08	>1
2	68	34	-10887.3	0.15	18.45	1893.59	781.48	0.08	>1
1	70	35	-7808.04	0.11	25.73	2167.35	902.84	0.09	>1
2	70	35	-11092	0.15	18.11	2167.35	902.84	0.09	>1
1	72	36	-7822.83	0.11	25.68	2060.55	658.18	0.08	>1
2	72	36	-11077.2	0.15	18.14	2060.55	658.18	0.08	>1
1	74	37	-8088.94	0.11	--	1717.04	529.77	0.07	--
2	74	37	-10811.1	0.15	--	1717.04	529.77	0.07	--
1	76	38	-8483.39	0.12	--	1275.98	531.7	0.05	--
2	76	38	-10416.6	0.14	--	1275.98	531.7	0.05	--
1	78	39	-8278.78	0.11	--	1549.79	653.06	0.06	--
2	78	39	-10621.2	0.15	--	1549.79	653.06	0.06	--
1	80	40	-8293.56	0.11	--	1446.58	408.4	0.06	--
2	80	40	-10606.4	0.15	--	1446.58	408.4	0.06	--
1	82	41	-8344.91	0.12	--	1368.79	339.12	0.05	--
2	82	41	-10555.1	0.15	--	1368.79	339.12	0.05	--
1	84	42	-8739.36	0.12	--	918.44	341.04	0.04	--
2	84	42	-10160.6	0.14	--	918.44	341.04	0.04	--
1	86	43	-8534.74	0.12	--	1191.68	462.41	0.05	--
2	86	43	-10365.3	0.14	--	1191.68	462.41	0.05	--
1	88	44	-8549.53	0.12	--	1102.29	217.75	0.04	--
2	88	44	-10350.5	0.14	--	1102.29	217.75	0.04	--
1	90	45	-8447.29	0.12	--	1231.63	262.86	0.05	--
2	90	45	-10452.7	0.14	--	1231.63	262.86	0.05	--
1	92	46	-8841.75	0.12	--	776.45	264.78	0.03	--
2	92	46	-10058.3	0.14	--	776.45	264.78	0.03	--
1	94	47	-8637.13	0.12	--	1049.1	386.15	0.04	--
2	94	47	-10262.9	0.14	--	1049.1	386.15	0.04	--
1	96	48	-8651.91	0.12	--	968.1	141.49	0.04	--
2	96	48	-10248.1	0.14	--	968.1	141.49	0.04	--

Plinto n. 20

Tipo palo=Trivellato
 Rotazione testa libera
 Coefficiente di efficienza=1.00
 Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>
 Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	-1.2	0
2	1.2	0

Verifiche in condizioni drenate

z_p <m>	τ_s <daN/cm²>	k_s <daN/cm²>	σ_h <daN/cm²>	k_h <daN/cm²>
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

Q_{S1im}=252333.00 <daN>
q_p=28.63 <daN/cm²>
Q_{P1im}=143893.00 <daN>
k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

z_p <m>	τ_s <daN/cm²>	k_s <daN/cm²>	σ_h <daN/cm²>	k_h <daN/cm²>
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

Q_{S1im}=321694.00 <daN>
q_p=16.60 <daN/cm²>
Q_{P1im}=83431.40 <daN>
k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-6945.02	0.1	27.61	4212.83	780.05	0.16	>1
2	1	1	-13845	0.19	13.85	4212.83	780.05	0.16	>1
1	3	2	-7198.86	0.1	--	3897.92	695.52	0.15	--
2	3	2	-13591.1	0.19	--	3897.92	695.52	0.15	--
1	5	3	-6835.91	0.09	28.05	4278.13	248.37	0.16	>1
2	5	3	-13954.1	0.19	13.74	4278.13	248.37	0.16	>1
1	7	4	-7105.08	0.1	--	3952.4	188.39	0.15	--
2	7	4	-13684.9	0.19	--	3952.4	188.39	0.15	--
1	9	5	-11351	0.16	16.89	1580.45	1087.1	0.07	>1
2	9	5	-9439.01	0.13	20.32	1580.45	1087.1	0.07	>1
1	11	6	-10985.7	0.15	--	1192.87	959.41	0.05	--
2	11	6	-9804.29	0.14	--	1192.87	959.41	0.05	--
1	13	7	-11241.9	0.15	17.06	1017.95	58.67	0.04	>1
2	13	7	-9548.12	0.13	20.08	1017.95	58.67	0.04	>1
1	15	8	-10891.9	0.15	--	601.08	75.5	0.02	--
2	15	8	-9898.07	0.14	--	601.08	75.5	0.02	--
1	17	9	-8614.4	0.12	22.26	2987.07	2087.35	0.13	>1
2	17	9	-12175.6	0.17	15.75	2987.07	2087.35	0.13	>1
1	19	10	-8633.66	0.12	--	2788.64	1819.11	0.12	--
2	19	10	-12156.3	0.17	--	2788.64	1819.11	0.12	--
1	21	11	-9936.2	0.14	19.3	2247.92	2179.46	0.1	>1
2	21	11	-10853.8	0.15	17.67	2247.92	2179.46	0.1	>1
1	23	12	-9769.72	0.13	--	2041.19	1898.28	0.09	--
2	23	12	-11020.3	0.15	--	2041.19	1898.28	0.09	--
1	25	13	-8250.7	0.11	23.24	2901.5	1340.73	0.12	>1
2	25	13	-12539.3	0.17	15.29	2901.5	1340.73	0.12	>1
1	27	14	-8321.07	0.11	--	2732.11	1127.26	0.11	--
2	27	14	-12468.9	0.17	--	2732.11	1127.26	0.11	--
1	29	15	-9572.5	0.13	20.03	1591.61	1248.62	0.07	>1
2	29	15	-11217.5	0.15	17.1	1591.61	1248.62	0.07	>1
1	31	16	-9457.13	0.13	--	1537.9	1048.09	0.07	--
2	31	16	-11332.9	0.16	--	1537.9	1048.09	0.07	--
1	33	17	-6261.05	0.09	30.63	4969.69	298.22	0.18	>1
2	33	17	-14528.9	0.2	13.2	4969.69	298.22	0.18	>1
1	35	18	-6611	0.09	--	4549.51	281.39	0.17	--
2	35	18	-14179	0.2	--	4549.51	281.39	0.17	--
1	37	19	-6151.94	0.08	31.17	5143.76	730.2	0.2	>1
2	37	19	-14638.1	0.2	13.1	5143.76	730.2	0.2	>1
1	39	20	-6517.22	0.09	--	4692.18	602.52	0.18	--
2	39	20	-14272.8	0.2	--	4692.18	602.52	0.18	--
1	41	21	-10667	0.15	17.98	687.68	605.26	0.03	>1
2	41	21	-10123	0.14	18.94	687.68	605.26	0.03	>1
1	43	22	-10397.9	0.14	--	545.3	545.29	0.03	--
2	43	22	-10392.1	0.14	--	545.3	545.29	0.03	--
1	45	23	-10557.9	0.15	18.16	466.14	423.16	0.02	>1
2	45	23	-10232.1	0.14	18.74	466.14	423.16	0.02	>1
1	47	24	-10304.1	0.14	--	355.77	338.62	0.02	--
2	47	24	-10485.9	0.14	--	355.77	338.62	0.02	--
1	49	25	-7930.44	0.11	24.18	3365.16	1605.51	0.14	>1
2	49	25	-12859.6	0.18	14.91	3365.16	1605.51	0.14	>1
1	51	26	-8045.81	0.11	--	3149.75	1404.98	0.13	--
2	51	26	-12744.2	0.18	--	3149.75	1404.98	0.13	--

1	53	27	-9252.23	0.13	20.73	2182.31	1697.63	0.1	>1
2	53	27	-11537.8	0.16	16.62	2182.31	1697.63	0.1	>1
1	55	28	-9181.86	0.13	--	2078.93	1484.15	0.09	--
2	55	28	-11608.1	0.16	--	2078.93	1484.15	0.09	--
1	57	29	-7566.74	0.1	25.34	3852.32	1822.56	0.16	>1
2	57	29	-13223.3	0.18	14.5	3852.32	1822.56	0.16	>1
1	59	30	-7733.21	0.11	--	3546.61	1541.38	0.15	--
2	59	30	-13056.8	0.18	--	3546.61	1541.38	0.15	--
1	61	31	-8888.53	0.12	21.57	2502.49	1730.45	0.11	>1
2	61	31	-11901.5	0.16	16.11	2502.49	1730.45	0.11	>1
1	63	32	-8869.27	0.12	--	2343.12	1462.22	0.1	--
2	63	32	-11920.7	0.16	--	2343.12	1462.22	0.1	--
1	65	33	-6353.65	0.09	30.18	3750.54	510.63	0.14	>1
2	65	33	-12546.4	0.17	15.28	3750.54	510.63	0.14	>1
1	67	34	-6680.95	0.09	28.7	3365.41	533.44	0.13	>1
2	67	34	-12219.1	0.17	15.69	3365.41	533.44	0.13	>1
1	69	35	-6530.81	0.09	29.36	3562.71	649.36	0.14	>1
2	69	35	-12369.2	0.17	15.5	3562.71	649.36	0.14	>1
1	71	36	-6503.79	0.09	29.49	3557.42	394.7	0.13	>1
2	71	36	-12396.2	0.17	15.47	3557.42	394.7	0.13	>1
1	73	37	-7188.1	0.1	--	2735.57	340.62	0.1	--
2	73	37	-11711.9	0.16	--	2735.57	340.62	0.1	--
1	75	38	-7515.4	0.1	--	2349.8	363.43	0.09	--
2	75	38	-11384.6	0.16	--	2349.8	363.43	0.09	--
1	77	39	-7365.26	0.1	--	2547.2	479.36	0.1	--
2	77	39	-11534.7	0.16	--	2547.2	479.36	0.1	--
1	79	40	-7338.24	0.1	--	2544.06	224.7	0.1	--
2	79	40	-11561.8	0.16	--	2544.06	224.7	0.1	--
1	81	41	-7619.62	0.11	--	2206.01	205.05	0.08	--
2	81	41	-11280.4	0.16	--	2206.01	205.05	0.08	--
1	83	42	-7946.92	0.11	--	1818.03	227.86	0.07	--
2	83	42	-10953.1	0.15	--	1818.03	227.86	0.07	--
1	85	43	-7796.78	0.11	--	2013.43	343.78	0.08	--
2	85	43	-11103.2	0.15	--	2013.43	343.78	0.08	--
1	87	44	-7769.76	0.11	--	2018.26	89.13	0.07	--
2	87	44	-11130.2	0.15	--	2018.26	89.13	0.07	--
1	89	45	-7792.23	0.11	--	1995.04	150.82	0.07	--
2	89	45	-11107.8	0.15	--	1995.04	150.82	0.07	--
1	91	46	-8119.53	0.11	--	1605.98	173.63	0.06	--
2	91	46	-10780.5	0.15	--	1605.98	173.63	0.06	--
1	93	47	-7969.39	0.11	--	1800.18	289.55	0.07	--
2	93	47	-10930.6	0.15	--	1800.18	289.55	0.07	--
1	95	48	-7942.37	0.11	--	1809.49	34.9	0.07	--
2	95	48	-10957.6	0.15	--	1809.49	34.9	0.07	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-6945.02	0.1	28.93	4212.83	780.05	0.16	>1
2	2	1	-13845	0.19	14.51	4212.83	780.05	0.16	>1
1	4	2	-7198.86	0.1	--	3897.92	695.52	0.15	--
2	4	2	-13591.1	0.19	--	3897.92	695.52	0.15	--
1	6	3	-6835.91	0.09	29.39	4278.13	248.37	0.16	>1
2	6	3	-13954.1	0.19	14.4	4278.13	248.37	0.16	>1
1	8	4	-7105.08	0.1	--	3952.4	188.39	0.15	--
2	8	4	-13684.9	0.19	--	3952.4	188.39	0.15	--
1	10	5	-11351	0.16	17.7	1580.45	1087.1	0.07	>1
2	10	5	-9439.01	0.13	21.28	1580.45	1087.1	0.07	>1
1	12	6	-10985.7	0.15	--	1192.87	959.41	0.05	--
2	12	6	-9804.29	0.14	--	1192.87	959.41	0.05	--
1	14	7	-11241.9	0.15	17.87	1017.95	58.67	0.04	>1
2	14	7	-9548.12	0.13	21.04	1017.95	58.67	0.04	>1
1	16	8	-10891.9	0.15	--	601.08	75.5	0.02	--
2	16	8	-9898.07	0.14	--	601.08	75.5	0.02	--
1	18	9	-8614.4	0.12	23.32	2987.07	2087.35	0.13	>1
2	18	9	-12175.6	0.17	16.5	2987.07	2087.35	0.13	>1
1	20	10	-8633.66	0.12	--	2788.64	1819.11	0.12	--
2	20	10	-12156.3	0.17	--	2788.64	1819.11	0.12	--
1	22	11	-9936.2	0.14	20.22	2247.92	2179.46	0.1	>1
2	22	11	-10853.8	0.15	18.51	2247.92	2179.46	0.1	>1
1	24	12	-9769.72	0.13	--	2041.19	1898.28	0.09	--
2	24	12	-11020.3	0.15	--	2041.19	1898.28	0.09	--
1	26	13	-8250.7	0.11	24.35	2901.5	1340.73	0.12	>1
2	26	13	-12539.3	0.17	16.02	2901.5	1340.73	0.12	>1
1	28	14	-8321.07	0.11	--	2732.11	1127.26	0.11	--
2	28	14	-12468.9	0.17	--	2732.11	1127.26	0.11	--
1	30	15	-9572.5	0.13	20.99	1591.61	1248.62	0.07	>1

Relazione geotecnica

2	30	15	-11217.5	0.15	17.91	1591.61	1248.62	0.07	>1
1	32	16	-9457.13	0.13	--	1537.9	1048.09	0.07	--
2	32	16	-11332.9	0.16	--	1537.9	1048.09	0.07	--
1	34	17	-6261.05	0.09	32.09	4969.69	298.22	0.18	>1
2	34	17	-14528.9	0.2	13.83	4969.69	298.22	0.18	>1
1	36	18	-6611	0.09	--	4549.51	281.39	0.17	--
2	36	18	-14179	0.2	--	4549.51	281.39	0.17	--
1	38	19	-6151.94	0.08	32.66	5143.76	730.2	0.2	>1
2	38	19	-14638.1	0.2	13.72	5143.76	730.2	0.2	>1
1	40	20	-6517.22	0.09	--	4692.18	602.52	0.18	--
2	40	20	-14272.8	0.2	--	4692.18	602.52	0.18	--
1	42	21	-10667	0.15	18.83	687.68	605.26	0.03	>1
2	42	21	-10123	0.14	19.85	687.68	605.26	0.03	>1
1	44	22	-10397.9	0.14	--	545.3	545.29	0.03	--
2	44	22	-10392.1	0.14	--	545.3	545.29	0.03	--
1	46	23	-10557.9	0.15	19.03	466.14	423.16	0.02	>1
2	46	23	-10232.1	0.14	19.63	466.14	423.16	0.02	>1
1	48	24	-10304.1	0.14	--	355.77	338.62	0.02	--
2	48	24	-10485.9	0.14	--	355.77	338.62	0.02	--
1	50	25	-7930.44	0.11	25.33	3365.16	1605.51	0.14	>1
2	50	25	-12859.6	0.18	15.62	3365.16	1605.51	0.14	>1
1	52	26	-8045.81	0.11	--	3149.75	1404.98	0.13	--
2	52	26	-12744.2	0.18	--	3149.75	1404.98	0.13	--
1	54	27	-9252.23	0.13	21.71	2182.31	1697.63	0.1	>1
2	54	27	-11537.8	0.16	17.41	2182.31	1697.63	0.1	>1
1	56	28	-9181.86	0.13	--	2078.93	1484.15	0.09	--
2	56	28	-11608.1	0.16	--	2078.93	1484.15	0.09	--
1	58	29	-7566.74	0.1	26.55	3852.32	1822.56	0.16	>1
2	58	29	-13223.3	0.18	15.19	3852.32	1822.56	0.16	>1
1	60	30	-7733.21	0.11	--	3546.61	1541.38	0.15	--
2	60	30	-13056.8	0.18	--	3546.61	1541.38	0.15	--
1	62	31	-8888.53	0.12	22.6	2502.49	1730.45	0.11	>1
2	62	31	-11901.5	0.16	16.88	2502.49	1730.45	0.11	>1
1	64	32	-8869.27	0.12	--	2343.12	1462.22	0.1	--
2	64	32	-11920.7	0.16	--	2343.12	1462.22	0.1	--
1	66	33	-6353.65	0.09	31.62	3750.54	510.63	0.14	>1
2	66	33	-12546.4	0.17	16.01	3750.54	510.63	0.14	>1
1	68	34	-6680.95	0.09	30.07	3365.41	533.44	0.13	>1
2	68	34	-12219.1	0.17	16.44	3365.41	533.44	0.13	>1
1	70	35	-6530.81	0.09	30.76	3562.71	649.36	0.14	>1
2	70	35	-12369.2	0.17	16.24	3562.71	649.36	0.14	>1
1	72	36	-6503.79	0.09	30.89	3557.42	394.7	0.13	>1
2	72	36	-12396.2	0.17	16.21	3557.42	394.7	0.13	>1
1	74	37	-7188.1	0.1	--	2735.57	340.62	0.1	--
2	74	37	-11711.9	0.16	--	2735.57	340.62	0.1	--
1	76	38	-7515.4	0.1	--	2349.8	363.43	0.09	--
2	76	38	-11384.6	0.16	--	2349.8	363.43	0.09	--
1	78	39	-7365.26	0.1	--	2547.2	479.36	0.1	--
2	78	39	-11534.7	0.16	--	2547.2	479.36	0.1	--
1	80	40	-7338.24	0.1	--	2544.06	224.7	0.1	--
2	80	40	-11561.8	0.16	--	2544.06	224.7	0.1	--
1	82	41	-7619.62	0.11	--	2206.01	205.05	0.08	--
2	82	41	-11280.4	0.16	--	2206.01	205.05	0.08	--
1	84	42	-7946.92	0.11	--	1818.03	227.86	0.07	--
2	84	42	-10953.1	0.15	--	1818.03	227.86	0.07	--
1	86	43	-7796.78	0.11	--	2013.43	343.78	0.08	--
2	86	43	-11103.2	0.15	--	2013.43	343.78	0.08	--
1	88	44	-7769.76	0.11	--	2018.26	89.13	0.07	--
2	88	44	-11130.2	0.15	--	2018.26	89.13	0.07	--
1	90	45	-7792.23	0.11	--	1995.04	150.82	0.07	--
2	90	45	-11107.8	0.15	--	1995.04	150.82	0.07	--
1	92	46	-8119.53	0.11	--	1605.98	173.63	0.06	--
2	92	46	-10780.5	0.15	--	1605.98	173.63	0.06	--
1	94	47	-7969.39	0.11	--	1800.18	289.55	0.07	--
2	94	47	-10930.6	0.15	--	1800.18	289.55	0.07	--
1	96	48	-7942.37	0.11	--	1809.49	34.9	0.07	--
2	96	48	-10957.6	0.15	--	1809.49	34.9	0.07	--

Plinto n. 15

Tipo palo=Trivellato
 Rotazione testa libera
 Coefficiente di efficienza=1.00
 Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>
 Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	-1.2	0

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2	1.2	0
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Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{lim}=252333.00 <daN>

q_p=28.63 <daN/cm²>

QP_{lim}=143893.00 <daN>

k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>

q_p=16.60 <daN/cm²>

QP_{lim}=83431.40 <daN>

k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-9758.24	0.13	19.65	810.37	269.88	0.03	>1
2	1	1	-11031.8	0.15	17.38	810.37	269.88	0.03	>1
1	3	2	-9949.66	0.14	--	582.58	231.95	0.02	--
2	3	2	-10840.3	0.15	--	582.58	231.95	0.02	--
1	5	3	-9916.86	0.14	19.34	807.51	568.21	0.04	>1
2	5	3	-10873.1	0.15	17.64	807.51	568.21	0.04	>1
1	7	4	-10086	0.14	--	613.2	488.37	0.03	--
2	7	4	-10704	0.15	--	613.2	488.37	0.03	--
1	9	5	-12868.5	0.18	14.9	2968.36	28.46	0.11	>1
2	9	5	-7921.48	0.11	24.21	2968.36	28.46	0.11	>1
1	11	6	-12622.9	0.17	--	2673.57	24.47	0.1	--
2	11	6	-8167.12	0.11	--	2673.57	24.47	0.1	--
1	13	7	-13027.1	0.18	14.72	3275.28	866.55	0.13	>1
2	13	7	-7762.86	0.11	24.7	3275.28	866.55	0.13	>1
1	15	8	-12759.2	0.18	--	2933.19	744.79	0.11	--
2	15	8	-8030.79	0.11	--	2933.19	744.79	0.11	--
1	17	9	-10661.8	0.15	17.99	1187.2	1143.22	0.05	>1
2	17	9	-10128.2	0.14	18.93	1187.2	1143.22	0.05	>1
1	19	10	-10726.2	0.15	--	1059.92	982.57	0.05	--
2	19	10	-10063.8	0.14	--	1059.92	982.57	0.05	--
1	21	11	-11594.9	0.16	16.54	1784.23	1053.72	0.08	>1
2	21	11	-9195.13	0.13	20.86	1784.23	1053.72	0.08	>1
1	23	12	-11528.2	0.16	--	1633.82	905.65	0.07	--
2	23	12	-9261.8	0.13	--	1633.82	905.65	0.07	--
1	25	13	-11190.5	0.15	17.14	1906.59	1650.39	0.09	>1
2	25	13	-9599.49	0.13	19.98	1906.59	1650.39	0.09	>1
1	27	14	-11180.7	0.15	--	1703.23	1418.49	0.08	--
2	27	14	-9609.33	0.13	--	1703.23	1418.49	0.08	--
1	29	15	-12123.6	0.17	15.82	2707.4	1739.9	0.12	>1
2	29	15	-8666.4	0.12	22.13	2707.4	1739.9	0.12	>1
1	31	16	-11982.6	0.17	--	2421.97	1495.41	0.1	--
2	31	16	-8807.36	0.12	--	2421.97	1495.41	0.1	--
1	33	17	-9213.74	0.13	20.81	1661.36	866.47	0.07	>1
2	33	17	-11576.3	0.16	16.57	1661.36	866.47	0.07	>1
1	35	18	-9481.67	0.13	--	1325.07	744.71	0.06	--
2	35	18	-11308.3	0.16	--	1325.07	744.71	0.06	--
1	37	19	-9372.36	0.13	20.46	1227.5	28.38	0.05	>1
2	37	19	-11417.6	0.16	16.8	1227.5	28.38	0.05	>1
1	39	20	-9618	0.13	--	932.72	24.39	0.03	--
2	39	20	-11172	0.15	--	932.72	24.39	0.03	--
1	41	21	-12324	0.17	15.56	2383.52	568.13	0.09	>1
2	41	21	-8465.98	0.12	22.65	2383.52	568.13	0.09	>1
1	43	22	-12154.9	0.17	--	2167.59	488.29	0.08	--
2	43	22	-8635.11	0.12	--	2167.59	488.29	0.08	--
1	45	23	-12482.6	0.17	15.36	2519.67	269.95	0.09	>1
2	45	23	-8307.36	0.11	23.08	2519.67	269.95	0.09	>1
1	47	24	-12291.2	0.17	--	2287.27	232.03	0.09	--
2	47	24	-8498.78	0.12	--	2287.27	232.03	0.09	--

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1	49	25	-10117.3	0.14	18.95	1771.45	1739.82	0.08	>1
2	49	25	-10672.7	0.15	17.97	1771.45	1739.82	0.08	>1
1	51	26	-10258.2	0.14	--	1504.31	1495.33	0.07	--
2	51	26	-10531.8	0.15	--	1504.31	1495.33	0.07	--
1	53	27	-11050.4	0.15	17.35	1828.12	1650.31	0.08	>1
2	53	27	-9739.64	0.13	19.69	1828.12	1650.31	0.08	>1
1	55	28	-11060.2	0.15	--	1627.6	1418.41	0.07	--
2	55	28	-9729.79	0.13	--	1627.6	1418.41	0.07	--
1	57	29	-10646	0.15	18.01	1096	1053.8	0.05	>1
2	57	29	-10144	0.14	18.9	1096	1053.8	0.05	>1
1	59	30	-10712.7	0.15	--	982.68	905.73	0.05	--
2	59	30	-10077.3	0.14	--	982.68	905.73	0.05	--
1	61	31	-11579.1	0.16	16.56	1823.77	1143.3	0.08	>1
2	61	31	-9210.9	0.13	20.82	1823.77	1143.3	0.08	>1
1	63	32	-11514.6	0.16	--	1664.57	982.65	0.07	--
2	63	32	-9275.35	0.13	--	1664.57	982.65	0.07	--
1	65	33	-10613.4	0.15	18.07	1408.63	187.94	0.05	>1
2	65	33	-8286.64	0.11	23.14	1408.63	187.94	0.05	>1
1	67	34	-10844.4	0.15	17.68	1681.49	165.78	0.06	>1
2	67	34	-8055.59	0.11	23.81	1681.49	165.78	0.06	>1
1	69	35	-10709.2	0.15	17.91	1536.93	280.63	0.06	>1
2	69	35	-8190.75	0.11	23.41	1536.93	280.63	0.06	>1
1	71	36	-10748.5	0.15	17.84	1559.94	73.1	0.06	>1
2	71	36	-8151.48	0.11	23.53	1559.94	73.1	0.06	>1
1	73	37	-10251.1	0.14	--	968.68	118.97	0.04	--
2	73	37	-8648.88	0.12	--	968.68	118.97	0.04	--
1	75	38	-10482.2	0.14	--	1242.38	96.8	0.05	--
2	75	38	-8417.83	0.12	--	1242.38	96.8	0.05	--
1	77	39	-10347	0.14	--	1097.02	211.65	0.04	--
2	77	39	-8553	0.12	--	1097.02	211.65	0.04	--
1	79	40	-10386.3	0.14	--	1123.55	4.12	0.04	--
2	79	40	-8513.72	0.12	--	1123.55	4.12	0.04	--
1	81	41	-10067.4	0.14	--	742.11	41.88	0.03	--
2	81	41	-8832.56	0.12	--	742.11	41.88	0.03	--
1	83	42	-10298.5	0.14	--	1018.38	19.72	0.04	--
2	83	42	-8601.51	0.12	--	1018.38	19.72	0.04	--
1	85	43	-10163.3	0.14	--	866.5	134.56	0.03	--
2	85	43	-8736.68	0.12	--	866.5	134.56	0.03	--
1	87	44	-10202.6	0.14	--	906.07	72.97	0.03	--
2	87	44	-8697.4	0.12	--	906.07	72.97	0.03	--
1	89	45	-9993.97	0.14	--	652.85	11.05	0.02	--
2	89	45	-8906.04	0.12	--	652.85	11.05	0.02	--
1	91	46	-10225	0.14	--	930.09	11.12	0.03	--
2	91	46	-8674.98	0.12	--	930.09	11.12	0.03	--
1	93	47	-10089.9	0.14	--	774.8	103.73	0.03	--
2	93	47	-8810.15	0.12	--	774.8	103.73	0.03	--
1	95	48	-10129.1	0.14	--	821.54	103.8	0.03	--
2	95	48	-8770.87	0.12	--	821.54	103.8	0.03	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-9758.24	0.13	20.59	810.37	269.88	0.03	>1
2	2	1	-11031.8	0.15	18.21	810.37	269.88	0.03	>1
1	4	2	-9949.66	0.14	--	582.58	231.95	0.02	--
2	4	2	-10840.3	0.15	--	582.58	231.95	0.02	--
1	6	3	-9916.86	0.14	20.26	807.51	568.21	0.04	>1
2	6	3	-10873.1	0.15	18.48	807.51	568.21	0.04	>1
1	8	4	-10086	0.14	--	613.2	488.37	0.03	--
2	8	4	-10704	0.15	--	613.2	488.37	0.03	--
1	10	5	-12868.5	0.18	15.61	2968.36	28.46	0.11	>1
2	10	5	-7921.48	0.11	25.36	2968.36	28.46	0.11	>1
1	12	6	-12622.9	0.17	--	2673.57	24.47	0.1	--
2	12	6	-8167.12	0.11	--	2673.57	24.47	0.1	--
1	14	7	-13027.1	0.18	15.42	3275.28	866.55	0.13	>1
2	14	7	-7762.86	0.11	25.88	3275.28	866.55	0.13	>1
1	16	8	-12759.2	0.18	--	2933.19	744.79	0.11	--
2	16	8	-8030.79	0.11	--	2933.19	744.79	0.11	--
1	18	9	-10661.8	0.15	18.84	1187.2	1143.22	0.05	>1
2	18	9	-10128.2	0.14	19.84	1187.2	1143.22	0.05	>1
1	20	10	-10726.2	0.15	--	1059.92	982.57	0.05	--
2	20	10	-10063.8	0.14	--	1059.92	982.57	0.05	--
1	22	11	-11594.9	0.16	17.33	1784.23	1053.72	0.08	>1
2	22	11	-9195.13	0.13	21.85	1784.23	1053.72	0.08	>1
1	24	12	-11528.2	0.16	--	1633.82	905.65	0.07	--
2	24	12	-9261.8	0.13	--	1633.82	905.65	0.07	--
1	26	13	-11190.5	0.15	17.95	1906.59	1650.39	0.09	>1

Relazione geotecnica

2	26	13	-9599.49	0.13	20.93	1906.59	1650.39	0.09	>1
1	28	14	-11180.7	0.15	--	1703.23	1418.49	0.08	--
2	28	14	-9609.33	0.13	--	1703.23	1418.49	0.08	--
1	30	15	-12123.6	0.17	16.57	2707.4	1739.9	0.12	>1
2	30	15	-8666.4	0.12	23.18	2707.4	1739.9	0.12	>1
1	32	16	-11982.6	0.17	--	2421.97	1495.41	0.1	--
2	32	16	-8807.36	0.12	--	2421.97	1495.41	0.1	--
1	34	17	-9213.74	0.13	21.8	1661.36	866.47	0.07	>1
2	34	17	-11576.3	0.16	17.35	1661.36	866.47	0.07	>1
1	36	18	-9481.67	0.13	--	1325.07	744.71	0.06	--
2	36	18	-11308.3	0.16	--	1325.07	744.71	0.06	--
1	38	19	-9372.36	0.13	21.44	1227.5	28.38	0.05	>1
2	38	19	-11417.6	0.16	17.6	1227.5	28.38	0.05	>1
1	40	20	-9618	0.13	--	932.72	24.39	0.03	--
2	40	20	-11172	0.15	--	932.72	24.39	0.03	--
1	42	21	-12324	0.17	16.3	2383.52	568.13	0.09	>1
2	42	21	-8465.98	0.12	23.73	2383.52	568.13	0.09	>1
1	44	22	-12154.9	0.17	--	2167.59	488.29	0.08	--
2	44	22	-8635.11	0.12	--	2167.59	488.29	0.08	--
1	46	23	-12482.6	0.17	16.09	2519.67	269.95	0.09	>1
2	46	23	-8307.36	0.11	24.18	2519.67	269.95	0.09	>1
1	48	24	-12291.2	0.17	--	2287.27	232.03	0.09	--
2	48	24	-8498.78	0.12	--	2287.27	232.03	0.09	--
1	50	25	-10117.3	0.14	19.86	1771.45	1739.82	0.08	>1
2	50	25	-10672.7	0.15	18.82	1771.45	1739.82	0.08	>1
1	52	26	-10258.2	0.14	--	1504.31	1495.33	0.07	--
2	52	26	-10531.8	0.15	--	1504.31	1495.33	0.07	--
1	54	27	-11050.4	0.15	18.18	1828.12	1650.31	0.08	>1
2	54	27	-9739.64	0.13	20.63	1828.12	1650.31	0.08	>1
1	56	28	-11060.2	0.15	--	1627.6	1418.41	0.07	--
2	56	28	-9729.79	0.13	--	1627.6	1418.41	0.07	--
1	58	29	-10646	0.15	18.87	1096	1053.8	0.05	>1
2	58	29	-10144	0.14	19.81	1096	1053.8	0.05	>1
1	60	30	-10712.7	0.15	--	982.68	905.73	0.05	--
2	60	30	-10077.3	0.14	--	982.68	905.73	0.05	--
1	62	31	-11579.1	0.16	17.35	1823.77	1143.3	0.08	>1
2	62	31	-9210.9	0.13	21.81	1823.77	1143.3	0.08	>1
1	64	32	-11514.6	0.16	--	1664.57	982.65	0.07	--
2	64	32	-9275.35	0.13	--	1664.57	982.65	0.07	--
1	66	33	-10613.4	0.15	18.93	1408.63	187.94	0.05	>1
2	66	33	-8286.64	0.11	24.24	1408.63	187.94	0.05	>1
1	68	34	-10844.4	0.15	18.53	1681.49	165.78	0.06	>1
2	68	34	-8055.59	0.11	24.94	1681.49	165.78	0.06	>1
1	70	35	-10709.2	0.15	18.76	1536.93	280.63	0.06	>1
2	70	35	-8190.75	0.11	24.53	1536.93	280.63	0.06	>1
1	72	36	-10748.5	0.15	18.69	1559.94	73.1	0.06	>1
2	72	36	-8151.48	0.11	24.65	1559.94	73.1	0.06	>1
1	74	37	-10251.1	0.14	--	968.68	118.97	0.04	--
2	74	37	-8648.88	0.12	--	968.68	118.97	0.04	--
1	76	38	-10482.2	0.14	--	1242.38	96.8	0.05	--
2	76	38	-8417.83	0.12	--	1242.38	96.8	0.05	--
1	78	39	-10347	0.14	--	1097.02	211.65	0.04	--
2	78	39	-8553	0.12	--	1097.02	211.65	0.04	--
1	80	40	-10386.3	0.14	--	1123.55	4.12	0.04	--
2	80	40	-8513.72	0.12	--	1123.55	4.12	0.04	--
1	82	41	-10067.4	0.14	--	742.11	41.88	0.03	--
2	82	41	-8832.56	0.12	--	742.11	41.88	0.03	--
1	84	42	-10298.5	0.14	--	1018.38	19.72	0.04	--
2	84	42	-8601.51	0.12	--	1018.38	19.72	0.04	--
1	86	43	-10163.3	0.14	--	866.5	134.56	0.03	--
2	86	43	-8736.68	0.12	--	866.5	134.56	0.03	--
1	88	44	-10202.6	0.14	--	906.07	72.97	0.03	--
2	88	44	-8697.4	0.12	--	906.07	72.97	0.03	--
1	90	45	-9993.97	0.14	--	652.85	11.05	0.02	--
2	90	45	-8906.04	0.12	--	652.85	11.05	0.02	--
1	92	46	-10225	0.14	--	930.09	11.12	0.03	--
2	92	46	-8674.98	0.12	--	930.09	11.12	0.03	--
1	94	47	-10089.9	0.14	--	774.8	103.73	0.03	--
2	94	47	-8810.15	0.12	--	774.8	103.73	0.03	--
1	96	48	-10129.1	0.14	--	821.54	103.8	0.03	--
2	96	48	-8770.87	0.12	--	821.54	103.8	0.03	--

Plinto n. 1

Tipo palo=Trivellato

Rotazione testa libera

Coefficiente di efficienza=1.00

Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>

Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	-1.2	0
2	1.2	0

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{1im}=252333.00 <daN>
 q_p=28.63 <daN/cm²>
 QP_{1im}=143893.00 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{1im}=321694.00 <daN>
 q_p=16.60 <daN/cm²>
 QP_{1im}=83431.40 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-9659.59	0.13	19.85	882.7	19.28	0.03	>1
2	1	1	-11130.4	0.15	17.23	882.7	19.28	0.03	>1
1	3	2	-9909.42	0.14	--	583.18	23.63	0.02	--
2	3	2	-10880.6	0.15	--	583.18	23.63	0.02	--
1	5	3	-9555.73	0.13	20.07	1295.31	814.57	0.06	>1
2	5	3	-11234.3	0.15	17.07	1295.31	814.57	0.06	>1
1	7	4	-9820.14	0.14	--	977.85	693.05	0.04	--
2	7	4	-10969.9	0.15	--	977.85	693.05	0.04	--
1	9	5	-12790.5	0.18	14.99	2891.97	316.47	0.11	>1
2	9	5	-7999.5	0.11	23.97	2891.97	316.47	0.11	>1
1	11	6	-12600.4	0.17	--	2661.12	279.05	0.1	--
2	11	6	-8189.63	0.11	--	2661.12	279.05	0.1	--
1	13	7	-12686.6	0.17	15.12	2798.21	517.38	0.11	>1
2	13	7	-8103.37	0.11	23.67	2798.21	517.38	0.11	>1
1	15	8	-12511.1	0.17	--	2576.76	437.63	0.1	--
2	15	8	-8278.9	0.11	--	2576.76	437.63	0.1	--
1	17	9	-10876.6	0.15	17.63	1239.14	1096.13	0.06	>1
2	17	9	-9913.41	0.14	19.34	1239.14	1096.13	0.06	>1
1	19	10	-10955.4	0.15	--	1163.24	949.15	0.05	--
2	19	10	-9834.6	0.14	--	1163.24	949.15	0.05	--
1	21	11	-11815.9	0.16	16.23	2076.55	1185.28	0.09	>1
2	21	11	-8974.14	0.12	21.37	2076.55	1185.28	0.09	>1
1	23	12	-11762.7	0.16	--	1935.42	1025.78	0.08	--
2	23	12	-9027.31	0.12	--	1935.42	1025.78	0.08	--
1	25	13	-10530.4	0.15	18.21	1691.19	1683.37	0.08	>1
2	25	13	-10259.6	0.14	18.69	1691.19	1683.37	0.08	>1
1	27	14	-10657.8	0.15	--	1473.92	1439.78	0.07	--
2	27	14	-10132.2	0.14	--	1473.92	1439.78	0.07	--
1	29	15	-11469.6	0.16	16.72	2050.49	1594.22	0.09	>1
2	29	15	-9320.36	0.13	20.58	2050.49	1594.22	0.09	>1
1	31	16	-11465.1	0.16	--	1872.75	1363.15	0.08	--
2	31	16	-9324.88	0.13	--	1872.75	1363.15	0.08	--
1	33	17	-10188.3	0.14	18.82	665.68	617.73	0.03	>1
2	33	17	-10601.7	0.15	18.09	665.68	617.73	0.03	>1
1	35	18	-10363.8	0.14	--	539.28	537.98	0.03	--
2	35	18	-10426.2	0.14	--	539.28	537.98	0.03	--
1	37	19	-10084.4	0.14	19.02	430.84	216.12	0.02	>1
2	37	19	-10705.6	0.15	17.91	430.84	216.12	0.02	>1
1	39	20	-10274.5	0.14	--	229.85	178.7	0.01	--
2	39	20	-10515.5	0.14	--	229.85	178.7	0.01	--
1	41	21	-13319.2	0.18	14.4	3626.34	914.92	0.14	>1
2	41	21	-7470.81	0.1	25.67	3626.34	914.92	0.14	>1
1	43	22	-13054.8	0.18	--	3288.86	793.41	0.13	--
2	43	22	-7735.23	0.11	--	3288.86	793.41	0.13	--

Relazione geotecnica

1	45	23	-13215.3	0.18	14.51	3385.36	81.07	0.12	>1
2	45	23	-7574.68	0.1	25.32	3385.36	81.07	0.12	>1
1	47	24	-12965.5	0.18	--	3085.55	76.73	0.11	--
2	47	24	-7824.5	0.11	--	3085.55	76.73	0.11	--
1	49	25	-11405.3	0.16	16.81	2083.58	1694.57	0.09	>1
2	49	25	-9384.73	0.13	20.43	2083.58	1694.57	0.09	>1
1	51	26	-11409.8	0.16	--	1903.88	1463.5	0.08	--
2	51	26	-9380.2	0.13	--	1903.88	1463.5	0.08	--
1	53	27	-12344.6	0.17	15.53	2941.9	1783.73	0.13	>1
2	53	27	-8445.45	0.12	22.71	2941.9	1783.73	0.13	>1
1	55	28	-12217.1	0.17	--	2674.47	1540.13	0.11	--
2	55	28	-8572.92	0.12	--	2674.47	1540.13	0.11	--
1	57	29	-11059.1	0.15	17.34	1346.13	1084.93	0.06	>1
2	57	29	-9730.95	0.13	19.71	1346.13	1084.93	0.06	>1
1	59	30	-11112.2	0.15	--	1263.79	925.43	0.06	--
2	59	30	-9677.78	0.13	--	1263.79	925.43	0.06	--
1	61	31	-11998.3	0.17	15.98	2166.4	995.77	0.09	>1
2	61	31	-8791.68	0.12	21.81	2166.4	995.77	0.09	>1
1	63	32	-11919.5	0.16	--	2016.73	848.8	0.08	--
2	63	32	-8870.49	0.12	--	2016.73	848.8	0.08	--
1	65	33	-11170.6	0.15	17.17	2068.02	115.86	0.08	>1
2	65	33	-7729.35	0.11	24.81	2068.02	115.86	0.08	>1
1	67	34	-11403.2	0.16	16.82	2345.75	93.78	0.09	>1
2	67	34	-7496.77	0.1	25.58	2345.75	93.78	0.09	>1
1	69	35	-11299.8	0.16	16.97	2219.76	1.58	0.08	>1
2	69	35	-7600.2	0.1	25.23	2219.76	1.58	0.08	>1
1	71	36	-11274.1	0.16	17.01	2198.76	208.06	0.08	>1
2	71	36	-7625.92	0.11	25.15	2198.76	208.06	0.08	>1
1	73	37	-10650.4	0.15	--	1442	65.54	0.05	--
2	73	37	-8249.58	0.11	--	1442	65.54	0.05	--
1	75	38	-10883	0.15	--	1720.16	43.46	0.06	--
2	75	38	-8016.99	0.11	--	1720.16	43.46	0.06	--
1	77	39	-10779.6	0.15	--	1596.24	48.74	0.06	--
2	77	39	-8120.42	0.11	--	1596.24	48.74	0.06	--
1	79	40	-10753.9	0.15	--	1572.56	157.74	0.06	--
2	79	40	-8146.14	0.11	--	1572.56	157.74	0.06	--
1	81	41	-10386.8	0.14	--	1124.22	5.97	0.04	--
2	81	41	-8513.17	0.12	--	1124.22	5.97	0.04	--
1	83	42	-10619.4	0.15	--	1403.58	28.05	0.05	--
2	83	42	-8280.58	0.11	--	1403.58	28.05	0.05	--
1	85	43	-10516	0.14	--	1284.82	120.25	0.05	--
2	85	43	-8384.02	0.12	--	1284.82	120.25	0.05	--
1	87	44	-10490.3	0.14	--	1251.29	86.23	0.05	--
2	87	44	-8409.74	0.12	--	1251.29	86.23	0.05	--
1	89	45	-10281.4	0.14	--	998.27	34.58	0.04	--
2	89	45	-8618.6	0.12	--	998.27	34.58	0.04	--
1	91	46	-10514	0.14	--	1278.03	56.65	0.05	--
2	91	46	-8386.02	0.12	--	1278.03	56.65	0.05	--
1	93	47	-10410.5	0.14	--	1162.23	148.85	0.04	--
2	93	47	-8489.45	0.12	--	1162.23	148.85	0.04	--
1	95	48	-10384.8	0.14	--	1123.27	57.62	0.04	--
2	95	48	-8515.17	0.12	--	1123.27	57.62	0.04	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-9659.59	0.13	20.8	882.7	19.28	0.03	>1
2	2	1	-11130.4	0.15	18.05	882.7	19.28	0.03	>1
1	4	2	-9909.42	0.14	--	583.18	23.63	0.02	--
2	4	2	-10880.6	0.15	--	583.18	23.63	0.02	--
1	6	3	-9555.73	0.13	21.02	1295.31	814.57	0.06	>1
2	6	3	-11234.3	0.15	17.88	1295.31	814.57	0.06	>1
1	8	4	-9820.14	0.14	--	977.85	693.05	0.04	--
2	8	4	-10969.9	0.15	--	977.85	693.05	0.04	--
1	10	5	-12790.5	0.18	15.71	2891.97	316.47	0.11	>1
2	10	5	-7999.5	0.11	25.11	2891.97	316.47	0.11	>1
1	12	6	-12600.4	0.17	--	2661.12	279.05	0.1	--
2	12	6	-8189.63	0.11	--	2661.12	279.05	0.1	--
1	14	7	-12686.6	0.17	15.84	2798.21	517.38	0.11	>1
2	14	7	-8103.37	0.11	24.79	2798.21	517.38	0.11	>1
1	16	8	-12511.1	0.17	--	2576.76	437.63	0.1	--
2	16	8	-8278.9	0.11	--	2576.76	437.63	0.1	--
1	18	9	-10876.6	0.15	18.47	1239.14	1096.13	0.06	>1
2	18	9	-9913.41	0.14	20.27	1239.14	1096.13	0.06	>1
1	20	10	-10955.4	0.15	--	1163.24	949.15	0.05	--
2	20	10	-9834.6	0.14	--	1163.24	949.15	0.05	--
1	22	11	-11815.9	0.16	17	2076.55	1185.28	0.09	>1

Relazione geotecnica

2	22	11	-8974.14	0.12	22.39	2076.55	1185.28	0.09	>1
1	24	12	-11762.7	0.16	--	1935.42	1025.78	0.08	--
2	24	12	-9027.31	0.12	--	1935.42	1025.78	0.08	--
1	26	13	-10530.4	0.15	19.08	1691.19	1683.37	0.08	>1
2	26	13	-10259.6	0.14	19.58	1691.19	1683.37	0.08	>1
1	28	14	-10657.8	0.15	--	1473.92	1439.78	0.07	--
2	28	14	-10132.2	0.14	--	1473.92	1439.78	0.07	--
1	30	15	-11469.6	0.16	17.52	2050.49	1594.22	0.09	>1
2	30	15	-9320.36	0.13	21.56	2050.49	1594.22	0.09	>1
1	32	16	-11465.1	0.16	--	1872.75	1363.15	0.08	--
2	32	16	-9324.88	0.13	--	1872.75	1363.15	0.08	--
1	34	17	-10188.3	0.14	19.72	665.68	617.73	0.03	>1
2	34	17	-10601.7	0.15	18.95	665.68	617.73	0.03	>1
1	36	18	-10363.8	0.14	--	539.28	537.98	0.03	--
2	36	18	-10426.2	0.14	--	539.28	537.98	0.03	--
1	38	19	-10084.4	0.14	19.92	430.84	216.12	0.02	>1
2	38	19	-10705.6	0.15	18.77	430.84	216.12	0.02	>1
1	40	20	-10274.5	0.14	--	229.85	178.7	0.01	--
2	40	20	-10515.5	0.14	--	229.85	178.7	0.01	--
1	42	21	-13319.2	0.18	15.08	3626.34	914.92	0.14	>1
2	42	21	-7470.81	0.1	26.89	3626.34	914.92	0.14	>1
1	44	22	-13054.8	0.18	--	3288.86	793.41	0.13	--
2	44	22	-7735.23	0.11	--	3288.86	793.41	0.13	--
1	46	23	-13215.3	0.18	15.2	3385.36	81.07	0.12	>1
2	46	23	-7574.68	0.1	26.52	3385.36	81.07	0.12	>1
1	48	24	-12965.5	0.18	--	3085.55	76.73	0.11	--
2	48	24	-7824.5	0.11	--	3085.55	76.73	0.11	--
1	50	25	-11405.3	0.16	17.61	2083.58	1694.57	0.09	>1
2	50	25	-9384.73	0.13	21.41	2083.58	1694.57	0.09	>1
1	52	26	-11409.8	0.16	--	1903.88	1463.5	0.08	--
2	52	26	-9380.2	0.13	--	1903.88	1463.5	0.08	--
1	54	27	-12344.6	0.17	16.27	2941.9	1783.73	0.13	>1
2	54	27	-8445.45	0.12	23.79	2941.9	1783.73	0.13	>1
1	56	28	-12217.1	0.17	--	2674.47	1540.13	0.11	--
2	56	28	-8572.92	0.12	--	2674.47	1540.13	0.11	--
1	58	29	-11059.1	0.15	18.17	1346.13	1084.93	0.06	>1
2	58	29	-9730.95	0.13	20.65	1346.13	1084.93	0.06	>1
1	60	30	-11112.2	0.15	--	1263.79	925.43	0.06	--
2	60	30	-9677.78	0.13	--	1263.79	925.43	0.06	--
1	62	31	-11998.3	0.17	16.74	2166.4	995.77	0.09	>1
2	62	31	-8791.68	0.12	22.85	2166.4	995.77	0.09	>1
1	64	32	-11919.5	0.16	--	2016.73	848.8	0.08	--
2	64	32	-8870.49	0.12	--	2016.73	848.8	0.08	--
1	66	33	-11170.6	0.15	17.98	2068.02	115.86	0.08	>1
2	66	33	-7729.35	0.11	25.99	2068.02	115.86	0.08	>1
1	68	34	-11403.2	0.16	17.62	2345.75	93.78	0.09	>1
2	68	34	-7496.77	0.1	26.8	2345.75	93.78	0.09	>1
1	70	35	-11299.8	0.16	17.78	2219.76	1.58	0.08	>1
2	70	35	-7600.2	0.1	26.43	2219.76	1.58	0.08	>1
1	72	36	-11274.1	0.16	17.82	2198.76	208.06	0.08	>1
2	72	36	-7625.92	0.11	26.34	2198.76	208.06	0.08	>1
1	74	37	-10650.4	0.15	--	1442	65.54	0.05	--
2	74	37	-8249.58	0.11	--	1442	65.54	0.05	--
1	76	38	-10883	0.15	--	1720.16	43.46	0.06	--
2	76	38	-8016.99	0.11	--	1720.16	43.46	0.06	--
1	78	39	-10779.6	0.15	--	1596.24	48.74	0.06	--
2	78	39	-8120.42	0.11	--	1596.24	48.74	0.06	--
1	80	40	-10753.9	0.15	--	1572.56	157.74	0.06	--
2	80	40	-8146.14	0.11	--	1572.56	157.74	0.06	--
1	82	41	-10386.8	0.14	--	1124.22	5.97	0.04	--
2	82	41	-8513.17	0.12	--	1124.22	5.97	0.04	--
1	84	42	-10619.4	0.15	--	1403.58	28.05	0.05	--
2	84	42	-8280.58	0.11	--	1403.58	28.05	0.05	--
1	86	43	-10516	0.14	--	1284.82	120.25	0.05	--
2	86	43	-8384.02	0.12	--	1284.82	120.25	0.05	--
1	88	44	-10490.3	0.14	--	1251.29	86.23	0.05	--
2	88	44	-8409.74	0.12	--	1251.29	86.23	0.05	--
1	90	45	-10281.4	0.14	--	998.27	34.58	0.04	--
2	90	45	-8618.6	0.12	--	998.27	34.58	0.04	--
1	92	46	-10514	0.14	--	1278.03	56.65	0.05	--
2	92	46	-8386.02	0.12	--	1278.03	56.65	0.05	--
1	94	47	-10410.5	0.14	--	1162.23	148.85	0.04	--
2	94	47	-8489.45	0.12	--	1162.23	148.85	0.04	--
1	96	48	-10384.8	0.14	--	1123.27	57.62	0.04	--
2	96	48	-8515.17	0.12	--	1123.27	57.62	0.04	--

Plinto n. 2

Tipo palo=Trivellato
Rotazione testa libera

Relazione geotecnica

Coefficiente di efficienza=1.00
 Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>
 Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp	Yp
	<m>	<m>
1	-1.2	0
2	1.2	0

Verifiche in condizioni drenate

Zp	τ_s	k_s	σ_h	k_h
<m>	<daN/cm ² >	<daN/cm ² >	<daN/cm ² >	<daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{1im}=252333.00 <daN>
 q_p=28.63 <daN/cm²>
 QP_{1im}=143893.00 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp	τ_s	k_s	σ_h	k_h
<m>	<daN/cm ² >	<daN/cm ² >	<daN/cm ² >	<daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{1im}=321694.00 <daN>
 q_p=16.60 <daN/cm²>
 QP_{1im}=83431.40 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N	Ced	Sic.V	T	M	Sps	Sic.O
			<daN>	<cm>		<daN>	<daNm>	<cm>	
1	1	1	-8617.02	0.12	22.25	2135.83	98.16	0.08	>1
2	1	1	-12173	0.17	15.75	2135.83	98.16	0.08	>1
1	3	2	-9008.03	0.12	--	1670.12	138.55	0.06	--
2	3	2	-11782	0.16	--	1670.12	138.55	0.06	--
1	5	3	-8601.16	0.12	22.3	2386.62	1030.63	0.1	>1
2	5	3	-12188.8	0.17	15.73	2386.62	1030.63	0.1	>1
1	7	4	-8994.4	0.12	--	1925.72	939.99	0.08	--
2	7	4	-11795.6	0.16	--	1925.72	939.99	0.08	--
1	9	5	-13457.8	0.19	14.25	3676.93	106.36	0.14	>1
2	9	5	-7332.18	0.1	26.15	3676.93	106.36	0.14	>1
1	11	6	-13168.6	0.18	--	3331.52	145.6	0.12	--
2	11	6	-7621.39	0.11	--	3331.52	145.6	0.12	--
1	13	7	-13442	0.19	14.27	3801.06	1038.84	0.15	>1
2	13	7	-7348.04	0.1	26.1	3801.06	1038.84	0.15	>1
1	15	8	-13155	0.18	--	3444.72	947.05	0.14	--
2	15	8	-7635.02	0.11	--	3444.72	947.05	0.14	--
1	17	9	-10329.8	0.14	18.56	989.95	986.85	0.05	>1
2	17	9	-10460.2	0.14	18.33	989.95	986.85	0.05	>1
1	19	10	-10480.1	0.14	--	800.54	794	0.04	--
2	19	10	-10309.9	0.14	--	800.54	794	0.04	--
1	21	11	-11782	0.16	16.28	1933.77	984.39	0.08	>1
2	21	11	-9007.95	0.12	21.29	1933.77	984.39	0.08	>1
1	23	12	-11728.3	0.16	--	1785.22	791.88	0.07	--
2	23	12	-9061.68	0.12	--	1785.22	791.88	0.07	--
1	25	13	-10276.9	0.14	18.66	2126.11	2121.39	0.1	>1
2	25	13	-10513.1	0.14	18.24	2126.11	2121.39	0.1	>1
1	27	14	-10434.7	0.14	--	1878.08	1877.48	0.09	--
2	27	14	-10355.3	0.14	--	1878.08	1877.48	0.09	--
1	29	15	-11729.2	0.16	16.35	2659.69	2123.85	0.12	>1
2	29	15	-9060.83	0.12	21.16	2659.69	2123.85	0.12	>1
1	31	16	-11682.9	0.16	--	2433.36	1879.59	0.11	--
2	31	16	-9107.13	0.13	--	2433.36	1879.59	0.11	--
1	33	17	-9357.37	0.13	20.49	1273.59	267.63	0.05	>1
2	33	17	-11432.6	0.16	16.77	1273.59	267.63	0.05	>1
1	35	18	-9644.35	0.13	--	917.78	175.83	0.04	--
2	35	18	-11145.7	0.15	--	917.78	175.83	0.04	--
1	37	19	-9341.51	0.13	20.53	1428.36	664.85	0.06	>1
2	37	19	-11448.5	0.16	16.75	1428.36	664.85	0.06	>1
1	39	20	-9630.72	0.13	--	1110.2	625.61	0.05	--
2	39	20	-11159.3	0.15	--	1110.2	625.61	0.05	--

Relazione geotecnica

1	41	21	-14198.2	0.2	13.51	4571.17	259.42	0.17	>1
2	41	21	-6591.83	0.09	29.09	4571.17	259.42	0.17	>1
1	43	22	-13804.9	0.19	--	4095.4	168.78	0.15	--
2	43	22	-6985.07	0.1	--	4095.4	168.78	0.15	--
1	45	23	-14182.3	0.2	13.52	4594.34	673.05	0.17	>1
2	45	23	-6607.69	0.09	29.02	4594.34	673.05	0.17	>1
1	47	24	-13791.3	0.19	--	4124.37	632.66	0.16	--
2	47	24	-6998.7	0.1	--	4124.37	632.66	0.16	--
1	49	25	-11070.2	0.15	17.32	1576.72	1352.64	0.07	>1
2	49	25	-9719.84	0.13	19.73	1576.72	1352.64	0.07	>1
1	51	26	-11116.5	0.15	--	1406.43	1108.38	0.06	--
2	51	26	-9673.54	0.13	--	1406.43	1108.38	0.06	--
1	53	27	-12522.4	0.17	15.31	2887.93	1350.17	0.12	>1
2	53	27	-8267.6	0.11	23.2	2887.93	1350.17	0.12	>1
1	55	28	-12364.6	0.17	--	2609.64	1106.27	0.11	--
2	55	28	-8425.37	0.12	--	2609.64	1106.27	0.11	--
1	57	29	-11017.3	0.15	17.41	1907.82	1755.6	0.09	>1
2	57	29	-9772.72	0.13	19.62	1907.82	1755.6	0.09	>1
1	59	30	-11071	0.15	--	1761.06	1563.09	0.08	--
2	59	30	-9718.99	0.13	--	1761.06	1563.09	0.08	--
1	61	31	-12469.5	0.17	15.38	3047.63	1758.07	0.13	>1
2	61	31	-8320.48	0.11	23.05	3047.63	1758.07	0.13	>1
1	63	32	-12319.2	0.17	--	2789.53	1565.21	0.12	--
2	63	32	-8470.81	0.12	--	2789.53	1565.21	0.12	--
1	65	33	-11116.5	0.15	17.25	2224.07	973.23	0.09	>1
2	65	33	-7783.48	0.11	24.64	2224.07	973.23	0.09	>1
1	67	34	-11476.1	0.16	16.71	2619.13	973.84	0.11	>1
2	67	34	-7423.88	0.1	25.83	2619.13	973.84	0.11	>1
1	69	35	-11298.3	0.16	16.97	2378.15	858.09	0.1	>1
2	69	35	-7601.72	0.1	25.23	2378.15	858.09	0.1	>1
1	71	36	-11294.4	0.16	16.98	2466.63	1088.99	0.1	>1
2	71	36	-7605.65	0.1	25.21	2466.63	1088.99	0.1	>1
1	73	37	-10585.5	0.15	--	1516.74	666.13	0.06	--
2	73	37	-8314.47	0.11	--	1516.74	666.13	0.06	--
1	75	38	-10945.1	0.15	--	1914.04	666.74	0.08	--
2	75	38	-7954.87	0.11	--	1914.04	666.74	0.08	--
1	77	39	-10767.3	0.15	--	1674.02	550.98	0.07	--
2	77	39	-8132.71	0.11	--	1674.02	550.98	0.07	--
1	79	40	-10763.4	0.15	--	1759.33	781.88	0.07	--
2	79	40	-8136.64	0.11	--	1759.33	781.88	0.07	--
1	81	41	-10298.4	0.14	--	1109.27	440.5	0.05	--
2	81	41	-8601.62	0.12	--	1109.27	440.5	0.05	--
1	83	42	-10658	0.15	--	1515.22	441.11	0.06	--
2	83	42	-8242.01	0.11	--	1515.22	441.11	0.06	--
1	85	43	-10480.2	0.14	--	1278.28	325.35	0.05	--
2	85	43	-8419.85	0.12	--	1278.28	325.35	0.05	--
1	87	44	-10476.2	0.14	--	1351.27	556.25	0.06	--
2	87	44	-8423.78	0.12	--	1351.27	556.25	0.06	--
1	89	45	-10183.5	0.14	--	947.36	350.25	0.04	--
2	89	45	-8716.47	0.12	--	947.36	350.25	0.04	--
1	91	46	-10543.1	0.15	--	1357.87	350.86	0.05	--
2	91	46	-8356.87	0.12	--	1357.87	350.86	0.05	--
1	93	47	-10365.3	0.14	--	1123.23	235.1	0.04	--
2	93	47	-8534.71	0.12	--	1123.23	235.1	0.04	--
1	95	48	-10361.4	0.14	--	1188.78	466	0.05	--
2	95	48	-8538.63	0.12	--	1188.78	466	0.05	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-8617.02	0.12	23.31	2135.83	98.16	0.08	>1
2	2	1	-12173	0.17	16.5	2135.83	98.16	0.08	>1
1	4	2	-9008.03	0.12	--	1670.12	138.55	0.06	--
2	4	2	-11782	0.16	--	1670.12	138.55	0.06	--
1	6	3	-8601.16	0.12	23.36	2386.62	1030.63	0.1	>1
2	6	3	-12188.8	0.17	16.48	2386.62	1030.63	0.1	>1
1	8	4	-8994.4	0.12	--	1925.72	939.99	0.08	--
2	8	4	-11795.6	0.16	--	1925.72	939.99	0.08	--
1	10	5	-13457.8	0.19	14.93	3676.93	106.36	0.14	>1
2	10	5	-7332.18	0.1	27.4	3676.93	106.36	0.14	>1
1	12	6	-13168.6	0.18	--	3331.52	145.6	0.12	--
2	12	6	-7621.39	0.11	--	3331.52	145.6	0.12	--
1	14	7	-13442	0.19	14.95	3801.06	1038.84	0.15	>1
2	14	7	-7348.04	0.1	27.34	3801.06	1038.84	0.15	>1
1	16	8	-13155	0.18	--	3444.72	947.05	0.14	--
2	16	8	-7635.02	0.11	--	3444.72	947.05	0.14	--
1	18	9	-10329.8	0.14	19.45	989.95	986.85	0.05	>1

Relazione geotecnica

2	18	9	-10460.2	0.14	19.21	989.95	986.85	0.05	>1
1	20	10	-10480.1	0.14	--	800.54	794	0.04	--
2	20	10	-10309.9	0.14	--	800.54	794	0.04	--
1	22	11	-11782	0.16	17.05	1933.77	984.39	0.08	>1
2	22	11	-9007.95	0.12	22.3	1933.77	984.39	0.08	>1
1	24	12	-11728.3	0.16	--	1785.22	791.88	0.07	--
2	24	12	-9061.68	0.12	--	1785.22	791.88	0.07	--
1	26	13	-10276.9	0.14	19.55	2126.11	2121.39	0.1	>1
2	26	13	-10513.1	0.14	19.11	2126.11	2121.39	0.1	>1
1	28	14	-10434.7	0.14	--	1878.08	1877.48	0.09	--
2	28	14	-10355.3	0.14	--	1878.08	1877.48	0.09	--
1	30	15	-11729.2	0.16	17.13	2659.69	2123.85	0.12	>1
2	30	15	-9060.83	0.12	22.17	2659.69	2123.85	0.12	>1
1	32	16	-11682.9	0.16	--	2433.36	1879.59	0.11	--
2	32	16	-9107.13	0.13	--	2433.36	1879.59	0.11	--
1	34	17	-9357.37	0.13	21.47	1273.59	267.63	0.05	>1
2	34	17	-11432.6	0.16	17.57	1273.59	267.63	0.05	>1
1	36	18	-9644.35	0.13	--	917.78	175.83	0.04	--
2	36	18	-11145.7	0.15	--	917.78	175.83	0.04	--
1	38	19	-9341.51	0.13	21.51	1428.36	664.85	0.06	>1
2	38	19	-11448.5	0.16	17.55	1428.36	664.85	0.06	>1
1	40	20	-9630.72	0.13	--	1110.2	625.61	0.05	--
2	40	20	-11159.3	0.15	--	1110.2	625.61	0.05	--
1	42	21	-14198.2	0.2	14.15	4571.17	259.42	0.17	>1
2	42	21	-6591.83	0.09	30.48	4571.17	259.42	0.17	>1
1	44	22	-13804.9	0.19	--	4095.4	168.78	0.15	--
2	44	22	-6985.07	0.1	--	4095.4	168.78	0.15	--
1	46	23	-14182.3	0.2	14.17	4594.34	673.05	0.17	>1
2	46	23	-6607.69	0.09	30.4	4594.34	673.05	0.17	>1
1	48	24	-13791.3	0.19	--	4124.37	632.66	0.16	--
2	48	24	-6998.7	0.1	--	4124.37	632.66	0.16	--
1	50	25	-11070.2	0.15	18.15	1576.72	1352.64	0.07	>1
2	50	25	-9719.84	0.13	20.67	1576.72	1352.64	0.07	>1
1	52	26	-11116.5	0.15	--	1406.43	1108.38	0.06	--
2	52	26	-9673.54	0.13	--	1406.43	1108.38	0.06	--
1	54	27	-12522.4	0.17	16.04	2887.93	1350.17	0.12	>1
2	54	27	-8267.6	0.11	24.3	2887.93	1350.17	0.12	>1
1	56	28	-12364.6	0.17	--	2609.64	1106.27	0.11	--
2	56	28	-8425.37	0.12	--	2609.64	1106.27	0.11	--
1	58	29	-11017.3	0.15	18.24	1907.82	1755.6	0.09	>1
2	58	29	-9772.72	0.13	20.56	1907.82	1755.6	0.09	>1
1	60	30	-11071	0.15	--	1761.06	1563.09	0.08	--
2	60	30	-9718.99	0.13	--	1761.06	1563.09	0.08	--
1	62	31	-12469.5	0.17	16.11	3047.63	1758.07	0.13	>1
2	62	31	-8320.48	0.11	24.15	3047.63	1758.07	0.13	>1
1	64	32	-12319.2	0.17	--	2789.53	1565.21	0.12	--
2	64	32	-8470.81	0.12	--	2789.53	1565.21	0.12	--
1	66	33	-11116.5	0.15	18.07	2224.07	973.23	0.09	>1
2	66	33	-7783.48	0.11	25.81	2224.07	973.23	0.09	>1
1	68	34	-11476.1	0.16	17.51	2619.13	973.84	0.11	>1
2	68	34	-7423.88	0.1	27.06	2619.13	973.84	0.11	>1
1	70	35	-11298.3	0.16	17.78	2378.15	858.09	0.1	>1
2	70	35	-7601.72	0.1	26.43	2378.15	858.09	0.1	>1
1	72	36	-11294.4	0.16	17.79	2466.63	1088.99	0.1	>1
2	72	36	-7605.65	0.1	26.41	2466.63	1088.99	0.1	>1
1	74	37	-10585.5	0.15	--	1516.74	666.13	0.06	--
2	74	37	-8314.47	0.11	--	1516.74	666.13	0.06	--
1	76	38	-10945.1	0.15	--	1914.04	666.74	0.08	--
2	76	38	-7954.87	0.11	--	1914.04	666.74	0.08	--
1	78	39	-10767.3	0.15	--	1674.02	550.98	0.07	--
2	78	39	-8132.71	0.11	--	1674.02	550.98	0.07	--
1	80	40	-10763.4	0.15	--	1759.33	781.88	0.07	--
2	80	40	-8136.64	0.11	--	1759.33	781.88	0.07	--
1	82	41	-10298.4	0.14	--	1109.27	440.5	0.05	--
2	82	41	-8601.62	0.12	--	1109.27	440.5	0.05	--
1	84	42	-10658	0.15	--	1515.22	441.11	0.06	--
2	84	42	-8242.01	0.11	--	1515.22	441.11	0.06	--
1	86	43	-10480.2	0.14	--	1278.28	325.35	0.05	--
2	86	43	-8419.85	0.12	--	1278.28	325.35	0.05	--
1	88	44	-10476.2	0.14	--	1351.27	556.25	0.06	--
2	88	44	-8423.78	0.12	--	1351.27	556.25	0.06	--
1	90	45	-10183.5	0.14	--	947.36	350.25	0.04	--
2	90	45	-8716.47	0.12	--	947.36	350.25	0.04	--
1	92	46	-10543.1	0.15	--	1357.87	350.86	0.05	--
2	92	46	-8356.87	0.12	--	1357.87	350.86	0.05	--
1	94	47	-10365.3	0.14	--	1123.23	235.1	0.04	--
2	94	47	-8534.71	0.12	--	1123.23	235.1	0.04	--
1	96	48	-10361.4	0.14	--	1188.78	466	0.05	--
2	96	48	-8538.63	0.12	--	1188.78	466	0.05	--

Plinto n. 3

Tipo palo=Trivellato
 Rotazione testa libera
 Coefficiente di efficienza=1.00
 Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>
 Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	-1.2	0
2	1.2	0

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{lim}=252333.00 <daN>
 q_p=28.63 <daN/cm²>
 QP_{lim}=143893.00 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>
 q_p=16.60 <daN/cm²>
 QP_{lim}=83431.40 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-7996.94	0.11	23.98	2877.8	27.5	0.11	>1
2	1	1	-12793.1	0.18	14.99	2877.8	27.5	0.11	>1
1	3	2	-8439.55	0.12	--	2348.06	84.69	0.09	--
2	3	2	-12350.4	0.17	--	2348.06	84.69	0.09	--
1	5	3	-8049.65	0.11	23.82	2981.32	983.51	0.12	>1
2	5	3	-12740.4	0.18	15.05	2981.32	983.51	0.12	>1
1	7	4	-8484.85	0.12	--	2464.87	906.36	0.1	--
2	7	4	-12305.1	0.17	--	2464.87	906.36	0.1	--
1	9	5	-13457	0.19	14.25	3674.71	51.57	0.13	>1
2	9	5	-7333.04	0.1	26.15	3674.71	51.57	0.13	>1
1	11	6	-13132.3	0.18	--	3286.5	105.37	0.12	--
2	11	6	-7657.66	0.11	--	3286.5	105.37	0.12	--
1	13	7	-13509.7	0.19	14.19	3871.03	1007.58	0.15	>1
2	13	7	-7280.33	0.1	26.34	3871.03	1007.58	0.15	>1
1	15	8	-13177.6	0.18	--	3465.47	927.05	0.14	--
2	15	8	-7612.36	0.1	--	3465.47	927.05	0.14	--
1	17	9	-9846.46	0.14	19.48	1264.3	1079.43	0.06	>1
2	17	9	-10943.5	0.15	17.52	1264.3	1079.43	0.06	>1
1	19	10	-10029.2	0.14	--	971.53	866.7	0.04	--
2	19	10	-10760.8	0.15	--	971.53	866.7	0.04	--
1	21	11	-11484.5	0.16	16.7	1690.8	1072.21	0.07	>1
2	21	11	-9305.54	0.13	20.61	1690.8	1072.21	0.07	>1
1	23	12	-11437	0.16	--	1517.89	860.49	0.06	--
2	23	12	-9352.99	0.13	--	1517.89	860.49	0.06	--
1	25	13	-10022.1	0.14	19.13	2154.26	2107.29	0.1	>1
2	25	13	-10767.9	0.15	17.81	2154.26	2107.29	0.1	>1
1	27	14	-10180.2	0.14	--	1889.89	1872.23	0.09	--
2	27	14	-10609.8	0.15	--	1889.89	1872.23	0.09	--
1	29	15	-11660.2	0.16	16.45	2603.08	2114.51	0.12	>1
2	29	15	-9129.85	0.13	21	2603.08	2114.51	0.12	>1
1	31	16	-11588	0.16	--	2361.79	1878.43	0.11	--
2	31	16	-9201.99	0.13	--	2361.79	1878.43	0.11	--
1	33	17	-8783.91	0.12	21.83	1938.27	138.62	0.07	>1
2	33	17	-12006.1	0.17	15.97	1938.27	138.62	0.07	>1
1	35	18	-9115.94	0.13	--	1535.97	58.09	0.06	--

2	35	18	-11674.1	0.16	--	1535.97	58.09	0.06	--
1	37	19	-8836.62	0.12	21.7	2040.89	817.39	0.08	>1
2	37	19	-11953.4	0.16	16.04	2040.89	817.39	0.08	>1
1	39	20	-9161.24	0.13	--	1665.83	763.59	0.07	--
2	39	20	-11628.8	0.16	--	1665.83	763.59	0.07	--
1	41	21	-14243.9	0.2	13.46	4620.14	114.55	0.17	>1
2	41	21	-6546.07	0.09	29.3	4620.14	114.55	0.17	>1
1	43	22	-13808.7	0.19	--	4096.64	37.4	0.15	--
2	43	22	-6981.28	0.1	--	4096.64	37.4	0.15	--
1	45	23	-14296.6	0.2	13.41	4756.98	841.47	0.18	>1
2	45	23	-6493.36	0.09	29.53	4756.98	841.47	0.18	>1
1	47	24	-13854	0.19	--	4224.27	784.28	0.16	--
2	47	24	-6935.98	0.1	--	4224.27	784.28	0.16	--
1	49	25	-10633.4	0.15	18.03	1277.99	1245.55	0.06	>1
2	49	25	-10156.6	0.14	18.88	1277.99	1245.55	0.06	>1
1	51	26	-10705.6	0.15	--	1076.07	1009.47	0.05	--
2	51	26	-10084.4	0.14	--	1076.07	1009.47	0.05	--
1	53	27	-12271.4	0.17	15.63	2569.76	1238.32	0.11	>1
2	53	27	-8518.57	0.12	22.51	2569.76	1238.32	0.11	>1
1	55	28	-12113.4	0.17	--	2293.19	1003.26	0.09	--
2	55	28	-8676.6	0.12	--	2293.19	1003.26	0.09	--
1	57	29	-10809.1	0.15	17.74	2003.77	1941.17	0.09	>1
2	57	29	-9980.88	0.14	19.21	2003.77	1941.17	0.09	>1
1	59	30	-10856.6	0.15	--	1815.98	1729.45	0.08	--
2	59	30	-9933.43	0.14	--	1815.98	1729.45	0.08	--
1	61	31	-12447.1	0.17	15.41	3140.12	1948.39	0.13	>1
2	61	31	-8342.88	0.12	22.99	3140.12	1948.39	0.13	>1
1	63	32	-12264.4	0.17	--	2836.34	1735.66	0.12	--
2	63	32	-8525.6	0.12	--	2836.34	1735.66	0.12	--
1	65	33	-10578.1	0.15	18.13	1721.02	1062.74	0.07	>1
2	65	33	-8321.92	0.11	23.04	1721.02	1062.74	0.07	>1
1	67	34	-10983.7	0.15	17.46	2126.11	1064.53	0.09	>1
2	67	34	-7916.32	0.11	24.22	2126.11	1064.53	0.09	>1
1	69	35	-10774.4	0.15	17.8	1849.1	945.27	0.08	>1
2	69	35	-8125.65	0.11	23.6	1849.1	945.27	0.08	>1
1	71	36	-10787.4	0.15	17.78	1993.18	1182	0.08	>1
2	71	36	-8112.6	0.11	23.64	1993.18	1182	0.08	>1
1	73	37	-10200.5	0.14	--	1159.13	729.7	0.05	--
2	73	37	-8699.48	0.12	--	1159.13	729.7	0.05	--
1	75	38	-10606.1	0.15	--	1568.37	731.48	0.06	--
2	75	38	-8293.88	0.11	--	1568.37	731.48	0.06	--
1	77	39	-10396.8	0.14	--	1290.6	612.22	0.05	--
2	77	39	-8503.21	0.12	--	1290.6	612.22	0.05	--
1	79	40	-10409.8	0.14	--	1430.87	848.95	0.06	--
2	79	40	-8490.16	0.12	--	1430.87	848.95	0.06	--
1	81	41	-10007.8	0.14	--	829.48	489.98	0.04	--
2	81	41	-8892.25	0.12	--	829.48	489.98	0.04	--
1	83	42	-10413.4	0.14	--	1256.27	491.76	0.05	--
2	83	42	-8486.65	0.12	--	1256.27	491.76	0.05	--
1	85	43	-10204	0.14	--	978.51	372.51	0.04	--
2	85	43	-8695.97	0.12	--	978.51	372.51	0.04	--
1	87	44	-10217.1	0.14	--	1103.85	609.24	0.05	--
2	87	44	-8682.92	0.12	--	1103.85	609.24	0.05	--
1	89	45	-9930.64	0.14	--	698.55	394.09	0.03	--
2	89	45	-8969.36	0.12	--	698.55	394.09	0.03	--
1	91	46	-10336.2	0.14	--	1134.79	395.88	0.05	--
2	91	46	-8563.75	0.12	--	1134.79	395.88	0.05	--
1	93	47	-10126.9	0.14	--	858.11	276.62	0.03	--
2	93	47	-8773.08	0.12	--	858.11	276.62	0.03	--
1	95	48	-10140	0.14	--	974.19	513.35	0.04	--
2	95	48	-8760.03	0.12	--	974.19	513.35	0.04	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-7996.94	0.11	25.12	2877.8	27.5	0.11	>1
2	2	1	-12793.1	0.18	15.7	2877.8	27.5	0.11	>1
1	4	2	-8439.55	0.12	--	2348.06	84.69	0.09	--
2	4	2	-12350.4	0.17	--	2348.06	84.69	0.09	--
1	6	3	-8049.65	0.11	24.96	2981.32	983.51	0.12	>1
2	6	3	-12740.4	0.18	15.77	2981.32	983.51	0.12	>1
1	8	4	-8484.85	0.12	--	2464.87	906.36	0.1	--
2	8	4	-12305.1	0.17	--	2464.87	906.36	0.1	--
1	10	5	-13457	0.19	14.93	3674.71	51.57	0.13	>1
2	10	5	-7333.04	0.1	27.4	3674.71	51.57	0.13	>1
1	12	6	-13132.3	0.18	--	3286.5	105.37	0.12	--
2	12	6	-7657.66	0.11	--	3286.5	105.37	0.12	--

Relazione geotecnica

1	14	7	-13509.7	0.19	14.87	3871.03	1007.58	0.15	>1
2	14	7	-7280.33	0.1	27.6	3871.03	1007.58	0.15	>1
1	16	8	-13177.6	0.18	--	3465.47	927.05	0.14	--
2	16	8	-7612.36	0.1	--	3465.47	927.05	0.14	--
1	18	9	-9846.46	0.14	20.4	1264.3	1079.43	0.06	>1
2	18	9	-10943.5	0.15	18.36	1264.3	1079.43	0.06	>1
1	20	10	-10029.2	0.14	--	971.53	866.7	0.04	--
2	20	10	-10760.8	0.15	--	971.53	866.7	0.04	--
1	22	11	-11484.5	0.16	17.49	1690.8	1072.21	0.07	>1
2	22	11	-9305.54	0.13	21.59	1690.8	1072.21	0.07	>1
1	24	12	-11437	0.16	--	1517.89	860.49	0.06	--
2	24	12	-9352.99	0.13	--	1517.89	860.49	0.06	--
1	26	13	-10022.1	0.14	20.05	2154.26	2107.29	0.1	>1
2	26	13	-10767.9	0.15	18.66	2154.26	2107.29	0.1	>1
1	28	14	-10180.2	0.14	--	1889.89	1872.23	0.09	--
2	28	14	-10609.8	0.15	--	1889.89	1872.23	0.09	--
1	30	15	-11660.2	0.16	17.23	2603.08	2114.51	0.12	>1
2	30	15	-9129.85	0.13	22	2603.08	2114.51	0.12	>1
1	32	16	-11588	0.16	--	2361.79	1878.43	0.11	--
2	32	16	-9201.99	0.13	--	2361.79	1878.43	0.11	--
1	34	17	-8783.91	0.12	22.87	1938.27	138.62	0.07	>1
2	34	17	-12006.1	0.17	16.73	1938.27	138.62	0.07	>1
1	36	18	-9115.94	0.13	--	1535.97	58.09	0.06	--
2	36	18	-11674.1	0.16	--	1535.97	58.09	0.06	--
1	38	19	-8836.62	0.12	22.74	2040.89	817.39	0.08	>1
2	38	19	-11953.4	0.16	16.81	2040.89	817.39	0.08	>1
1	40	20	-9161.24	0.13	--	1665.83	763.59	0.07	--
2	40	20	-11628.8	0.16	--	1665.83	763.59	0.07	--
1	42	21	-14243.9	0.2	14.1	4620.14	114.55	0.17	>1
2	42	21	-6546.07	0.09	30.69	4620.14	114.55	0.17	>1
1	44	22	-13808.7	0.19	--	4096.64	37.4	0.15	--
2	44	22	-6981.28	0.1	--	4096.64	37.4	0.15	--
1	46	23	-14296.6	0.2	14.05	4756.98	841.47	0.18	>1
2	46	23	-6493.36	0.09	30.94	4756.98	841.47	0.18	>1
1	48	24	-13854	0.19	--	4224.27	784.28	0.16	--
2	48	24	-6935.98	0.1	--	4224.27	784.28	0.16	--
1	50	25	-10633.4	0.15	18.89	1277.99	1245.55	0.06	>1
2	50	25	-10156.6	0.14	19.78	1277.99	1245.55	0.06	>1
1	52	26	-10705.6	0.15	--	1076.07	1009.47	0.05	--
2	52	26	-10084.4	0.14	--	1076.07	1009.47	0.05	--
1	54	27	-12271.4	0.17	16.37	2569.76	1238.32	0.11	>1
2	54	27	-8518.57	0.12	23.58	2569.76	1238.32	0.11	>1
1	56	28	-12113.4	0.17	--	2293.19	1003.26	0.09	--
2	56	28	-8676.6	0.12	--	2293.19	1003.26	0.09	--
1	58	29	-10809.1	0.15	18.59	2003.77	1941.17	0.09	>1
2	58	29	-9980.88	0.14	20.13	2003.77	1941.17	0.09	>1
1	60	30	-10856.6	0.15	--	1815.98	1729.45	0.08	--
2	60	30	-9933.43	0.14	--	1815.98	1729.45	0.08	--
1	62	31	-12447.1	0.17	16.14	3140.12	1948.39	0.13	>1
2	62	31	-8342.88	0.12	24.08	3140.12	1948.39	0.13	>1
1	64	32	-12264.4	0.17	--	2836.34	1735.66	0.12	--
2	64	32	-8525.6	0.12	--	2836.34	1735.66	0.12	--
1	66	33	-10578.1	0.15	18.99	1721.02	1062.74	0.07	>1
2	66	33	-8321.92	0.11	24.14	1721.02	1062.74	0.07	>1
1	68	34	-10983.7	0.15	18.29	2126.11	1064.53	0.09	>1
2	68	34	-7916.32	0.11	25.38	2126.11	1064.53	0.09	>1
1	70	35	-10774.4	0.15	18.65	1849.1	945.27	0.08	>1
2	70	35	-8125.65	0.11	24.72	1849.1	945.27	0.08	>1
1	72	36	-10787.4	0.15	18.62	1993.18	1182	0.08	>1
2	72	36	-8112.6	0.11	24.76	1993.18	1182	0.08	>1
1	74	37	-10200.5	0.14	--	1159.13	729.7	0.05	--
2	74	37	-8699.48	0.12	--	1159.13	729.7	0.05	--
1	76	38	-10606.1	0.15	--	1568.37	731.48	0.06	--
2	76	38	-8293.88	0.11	--	1568.37	731.48	0.06	--
1	78	39	-10396.8	0.14	--	1290.6	612.22	0.05	--
2	78	39	-8503.21	0.12	--	1290.6	612.22	0.05	--
1	80	40	-10409.8	0.14	--	1430.87	848.95	0.06	--
2	80	40	-8490.16	0.12	--	1430.87	848.95	0.06	--
1	82	41	-10007.8	0.14	--	829.48	489.98	0.04	--
2	82	41	-8892.25	0.12	--	829.48	489.98	0.04	--
1	84	42	-10413.4	0.14	--	1256.27	491.76	0.05	--
2	84	42	-8486.65	0.12	--	1256.27	491.76	0.05	--
1	86	43	-10204	0.14	--	978.51	372.51	0.04	--
2	86	43	-8695.97	0.12	--	978.51	372.51	0.04	--
1	88	44	-10217.1	0.14	--	1103.85	609.24	0.05	--
2	88	44	-8682.92	0.12	--	1103.85	609.24	0.05	--
1	90	45	-9930.64	0.14	--	698.55	394.09	0.03	--
2	90	45	-8969.36	0.12	--	698.55	394.09	0.03	--
1	92	46	-10336.2	0.14	--	1134.79	395.88	0.05	--

Relazione geotecnica

2	92	46	-8563.75	0.12	--	1134.79	395.88	0.05	--
1	94	47	-10126.9	0.14	--	858.11	276.62	0.03	--
2	94	47	-8773.08	0.12	--	858.11	276.62	0.03	--
1	96	48	-10140	0.14	--	974.19	513.35	0.04	--
2	96	48	-8760.03	0.12	--	974.19	513.35	0.04	--

Plinto n. 4

Tipo palo=Trivellato

Rotazione testa libera

Coefficiente di efficienza=1.00

Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>

Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	-1.2	0
2	1.2	0

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{lim}=252333.00 <daN>

q_p=28.63 <daN/cm²>

QP_{lim}=143893.00 <daN>

k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>

q_p=16.60 <daN/cm²>

QP_{lim}=83431.40 <daN>

k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-7696.69	0.11	24.92	3238.33	48.01	0.12	>1
2	1	1	-13093.3	0.18	14.65	3238.33	48.01	0.12	>1
1	3	2	-8152.47	0.11	--	2691.14	23.28	0.1	--
2	3	2	-12637.5	0.17	--	2691.14	23.28	0.1	--
1	5	3	-7759.89	0.11	24.71	3292.68	917.98	0.13	>1
2	5	3	-13030.1	0.18	14.72	3292.68	917.98	0.13	>1
1	7	4	-8206.8	0.11	--	2761.08	853.54	0.11	--
2	7	4	-12583.2	0.17	--	2761.08	853.54	0.11	--
1	9	5	-13320.9	0.18	14.4	3511.1	19.49	0.13	>1
2	9	5	-7469.13	0.1	25.67	3511.1	19.49	0.13	>1
1	11	6	-12986.4	0.18	--	3109.99	47.8	0.11	--
2	11	6	-7803.65	0.11	--	3109.99	47.8	0.11	--
1	13	7	-13384.1	0.18	14.33	3709.67	946.51	0.15	>1
2	13	7	-7405.92	0.1	25.89	3709.67	946.51	0.15	>1
1	15	8	-13040.7	0.18	--	3294	878.05	0.13	--
2	15	8	-7749.32	0.11	--	3294	878.05	0.13	--
1	17	9	-9591.41	0.13	19.99	1512.34	1165.03	0.07	>1
2	17	9	-11198.6	0.15	17.12	1512.34	1165.03	0.07	>1
1	19	10	-9780.95	0.13	--	1191.85	936.77	0.05	--
2	19	10	-11009.1	0.15	--	1191.85	936.77	0.05	--
1	21	11	-11278.7	0.16	17	1569.03	1156.47	0.07	>1
2	21	11	-9511.34	0.13	20.16	1569.03	1156.47	0.07	>1
1	23	12	-11231.1	0.15	--	1367.66	929.42	0.06	--
2	23	12	-9558.89	0.13	--	1367.66	929.42	0.06	--
1	25	13	-9802.1	0.14	19.56	2174.64	2054.96	0.1	>1
2	25	13	-10987.9	0.15	17.45	2174.64	2054.96	0.1	>1
1	27	14	-9962.04	0.14	--	1903.04	1830.75	0.09	--
2	27	14	-10828	0.15	--	1903.04	1830.75	0.09	--
1	29	15	-11489.4	0.16	16.69	2445.95	2063.52	0.11	>1
2	29	15	-9300.65	0.13	20.62	2445.95	2063.52	0.11	>1

Relazione geotecnica

1	31	16	-11412.2	0.16	--	2206.49	1838.1	0.1	--
2	31	16	-9377.8	0.13	--	2206.49	1838.1	0.1	--
1	33	17	-8496.51	0.12	22.57	2278.35	27.83	0.08	>1
2	33	17	-12293.5	0.17	15.6	2278.35	27.83	0.08	>1
1	35	18	-8839.91	0.12	--	1866.55	40.63	0.07	--
2	35	18	-11950.1	0.16	--	1866.55	40.63	0.07	--
1	37	19	-8559.72	0.12	22.4	2393.83	938.17	0.1	>1
2	37	19	-12230.3	0.17	15.68	2393.83	938.17	0.1	>1
1	39	20	-8894.24	0.12	--	2000.43	870.88	0.08	--
2	39	20	-11895.8	0.16	--	2000.43	870.88	0.08	--
1	41	21	-14120.7	0.19	13.58	4470.84	0.69	0.16	>1
2	41	21	-6669.3	0.09	28.75	4470.84	0.69	0.16	>1
1	43	22	-13673.8	0.19	--	3935.09	65.14	0.14	--
2	43	22	-7116.21	0.1	--	3935.09	65.14	0.14	--
1	45	23	-14183.9	0.2	13.52	4648.32	966.69	0.18	>1
2	45	23	-6606.1	0.09	29.03	4648.32	966.69	0.18	>1
1	47	24	-13728.1	0.19	--	4098.74	895.4	0.16	--
2	47	24	-7061.88	0.1	--	4098.74	895.4	0.16	--
1	49	25	-10391.2	0.14	18.45	1144.85	1144.84	0.05	>1
2	49	25	-10398.8	0.14	18.44	1144.85	1144.84	0.05	>1
1	51	26	-10468.4	0.14	--	923.63	919.42	0.04	--
2	51	26	-10321.6	0.14	--	923.63	919.42	0.04	--
1	53	27	-12078.5	0.17	15.88	2317.82	1136.28	0.1	>1
2	53	27	-8711.51	0.12	22.01	2317.82	1136.28	0.1	>1
1	55	28	-11918.6	0.16	--	2043.14	912.07	0.08	--
2	55	28	-8871.45	0.12	--	2043.14	912.07	0.08	--
1	57	29	-10601.9	0.15	18.09	2089.95	2075.15	0.1	>1
2	57	29	-10188.1	0.14	18.82	2089.95	2075.15	0.1	>1
1	59	30	-10649.5	0.15	--	1873.16	1848.1	0.09	--
2	59	30	-10140.5	0.14	--	1873.16	1848.1	0.09	--
1	61	31	-12289.2	0.17	15.6	3083.58	2083.7	0.13	>1
2	61	31	-8500.82	0.12	22.56	3083.58	2083.7	0.13	>1
1	63	32	-12099.6	0.17	--	2761.71	1855.45	0.12	--
2	63	32	-8690.36	0.12	--	2761.71	1855.45	0.12	--
1	65	33	-10176.2	0.14	18.84	1406.37	1103.85	0.06	>1
2	65	33	-8723.8	0.12	21.98	1406.37	1103.85	0.06	>1
1	67	34	-10594	0.15	18.1	1762.88	1105.97	0.08	>1
2	67	34	-8306.01	0.11	23.09	1762.88	1105.97	0.08	>1
1	69	35	-10377.3	0.14	18.48	1486.27	985.31	0.06	>1
2	69	35	-8522.73	0.12	22.5	1486.27	985.31	0.06	>1
1	71	36	-10392.9	0.14	18.45	1667.25	1224.51	0.07	>1
2	71	36	-8507.08	0.12	22.54	1667.25	1224.51	0.07	>1
1	73	37	-9914.13	0.14	--	941.74	759.39	0.04	--
2	73	37	-8985.87	0.12	--	941.74	759.39	0.04	--
1	75	38	-10331.9	0.14	--	1303.81	761.5	0.06	--
2	75	38	-8568.07	0.12	--	1303.81	761.5	0.06	--
1	77	39	-10115.2	0.14	--	1023.66	640.85	0.04	--
2	77	39	-8784.8	0.12	--	1023.66	640.85	0.04	--
1	79	40	-10130.9	0.14	--	1200.84	880.05	0.05	--
2	79	40	-8769.15	0.12	--	1200.84	880.05	0.05	--
1	81	41	-9787.48	0.13	--	654.75	514.48	0.03	--
2	81	41	-9112.52	0.13	--	654.75	514.48	0.03	--
1	83	42	-10205.3	0.14	--	1043.23	516.6	0.04	--
2	83	42	-8694.72	0.12	--	1043.23	516.6	0.04	--
1	85	43	-9988.56	0.14	--	757.91	395.94	0.03	--
2	85	43	-8911.45	0.12	--	757.91	395.94	0.03	--
1	87	44	-10004.2	0.14	--	919.62	635.14	0.04	--
2	87	44	-8895.79	0.12	--	919.62	635.14	0.04	--
1	89	45	-9736.82	0.13	--	540.33	416.52	0.02	--
2	89	45	-9163.18	0.13	--	540.33	416.52	0.02	--
1	91	46	-10154.6	0.14	--	943.51	418.64	0.04	--
2	91	46	-8745.38	0.12	--	943.51	418.64	0.04	--
1	93	47	-9937.9	0.14	--	656.94	297.98	0.03	--
2	93	47	-8962.1	0.12	--	656.94	297.98	0.03	--
1	95	48	-9953.55	0.14	--	808.51	537.18	0.03	--
2	95	48	-8946.45	0.12	--	808.51	537.18	0.03	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-7696.69	0.11	26.1	3238.33	48.01	0.12	>1
2	2	1	-13093.3	0.18	15.34	3238.33	48.01	0.12	>1
1	4	2	-8152.47	0.11	--	2691.14	23.28	0.1	--
2	4	2	-12637.5	0.17	--	2691.14	23.28	0.1	--
1	6	3	-7759.89	0.11	25.89	3292.68	917.98	0.13	>1
2	6	3	-13030.1	0.18	15.42	3292.68	917.98	0.13	>1
1	8	4	-8206.8	0.11	--	2761.08	853.54	0.11	--

Relazione geotecnica

2	8	4	-12583.2	0.17	--	2761.08	853.54	0.11	--
1	10	5	-13320.9	0.18	15.08	3511.1	19.49	0.13	>1
2	10	5	-7469.13	0.1	26.9	3511.1	19.49	0.13	>1
1	12	6	-12986.4	0.18	--	3109.99	47.8	0.11	--
2	12	6	-7803.65	0.11	--	3109.99	47.8	0.11	--
1	14	7	-13384.1	0.18	15.01	3709.67	946.51	0.15	>1
2	14	7	-7405.92	0.1	27.13	3709.67	946.51	0.15	>1
1	16	8	-13040.7	0.18	--	3294	878.05	0.13	--
2	16	8	-7749.32	0.11	--	3294	878.05	0.13	--
1	18	9	-9591.41	0.13	20.95	1512.34	1165.03	0.07	>1
2	18	9	-11198.6	0.15	17.94	1512.34	1165.03	0.07	>1
1	20	10	-9780.95	0.13	--	1191.85	936.77	0.05	--
2	20	10	-11009.1	0.15	--	1191.85	936.77	0.05	--
1	22	11	-11278.7	0.16	17.81	1569.03	1156.47	0.07	>1
2	22	11	-9511.34	0.13	21.12	1569.03	1156.47	0.07	>1
1	24	12	-11231.1	0.15	--	1367.66	929.42	0.06	--
2	24	12	-9558.89	0.13	--	1367.66	929.42	0.06	--
1	26	13	-9802.1	0.14	20.5	2174.64	2054.96	0.1	>1
2	26	13	-10987.9	0.15	18.28	2174.64	2054.96	0.1	>1
1	28	14	-9962.04	0.14	--	1903.04	1830.75	0.09	--
2	28	14	-10828	0.15	--	1903.04	1830.75	0.09	--
1	30	15	-11489.4	0.16	17.49	2445.95	2063.52	0.11	>1
2	30	15	-9300.65	0.13	21.6	2445.95	2063.52	0.11	>1
1	32	16	-11412.2	0.16	--	2206.49	1838.1	0.1	--
2	32	16	-9377.8	0.13	--	2206.49	1838.1	0.1	--
1	34	17	-8496.51	0.12	23.65	2278.35	27.83	0.08	>1
2	34	17	-12293.5	0.17	16.34	2278.35	27.83	0.08	>1
1	36	18	-8839.91	0.12	--	1866.55	40.63	0.07	--
2	36	18	-11950.1	0.16	--	1866.55	40.63	0.07	--
1	38	19	-8559.72	0.12	23.47	2393.83	938.17	0.1	>1
2	38	19	-12230.3	0.17	16.43	2393.83	938.17	0.1	>1
1	40	20	-8894.24	0.12	--	2000.43	870.88	0.08	--
2	40	20	-11895.8	0.16	--	2000.43	870.88	0.08	--
1	42	21	-14120.7	0.19	14.23	4470.84	0.69	0.16	>1
2	42	21	-6669.3	0.09	30.12	4470.84	0.69	0.16	>1
1	44	22	-13673.8	0.19	--	3935.09	65.14	0.14	--
2	44	22	-7116.21	0.1	--	3935.09	65.14	0.14	--
1	46	23	-14183.9	0.2	14.16	4648.32	966.69	0.18	>1
2	46	23	-6606.1	0.09	30.41	4648.32	966.69	0.18	>1
1	48	24	-13728.1	0.19	--	4098.74	895.4	0.16	--
2	48	24	-7061.88	0.1	--	4098.74	895.4	0.16	--
1	50	25	-10391.2	0.14	19.33	1144.85	1144.84	0.05	>1
2	50	25	-10398.8	0.14	19.32	1144.85	1144.84	0.05	>1
1	52	26	-10468.4	0.14	--	923.63	919.42	0.04	--
2	52	26	-10321.6	0.14	--	923.63	919.42	0.04	--
1	54	27	-12078.5	0.17	16.63	2317.82	1136.28	0.1	>1
2	54	27	-8711.51	0.12	23.06	2317.82	1136.28	0.1	>1
1	56	28	-11918.6	0.16	--	2043.14	912.07	0.08	--
2	56	28	-8871.45	0.12	--	2043.14	912.07	0.08	--
1	58	29	-10601.9	0.15	18.95	2089.95	2075.15	0.1	>1
2	58	29	-10188.1	0.14	19.72	2089.95	2075.15	0.1	>1
1	60	30	-10649.5	0.15	--	1873.16	1848.1	0.09	--
2	60	30	-10140.5	0.14	--	1873.16	1848.1	0.09	--
1	62	31	-12289.2	0.17	16.35	3083.58	2083.7	0.13	>1
2	62	31	-8500.82	0.12	23.63	3083.58	2083.7	0.13	>1
1	64	32	-12099.6	0.17	--	2761.71	1855.45	0.12	--
2	64	32	-8690.36	0.12	--	2761.71	1855.45	0.12	--
1	66	33	-10176.2	0.14	19.74	1406.37	1103.85	0.06	>1
2	66	33	-8723.8	0.12	23.03	1406.37	1103.85	0.06	>1
1	68	34	-10594	0.15	18.96	1762.88	1105.97	0.08	>1
2	68	34	-8306.01	0.11	24.19	1762.88	1105.97	0.08	>1
1	70	35	-10377.3	0.14	19.36	1486.27	985.31	0.06	>1
2	70	35	-8522.73	0.12	23.57	1486.27	985.31	0.06	>1
1	72	36	-10392.9	0.14	19.33	1667.25	1224.51	0.07	>1
2	72	36	-8507.08	0.12	23.62	1667.25	1224.51	0.07	>1
1	74	37	-9914.13	0.14	--	941.74	759.39	0.04	--
2	74	37	-8985.87	0.12	--	941.74	759.39	0.04	--
1	76	38	-10331.9	0.14	--	1303.81	761.5	0.06	--
2	76	38	-8568.07	0.12	--	1303.81	761.5	0.06	--
1	78	39	-10115.2	0.14	--	1023.66	640.85	0.04	--
2	78	39	-8784.8	0.12	--	1023.66	640.85	0.04	--
1	80	40	-10130.9	0.14	--	1200.84	880.05	0.05	--
2	80	40	-8769.15	0.12	--	1200.84	880.05	0.05	--
1	82	41	-9787.48	0.13	--	654.75	514.48	0.03	--
2	82	41	-9112.52	0.13	--	654.75	514.48	0.03	--
1	84	42	-10205.3	0.14	--	1043.23	516.6	0.04	--
2	84	42	-8694.72	0.12	--	1043.23	516.6	0.04	--
1	86	43	-9988.56	0.14	--	757.91	395.94	0.03	--
2	86	43	-8911.45	0.12	--	757.91	395.94	0.03	--

Relazione geotecnica

1	88	44	-10004.2	0.14	--	919.62	635.14	0.04	--
2	88	44	-8895.79	0.12	--	919.62	635.14	0.04	--
1	90	45	-9736.82	0.13	--	540.33	416.52	0.02	--
2	90	45	-9163.18	0.13	--	540.33	416.52	0.02	--
1	92	46	-10154.6	0.14	--	943.51	418.64	0.04	--
2	92	46	-8745.38	0.12	--	943.51	418.64	0.04	--
1	94	47	-9937.9	0.14	--	656.94	297.98	0.03	--
2	94	47	-8962.1	0.12	--	656.94	297.98	0.03	--
1	96	48	-9953.55	0.14	--	808.51	537.18	0.03	--
2	96	48	-8946.45	0.12	--	808.51	537.18	0.03	--

Plinto n. 5

Tipo palo=Trivellato

Rotazione testa libera

Coefficiente di efficienza=1.00

Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>

Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	-1.2	0
2	1.2	0

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{lim}=252333.00 <daN>

q_p=28.63 <daN/cm²>

QP_{lim}=143893.00 <daN>

k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>

q_p=16.60 <daN/cm²>

QP_{lim}=83431.40 <daN>

k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-7376.36	0.1	26	3625.82	158.31	0.13	>1
2	1	1	-13413.6	0.18	14.3	3625.82	158.31	0.13	>1
1	3	2	-7821.64	0.11	--	3088.89	72.79	0.11	--
2	3	2	-12968.4	0.18	--	3088.89	72.79	0.11	--
1	5	3	-7430.16	0.1	25.81	3650.93	819.27	0.14	>1
2	5	3	-13359.8	0.18	14.35	3650.93	819.27	0.14	>1
1	7	4	-7867.87	0.11	--	3128.15	767.42	0.12	--
2	7	4	-12922.1	0.18	--	3128.15	767.42	0.12	--
1	9	5	-12882.8	0.18	14.89	2988.12	129.02	0.11	>1
2	9	5	-7907.22	0.11	24.25	2988.12	129.02	0.11	>1
1	11	6	-12554.3	0.17	--	2591.6	47.62	0.1	--
2	11	6	-8235.7	0.11	--	2591.6	47.62	0.1	--
1	13	7	-12936.6	0.18	14.82	3165.73	848.56	0.12	>1
2	13	7	-7853.43	0.11	24.42	3165.73	848.56	0.12	>1
1	15	8	-12600.5	0.17	--	2762.78	792.6	0.11	--
2	15	8	-8189.46	0.11	--	2762.78	792.6	0.11	--
1	17	9	-9240.85	0.13	20.75	1891.71	1288.57	0.08	>1
2	17	9	-11549.1	0.16	16.6	1891.71	1288.57	0.08	>1
1	19	10	-9424.14	0.13	--	1564.52	1044.23	0.07	--
2	19	10	-11365.9	0.16	--	1564.52	1044.23	0.07	--
1	21	11	-10892.8	0.15	17.61	1412.33	1279.79	0.06	>1
2	21	11	-9897.22	0.14	19.38	1412.33	1279.79	0.06	>1
1	23	12	-10843.9	0.15	--	1168.3	1036.68	0.05	--
2	23	12	-9946.07	0.14	--	1168.3	1036.68	0.05	--
1	25	13	-9420.16	0.13	20.36	2291.18	1970.04	0.1	>1

Relazione geotecnica

2	25	13	-11369.8	0.16	16.87	2291.18	1970.04	0.1	>1
1	27	14	-9578.25	0.13	--	2011.43	1756.49	0.09	--
2	27	14	-11211.8	0.15	--	2011.43	1756.49	0.09	--
1	29	15	-11072.1	0.15	17.32	2139.14	1978.82	0.1	>1
2	29	15	-9717.92	0.13	19.73	2139.14	1978.82	0.1	>1
1	31	16	-10998	0.15	--	1906.7	1764.04	0.09	--
2	31	16	-9791.96	0.14	--	1906.7	1764.04	0.09	--
1	33	17	-8153.79	0.11	23.52	2689.96	52.01	0.1	>1
2	33	17	-12636.2	0.17	15.18	2689.96	52.01	0.1	>1
1	35	18	-8489.82	0.12	--	2288.76	107.97	0.08	--
2	35	18	-12300.2	0.17	--	2288.76	107.97	0.08	--
1	37	19	-8207.58	0.11	23.36	2819.61	1029.59	0.11	>1
2	37	19	-12582.4	0.17	15.24	2819.61	1029.59	0.11	>1
1	39	20	-8536.06	0.12	--	2423.89	948.19	0.1	--
2	39	20	-12253.9	0.17	--	2423.89	948.19	0.1	--
1	41	21	-13660.2	0.19	14.04	3919.09	81.29	0.14	>1
2	41	21	-7129.79	0.1	26.9	3919.09	81.29	0.14	>1
1	43	22	-13222.5	0.18	--	3395.6	133.14	0.13	--
2	43	22	-7567.51	0.1	--	3395.6	133.14	0.13	--
1	45	23	-13714	0.19	13.98	4121.15	1058.88	0.16	>1
2	45	23	-7076	0.1	27.1	4121.15	1058.88	0.16	>1
1	47	24	-13268.7	0.18	--	3583.2	973.36	0.14	--
2	47	24	-7521.28	0.1	--	3583.2	973.36	0.14	--
1	49	25	-10018.3	0.14	19.14	1169.19	1078.26	0.05	>1
2	49	25	-10771.7	0.15	17.8	1169.19	1078.26	0.05	>1
1	51	26	-10092.3	0.14	--	936.75	863.47	0.04	--
2	51	26	-10697.7	0.15	--	936.75	863.47	0.04	--
1	53	27	-11670.2	0.16	16.43	1866.93	1069.47	0.08	>1
2	53	27	-9119.8	0.13	21.03	1866.93	1069.47	0.08	>1
1	55	28	-11512.1	0.16	--	1590.48	855.92	0.07	--
2	55	28	-9277.88	0.13	--	1590.48	855.92	0.07	--
1	57	29	-10197.6	0.14	18.81	2193.19	2180.36	0.1	>1
2	57	29	-10592.4	0.15	18.1	2193.19	2180.36	0.1	>1
1	59	30	-10246.4	0.14	--	1945.44	1937.25	0.09	--
2	59	30	-10543.6	0.15	--	1945.44	1937.25	0.09	--
1	61	31	-11849.5	0.16	16.18	2799.79	2189.14	0.12	>1
2	61	31	-8940.49	0.12	21.45	2799.79	2189.14	0.12	>1
1	63	32	-11666.2	0.16	--	2471.7	1944.8	0.11	--
2	63	32	-9123.77	0.13	--	2471.7	1944.8	0.11	--
1	65	33	-9474.5	0.13	20.24	1084.54	1084.14	0.05	>1
2	65	33	-9425.5	0.13	20.35	1084.54	1084.14	0.05	>1
1	67	34	-9883.55	0.14	19.4	1204.47	1086.32	0.05	>1
2	67	34	-9016.45	0.12	21.27	1204.47	1086.32	0.05	>1
1	69	35	-9672.37	0.13	19.83	1000.44	964.19	0.05	>1
2	69	35	-9227.64	0.13	20.78	1000.44	964.19	0.05	>1
1	71	36	-9685.69	0.13	19.8	1238.97	1206.26	0.06	>1
2	71	36	-9214.32	0.13	20.81	1238.97	1206.26	0.06	>1
1	73	37	-9413.44	0.13	--	746.94	745.65	0.03	--
2	73	37	-9486.56	0.13	--	746.94	745.65	0.03	--
1	75	38	-9822.49	0.14	--	871.23	747.82	0.04	--
2	75	38	-9077.51	0.13	--	871.23	747.82	0.04	--
1	77	39	-9611.31	0.13	--	654.96	625.7	0.03	--
2	77	39	-9288.69	0.13	--	654.96	625.7	0.03	--
1	79	40	-9624.63	0.13	--	892.72	867.77	0.04	--
2	79	40	-9275.37	0.13	--	892.72	867.77	0.04	--
1	81	41	-9390.99	0.13	--	509.6	504.66	0.02	--
2	81	41	-9509.02	0.13	--	509.6	504.66	0.02	--
1	83	42	-9800.04	0.14	--	658.27	506.83	0.03	--
2	83	42	-9099.97	0.13	--	658.27	506.83	0.03	--
1	85	43	-9588.85	0.13	--	419.24	384.71	0.02	--
2	85	43	-9311.15	0.13	--	419.24	384.71	0.02	--
1	87	44	-9602.17	0.13	--	652.84	626.78	0.03	--
2	87	44	-9297.83	0.13	--	652.84	626.78	0.03	--
1	89	45	-9382	0.13	--	416.33	408.26	0.02	--
2	89	45	-9518	0.13	--	416.33	408.26	0.02	--
1	91	46	-9791.05	0.13	--	579.62	410.44	0.03	--
2	91	46	-9108.95	0.13	--	579.62	410.44	0.03	--
1	93	47	-9579.87	0.13	--	327.74	288.31	0.01	--
2	93	47	-9320.13	0.13	--	327.74	288.31	0.01	--
1	95	48	-9593.19	0.13	--	557.52	530.38	0.03	--
2	95	48	-9306.81	0.13	--	557.52	530.38	0.03	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-7376.36	0.1	27.24	3625.82	158.31	0.13	>1
2	2	1	-13413.6	0.18	14.98	3625.82	158.31	0.13	>1

Relazione geotecnica

1	4	2	-7821.64	0.11	--	3088.89	72.79	0.11	--
2	4	2	-12968.4	0.18	--	3088.89	72.79	0.11	--
1	6	3	-7430.16	0.1	27.04	3650.93	819.27	0.14	>1
2	6	3	-13359.8	0.18	15.04	3650.93	819.27	0.14	>1
1	8	4	-7867.87	0.11	--	3128.15	767.42	0.12	--
2	8	4	-12922.1	0.18	--	3128.15	767.42	0.12	--
1	10	5	-12882.8	0.18	15.59	2988.12	129.02	0.11	>1
2	10	5	-7907.22	0.11	25.41	2988.12	129.02	0.11	>1
1	12	6	-12554.3	0.17	--	2591.6	47.62	0.1	--
2	12	6	-8235.7	0.11	--	2591.6	47.62	0.1	--
1	14	7	-12936.6	0.18	15.53	3165.73	848.56	0.12	>1
2	14	7	-7853.43	0.11	25.58	3165.73	848.56	0.12	>1
1	16	8	-12600.5	0.17	--	2762.78	792.6	0.11	--
2	16	8	-8189.46	0.11	--	2762.78	792.6	0.11	--
1	18	9	-9240.85	0.13	21.74	1891.71	1288.57	0.08	>1
2	18	9	-11549.1	0.16	17.4	1891.71	1288.57	0.08	>1
1	20	10	-9424.14	0.13	--	1564.52	1044.23	0.07	--
2	20	10	-11365.9	0.16	--	1564.52	1044.23	0.07	--
1	22	11	-10892.8	0.15	18.44	1412.33	1279.79	0.06	>1
2	22	11	-9897.22	0.14	20.3	1412.33	1279.79	0.06	>1
1	24	12	-10843.9	0.15	--	1168.3	1036.68	0.05	--
2	24	12	-9946.07	0.14	--	1168.3	1036.68	0.05	--
1	26	13	-9420.16	0.13	21.33	2291.18	1970.04	0.1	>1
2	26	13	-11369.8	0.16	17.67	2291.18	1970.04	0.1	>1
1	28	14	-9578.25	0.13	--	2011.43	1756.49	0.09	--
2	28	14	-11211.8	0.15	--	2011.43	1756.49	0.09	--
1	30	15	-11072.1	0.15	18.14	2139.14	1978.82	0.1	>1
2	30	15	-9717.92	0.13	20.67	2139.14	1978.82	0.1	>1
1	32	16	-10998	0.15	--	1906.7	1764.04	0.09	--
2	32	16	-9791.96	0.14	--	1906.7	1764.04	0.09	--
1	34	17	-8153.79	0.11	24.64	2689.96	52.01	0.1	>1
2	34	17	-12636.2	0.17	15.9	2689.96	52.01	0.1	>1
1	36	18	-8489.82	0.12	--	2288.76	107.97	0.08	--
2	36	18	-12300.2	0.17	--	2288.76	107.97	0.08	--
1	38	19	-8207.58	0.11	24.48	2819.61	1029.59	0.11	>1
2	38	19	-12582.4	0.17	15.97	2819.61	1029.59	0.11	>1
1	40	20	-8536.06	0.12	--	2423.89	948.19	0.1	--
2	40	20	-12253.9	0.17	--	2423.89	948.19	0.1	--
1	42	21	-13660.2	0.19	14.71	3919.09	81.29	0.14	>1
2	42	21	-7129.79	0.1	28.18	3919.09	81.29	0.14	>1
1	44	22	-13222.5	0.18	--	3395.6	133.14	0.13	--
2	44	22	-7567.51	0.1	--	3395.6	133.14	0.13	--
1	46	23	-13714	0.19	14.65	4121.15	1058.88	0.16	>1
2	46	23	-7076	0.1	28.39	4121.15	1058.88	0.16	>1
1	48	24	-13268.7	0.18	--	3583.2	973.36	0.14	--
2	48	24	-7521.28	0.1	--	3583.2	973.36	0.14	--
1	50	25	-10018.3	0.14	20.05	1169.19	1078.26	0.05	>1
2	50	25	-10771.7	0.15	18.65	1169.19	1078.26	0.05	>1
1	52	26	-10092.3	0.14	--	936.75	863.47	0.04	--
2	52	26	-10697.7	0.15	--	936.75	863.47	0.04	--
1	54	27	-11670.2	0.16	17.21	1866.93	1069.47	0.08	>1
2	54	27	-9119.8	0.13	22.03	1866.93	1069.47	0.08	>1
1	56	28	-11512.1	0.16	--	1590.48	855.92	0.07	--
2	56	28	-9277.88	0.13	--	1590.48	855.92	0.07	--
1	58	29	-10197.6	0.14	19.7	2193.19	2180.36	0.1	>1
2	58	29	-10592.4	0.15	18.97	2193.19	2180.36	0.1	>1
1	60	30	-10246.4	0.14	--	1945.44	1937.25	0.09	--
2	60	30	-10543.6	0.15	--	1945.44	1937.25	0.09	--
1	62	31	-11849.5	0.16	16.95	2799.79	2189.14	0.12	>1
2	62	31	-8940.49	0.12	22.47	2799.79	2189.14	0.12	>1
1	64	32	-11666.2	0.16	--	2471.7	1944.8	0.11	--
2	64	32	-9123.77	0.13	--	2471.7	1944.8	0.11	--
1	66	33	-9474.5	0.13	21.2	1084.54	1084.14	0.05	>1
2	66	33	-9425.5	0.13	21.31	1084.54	1084.14	0.05	>1
1	68	34	-9883.55	0.14	20.33	1204.47	1086.32	0.05	>1
2	68	34	-9016.45	0.12	22.28	1204.47	1086.32	0.05	>1
1	70	35	-9672.37	0.13	20.77	1000.44	964.19	0.05	>1
2	70	35	-9227.64	0.13	21.77	1000.44	964.19	0.05	>1
1	72	36	-9685.69	0.13	20.74	1238.97	1206.26	0.06	>1
2	72	36	-9214.32	0.13	21.8	1238.97	1206.26	0.06	>1
1	74	37	-9413.44	0.13	--	746.94	745.65	0.03	--
2	74	37	-9486.56	0.13	--	746.94	745.65	0.03	--
1	76	38	-9822.49	0.14	--	871.23	747.82	0.04	--
2	76	38	-9077.51	0.13	--	871.23	747.82	0.04	--
1	78	39	-9611.31	0.13	--	654.96	625.7	0.03	--
2	78	39	-9288.69	0.13	--	654.96	625.7	0.03	--
1	80	40	-9624.63	0.13	--	892.72	867.77	0.04	--
2	80	40	-9275.37	0.13	--	892.72	867.77	0.04	--
1	82	41	-9390.99	0.13	--	509.6	504.66	0.02	--

Relazione geotecnica

2	82	41	-9509.02	0.13	--	509.6	504.66	0.02	--
1	84	42	-9800.04	0.14	--	658.27	506.83	0.03	--
2	84	42	-9099.97	0.13	--	658.27	506.83	0.03	--
1	86	43	-9588.85	0.13	--	419.24	384.71	0.02	--
2	86	43	-9311.15	0.13	--	419.24	384.71	0.02	--
1	88	44	-9602.17	0.13	--	652.84	626.78	0.03	--
2	88	44	-9297.83	0.13	--	652.84	626.78	0.03	--
1	90	45	-9382	0.13	--	416.33	408.26	0.02	--
2	90	45	-9518	0.13	--	416.33	408.26	0.02	--
1	92	46	-9791.05	0.13	--	579.62	410.44	0.03	--
2	92	46	-9108.95	0.13	--	579.62	410.44	0.03	--
1	94	47	-9579.87	0.13	--	327.74	288.31	0.01	--
2	94	47	-9320.13	0.13	--	327.74	288.31	0.01	--
1	96	48	-9593.19	0.13	--	557.52	530.38	0.03	--
2	96	48	-9306.81	0.13	--	557.52	530.38	0.03	--

Plinto n. 6

Tipo palo=Trivellato
 Rotazione testa libera
 Coefficiente di efficienza=1.00
 Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>
 Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	-1.2	0
2	1.2	0

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{lim}=252333.00 <daN>
 q_p=28.63 <daN/cm²>
 QP_{lim}=143893.00 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>
 q_p=16.60 <daN/cm²>
 QP_{lim}=83431.40 <daN>
 k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-6835.95	0.09	28.05	4299.39	494.47	0.16	>1
2	1	1	-13954	0.19	13.74	4299.39	494.47	0.16	>1
1	3	2	-7243.99	0.1	--	3801.43	391.53	0.14	--
2	3	2	-13546	0.19	--	3801.43	391.53	0.14	--
1	5	3	-6866.99	0.09	27.93	4262.49	495.24	0.16	>1
2	5	3	-13923	0.19	13.77	4262.49	495.24	0.16	>1
1	7	4	-7270.66	0.1	--	3777.21	459.11	0.14	--
2	7	4	-13519.3	0.19	--	3777.21	459.11	0.14	--
1	9	5	-11903.2	0.16	16.11	1861.54	435.44	0.07	>1
2	9	5	-8886.75	0.12	21.58	1861.54	435.44	0.07	>1
1	11	6	-11599.2	0.16	--	1484.72	340.8	0.06	--
2	11	6	-9190.77	0.13	--	1484.72	340.8	0.06	--
1	13	7	-11934.3	0.16	16.07	1928.51	554.27	0.08	>1
2	13	7	-8855.72	0.12	21.65	1928.51	554.27	0.08	>1
1	15	8	-11625.9	0.16	--	1562.61	509.85	0.06	--
2	15	8	-9164.09	0.13	--	1562.61	509.85	0.06	--
1	17	9	-8573.3	0.12	22.37	2725.93	1628.48	0.12	>1
2	17	9	-12216.7	0.17	15.7	2725.93	1628.48	0.12	>1
1	19	10	-8737.21	0.12	--	2413.3	1366.19	0.1	--
2	19	10	-12052.8	0.17	--	2413.3	1366.19	0.1	--

1	21	11	-10093.5	0.14	19	1650.9	1610.77	0.08	>1
2	21	11	-10696.5	0.15	17.93	1650.9	1610.77	0.08	>1
1	23	12	-10043.8	0.14	--	1415.19	1350.97	0.07	--
2	23	12	-10746.2	0.15	--	1415.19	1350.97	0.07	--
1	25	13	-8676.75	0.12	22.1	2653.73	1670.57	0.11	>1
2	25	13	-12113.3	0.17	15.83	2653.73	1670.57	0.11	>1
1	27	14	-8826.12	0.12	--	2388.14	1469.28	0.1	--
2	27	14	-11963.9	0.16	--	2388.14	1469.28	0.1	--
1	29	15	-10196.9	0.14	18.81	1704.93	1688.28	0.08	>1
2	29	15	-10593.1	0.15	18.1	1704.93	1688.28	0.08	>1
1	31	16	-10132.7	0.14	--	1517.51	1484.5	0.07	--
2	31	16	-10657.3	0.15	--	1517.51	1484.5	0.07	--
1	33	17	-7545.21	0.1	25.42	3420.65	78.09	0.13	>1
2	33	17	-13244.8	0.18	14.48	3420.65	78.09	0.13	>1
1	35	18	-7853.58	0.11	--	3049.89	33.66	0.11	--
2	35	18	-12936.4	0.18	--	3049.89	33.66	0.11	--
1	37	19	-7576.24	0.1	25.31	3503.21	911.62	0.14	>1
2	37	19	-13213.8	0.18	14.51	3503.21	911.62	0.14	>1
1	39	20	-7880.25	0.11	--	3126.33	816.98	0.12	--
2	39	20	-12909.8	0.18	--	3126.33	816.98	0.12	--
1	41	21	-12612.5	0.17	15.2	2661.07	19.06	0.1	>1
2	41	21	-8177.5	0.11	23.45	2661.07	19.06	0.1	>1
1	43	22	-12208.8	0.17	--	2176.66	17.07	0.08	--
2	43	22	-8581.18	0.12	--	2176.66	17.07	0.08	--
1	45	23	-12643.5	0.17	15.17	2867.52	970.65	0.11	>1
2	45	23	-8146.47	0.11	23.54	2867.52	970.65	0.11	>1
1	47	24	-12235.5	0.17	--	2372.94	867.72	0.1	--
2	47	24	-8554.5	0.12	--	2372.94	867.72	0.1	--
1	49	25	-9282.55	0.13	20.66	1803.12	1212.1	0.08	>1
2	49	25	-11507.4	0.16	16.66	1803.12	1212.1	0.08	>1
1	51	26	-9346.8	0.13	--	1612.11	1008.32	0.07	--
2	51	26	-11443.2	0.16	--	1612.11	1008.32	0.07	--
1	53	27	-10802.7	0.15	17.75	1290.73	1194.39	0.06	>1
2	53	27	-9987.26	0.14	19.2	1290.73	1194.39	0.06	>1
1	55	28	-10653.4	0.15	--	1040.37	993.1	0.05	--
2	55	28	-10136.6	0.14	--	1040.37	993.1	0.05	--
1	57	29	-9386	0.13	20.43	2412.76	2086.95	0.11	>1
2	57	29	-11404	0.16	16.82	2412.76	2086.95	0.11	>1
1	59	30	-9435.71	0.13	--	2159.55	1827.15	0.1	--
2	59	30	-11354.3	0.16	--	2159.55	1827.15	0.1	--
1	61	31	-10906.2	0.15	17.58	2192.23	2104.66	0.1	>1
2	61	31	-9883.82	0.14	19.4	2192.23	2104.66	0.1	>1
1	63	32	-10742.3	0.15	--	1888.92	1842.37	0.09	--
2	63	32	-10047.7	0.14	--	1888.92	1842.37	0.09	--
1	65	33	-8083.51	0.11	23.72	1785.76	707.13	0.07	>1
2	65	33	-10816.5	0.15	17.73	1785.76	707.13	0.07	>1
1	67	34	-8459.94	0.12	22.67	1384.84	711.52	0.06	>1
2	67	34	-10440.1	0.14	18.37	1384.84	711.52	0.06	>1
1	69	35	-8267.88	0.11	23.19	1535.11	586.79	0.06	>1
2	69	35	-10632.1	0.15	18.04	1535.11	586.79	0.06	>1
1	71	36	-8275.57	0.11	23.17	1636.51	831.86	0.07	>1
2	71	36	-10624.4	0.15	18.05	1636.51	831.86	0.07	>1
1	73	37	-8419.72	0.12	--	1324.55	475.31	0.05	--
2	73	37	-10480.3	0.14	--	1324.55	475.31	0.05	--
1	75	38	-8796.15	0.12	--	919.64	479.7	0.04	--
2	75	38	-10103.8	0.14	--	919.64	479.7	0.04	--
1	77	39	-8604.1	0.12	--	1075.36	354.97	0.04	--
2	77	39	-10295.9	0.14	--	1075.36	354.97	0.04	--
1	79	40	-8611.78	0.12	--	1171.24	600.04	0.05	--
2	79	40	-10288.2	0.14	--	1171.24	600.04	0.05	--
1	81	41	-8595.71	0.12	--	1065.07	288.84	0.04	--
2	81	41	-10304.3	0.14	--	1065.07	288.84	0.04	--
1	83	42	-8972.13	0.12	--	644.06	293.23	0.03	--
2	83	42	-9927.87	0.14	--	644.06	293.23	0.03	--
1	85	43	-8780.08	0.12	--	821.38	168.5	0.03	--
2	85	43	-10119.9	0.14	--	821.38	168.5	0.03	--
1	87	44	-8787.76	0.12	--	895.86	413.57	0.04	--
2	87	44	-10112.2	0.14	--	895.86	413.57	0.04	--
1	89	45	-8666.1	0.12	--	964.77	214.25	0.04	--
2	89	45	-10233.9	0.14	--	964.77	214.25	0.04	--
1	91	46	-9042.53	0.12	--	535.62	218.64	0.02	--
2	91	46	-9857.47	0.14	--	535.62	218.64	0.02	--
1	93	47	-8850.47	0.12	--	725.54	93.91	0.03	--
2	93	47	-10049.5	0.14	--	725.54	93.91	0.03	--
1	95	48	-8858.16	0.12	--	786.97	338.98	0.03	--
2	95	48	-10041.8	0.14	--	786.97	338.98	0.03	--

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-6835.95	0.09	29.39	4299.39	494.47	0.16	>1
2	2	1	-13954	0.19	14.4	4299.39	494.47	0.16	>1
1	4	2	-7243.99	0.1	--	3801.43	391.53	0.14	--
2	4	2	-13546	0.19	--	3801.43	391.53	0.14	--
1	6	3	-6866.99	0.09	29.26	4262.49	495.24	0.16	>1
2	6	3	-13923	0.19	14.43	4262.49	495.24	0.16	>1
1	8	4	-7270.66	0.1	--	3777.21	459.11	0.14	--
2	8	4	-13519.3	0.19	--	3777.21	459.11	0.14	--
1	10	5	-11903.2	0.16	16.88	1861.54	435.44	0.07	>1
2	10	5	-8886.75	0.12	22.61	1861.54	435.44	0.07	>1
1	12	6	-11599.2	0.16	--	1484.72	340.8	0.06	--
2	12	6	-9190.77	0.13	--	1484.72	340.8	0.06	--
1	14	7	-11934.3	0.16	16.83	1928.51	554.27	0.08	>1
2	14	7	-8855.72	0.12	22.69	1928.51	554.27	0.08	>1
1	16	8	-11625.9	0.16	--	1562.61	509.85	0.06	--
2	16	8	-9164.09	0.13	--	1562.61	509.85	0.06	--
1	18	9	-8573.3	0.12	23.43	2725.93	1628.48	0.12	>1
2	18	9	-12216.7	0.17	16.44	2725.93	1628.48	0.12	>1
1	20	10	-8737.21	0.12	--	2413.3	1366.19	0.1	--
2	20	10	-12052.8	0.17	--	2413.3	1366.19	0.1	--
1	22	11	-10093.5	0.14	19.9	1650.9	1610.77	0.08	>1
2	22	11	-10696.5	0.15	18.78	1650.9	1610.77	0.08	>1
1	24	12	-10043.8	0.14	--	1415.19	1350.97	0.07	--
2	24	12	-10746.2	0.15	--	1415.19	1350.97	0.07	--
1	26	13	-8676.75	0.12	23.15	2653.73	1670.57	0.11	>1
2	26	13	-12113.3	0.17	16.59	2653.73	1670.57	0.11	>1
1	28	14	-8826.12	0.12	--	2388.14	1469.28	0.1	--
2	28	14	-11963.9	0.16	--	2388.14	1469.28	0.1	--
1	30	15	-10196.9	0.14	19.7	1704.93	1688.28	0.08	>1
2	30	15	-10593.1	0.15	18.97	1704.93	1688.28	0.08	>1
1	32	16	-10132.7	0.14	--	1517.51	1484.5	0.07	--
2	32	16	-10657.3	0.15	--	1517.51	1484.5	0.07	--
1	34	17	-7545.21	0.1	26.63	3420.65	78.09	0.13	>1
2	34	17	-13244.8	0.18	15.17	3420.65	78.09	0.13	>1
1	36	18	-7853.58	0.11	--	3049.89	33.66	0.11	--
2	36	18	-12936.4	0.18	--	3049.89	33.66	0.11	--
1	38	19	-7576.24	0.1	26.52	3503.21	911.62	0.14	>1
2	38	19	-13213.8	0.18	15.2	3503.21	911.62	0.14	>1
1	40	20	-7880.25	0.11	--	3126.33	816.98	0.12	--
2	40	20	-12909.8	0.18	--	3126.33	816.98	0.12	--
1	42	21	-12612.5	0.17	15.93	2661.07	19.06	0.1	>1
2	42	21	-8177.5	0.11	24.57	2661.07	19.06	0.1	>1
1	44	22	-12208.8	0.17	--	2176.66	17.07	0.08	--
2	44	22	-8581.18	0.12	--	2176.66	17.07	0.08	--
1	46	23	-12643.5	0.17	15.89	2867.52	970.65	0.11	>1
2	46	23	-8146.47	0.11	24.66	2867.52	970.65	0.11	>1
1	48	24	-12235.5	0.17	--	2372.94	867.72	0.1	--
2	48	24	-8554.5	0.12	--	2372.94	867.72	0.1	--
1	50	25	-9282.55	0.13	21.64	1803.12	1212.1	0.08	>1
2	50	25	-11507.4	0.16	17.46	1803.12	1212.1	0.08	>1
1	52	26	-9346.8	0.13	--	1612.11	1008.32	0.07	--
2	52	26	-11443.2	0.16	--	1612.11	1008.32	0.07	--
1	54	27	-10802.7	0.15	18.6	1290.73	1194.39	0.06	>1
2	54	27	-9987.26	0.14	20.12	1290.73	1194.39	0.06	>1
1	56	28	-10653.4	0.15	--	1040.37	993.1	0.05	--
2	56	28	-10136.6	0.14	--	1040.37	993.1	0.05	--
1	58	29	-9386	0.13	21.4	2412.76	2086.95	0.11	>1
2	58	29	-11404	0.16	17.62	2412.76	2086.95	0.11	>1
1	60	30	-9435.71	0.13	--	2159.55	1827.15	0.1	--
2	60	30	-11354.3	0.16	--	2159.55	1827.15	0.1	--
1	62	31	-10906.2	0.15	18.42	2192.23	2104.66	0.1	>1
2	62	31	-9883.82	0.14	20.33	2192.23	2104.66	0.1	>1
1	64	32	-10742.3	0.15	--	1888.92	1842.37	0.09	--
2	64	32	-10047.7	0.14	--	1888.92	1842.37	0.09	--
1	66	33	-8083.51	0.11	24.85	1785.76	707.13	0.07	>1
2	66	33	-10816.5	0.15	18.57	1785.76	707.13	0.07	>1
1	68	34	-8459.94	0.12	23.75	1384.84	711.52	0.06	>1
2	68	34	-10440.1	0.14	19.24	1384.84	711.52	0.06	>1
1	70	35	-8267.88	0.11	24.3	1535.11	586.79	0.06	>1
2	70	35	-10632.1	0.15	18.9	1535.11	586.79	0.06	>1
1	72	36	-8275.57	0.11	24.28	1636.51	831.86	0.07	>1
2	72	36	-10624.4	0.15	18.91	1636.51	831.86	0.07	>1
1	74	37	-8419.72	0.12	--	1324.55	475.31	0.05	--
2	74	37	-10480.3	0.14	--	1324.55	475.31	0.05	--
1	76	38	-8796.15	0.12	--	919.64	479.7	0.04	--
2	76	38	-10103.8	0.14	--	919.64	479.7	0.04	--

Relazione geotecnica

1	78	39	-8604.1	0.12	--	1075.36	354.97	0.04	--
2	78	39	-10295.9	0.14	--	1075.36	354.97	0.04	--
1	80	40	-8611.78	0.12	--	1171.24	600.04	0.05	--
2	80	40	-10288.2	0.14	--	1171.24	600.04	0.05	--
1	82	41	-8595.71	0.12	--	1065.07	288.84	0.04	--
2	82	41	-10304.3	0.14	--	1065.07	288.84	0.04	--
1	84	42	-8972.13	0.12	--	644.06	293.23	0.03	--
2	84	42	-9927.87	0.14	--	644.06	293.23	0.03	--
1	86	43	-8780.08	0.12	--	821.38	168.5	0.03	--
2	86	43	-10119.9	0.14	--	821.38	168.5	0.03	--
1	88	44	-8787.76	0.12	--	895.86	413.57	0.04	--
2	88	44	-10112.2	0.14	--	895.86	413.57	0.04	--
1	90	45	-8666.1	0.12	--	964.77	214.25	0.04	--
2	90	45	-10233.9	0.14	--	964.77	214.25	0.04	--
1	92	46	-9042.53	0.12	--	535.62	218.64	0.02	--
2	92	46	-9857.47	0.14	--	535.62	218.64	0.02	--
1	94	47	-8850.47	0.12	--	725.54	93.91	0.03	--
2	94	47	-10049.5	0.14	--	725.54	93.91	0.03	--
1	96	48	-8858.16	0.12	--	786.97	338.98	0.03	--
2	96	48	-10041.8	0.14	--	786.97	338.98	0.03	--

Plinto n. 7

Tipo palo=Trivellato

Rotazione testa libera

Coefficiente di efficienza=1.00

Dp=0.800000 <m> Lp=16.000000 <m> Wp=20106.20 <daN> D=1.00 <m>

Colonna stratigrafica numero 1

Numerazione e posizione pali

Palo	Xp <m>	Yp <m>
1	-1.2	0
2	1.2	0

Verifiche in condizioni drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.25	0.17	3.45	1.88
17	1.01	0.17	22.05	1.88

QS_{lim}=252333.00 <daN>

q_p=28.63 <daN/cm²>

QP_{lim}=143893.00 <daN>

k_p=1.42 <daN/cm²>

Verifiche in condizioni non drenate

Zp <m>	τ_s <daN/cm ² >	k_s <daN/cm ² >	σ_h <daN/cm ² >	k_h <daN/cm ² >
1	0.8	0.17	16	1.88
17	0.8	0.17	16	1.88

QS_{lim}=321694.00 <daN>

q_p=16.60 <daN/cm²>

QP_{lim}=83431.40 <daN>

k_p=1.42 <daN/cm²>

Verifiche in condizioni drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	1	1	-7017.91	0.1	27.33	4186.03	1048.84	0.16	>1
2	1	1	-13772.1	0.19	13.92	4186.03	1048.84	0.16	>1
1	3	2	-7306.17	0.1	--	3817.33	912.77	0.15	--
2	3	2	-13483.8	0.19	--	3817.33	912.77	0.15	--
1	5	3	-7086.04	0.1	27.06	3974.74	178.11	0.15	>1
2	5	3	-13704	0.19	13.99	3974.74	178.11	0.15	>1
1	7	4	-7364.72	0.1	--	3640.05	164.39	0.13	--
2	7	4	-13425.3	0.19	--	3640.05	164.39	0.13	--
1	9	5	-10545.7	0.15	18.18	623.97	597.19	0.03	>1
2	9	5	-10244.3	0.14	18.72	623.97	597.19	0.03	>1
1	11	6	-10338.2	0.14	--	528.99	524.58	0.02	--
2	11	6	-10451.8	0.14	--	528.99	524.58	0.02	--
1	13	7	-10613.8	0.15	18.07	379.18	273.54	0.02	>1
2	13	7	-10176.2	0.14	18.84	379.18	273.54	0.02	>1
1	15	8	-10396.8	0.14	--	223.81	223.8	0.01	--

Relazione geotecnica

2	15	8	-10393.2	0.14	--	223.81	223.8	0.01	--
1	17	9	-8173.16	0.11	23.46	3277.79	1906.62	0.14	>1
2	17	9	-12616.8	0.17	15.2	3277.79	1906.62	0.14	>1
1	19	10	-8299.08	0.11	--	3008.04	1650.01	0.13	--
2	19	10	-12490.9	0.17	--	3008.04	1650.01	0.13	--
1	21	11	-9231.49	0.13	20.77	2255.28	1771.12	0.1	>1
2	21	11	-11558.5	0.16	16.59	2255.28	1771.12	0.1	>1
1	23	12	-9208.7	0.13	--	2092.44	1533.55	0.09	--
2	23	12	-11581.3	0.16	--	2092.44	1533.55	0.09	--
1	25	13	-8400.25	0.12	22.83	2592.58	995.82	0.1	>1
2	25	13	-12389.8	0.17	15.48	2592.58	995.82	0.1	>1
1	27	14	-8494.26	0.12	--	2432.24	844.58	0.1	--
2	27	14	-12295.7	0.17	--	2432.24	844.58	0.1	--
1	29	15	-9458.58	0.13	20.27	1594.55	1131.32	0.07	>1
2	29	15	-11331.4	0.16	16.92	1594.55	1131.32	0.07	>1
1	31	16	-9403.88	0.13	--	1529.1	961.04	0.07	--
2	31	16	-11386.1	0.16	--	1529.1	961.04	0.07	--
1	33	17	-7524.75	0.1	25.49	3471.6	434.48	0.13	>1
2	33	17	-13265.3	0.18	14.46	3471.6	434.48	0.13	>1
1	35	18	-7741.78	0.11	--	3207.02	384.73	0.12	--
2	35	18	-13048.2	0.18	--	3207.02	384.73	0.12	--
1	37	19	-7592.87	0.1	25.26	3390.74	436.26	0.13	>1
2	37	19	-13197.1	0.18	14.53	3390.74	436.26	0.13	>1
1	39	20	-7800.34	0.11	--	3134.76	363.65	0.12	--
2	39	20	-12989.7	0.18	--	3134.76	363.65	0.12	--
1	41	21	-11052.5	0.15	17.35	789.22	17.18	0.03	>1
2	41	21	-9737.47	0.13	19.69	789.22	17.18	0.03	>1
1	43	22	-10773.8	0.15	--	454.63	3.46	0.02	--
2	43	22	-10016.2	0.14	--	454.63	3.46	0.02	--
1	45	23	-11120.7	0.15	17.24	1243.65	887.91	0.05	>1
2	45	23	-9669.34	0.13	19.83	1243.65	887.91	0.05	>1
1	47	24	-10832.4	0.15	--	916.93	751.83	0.04	--
2	47	24	-9957.6	0.14	--	916.93	751.83	0.04	--
1	49	25	-8679.99	0.12	22.09	2430.09	1292.25	0.1	>1
2	49	25	-12110	0.17	15.84	2430.09	1292.25	0.1	>1
1	51	26	-8734.69	0.12	--	2286.56	1121.97	0.09	--
2	51	26	-12055.3	0.17	--	2286.56	1121.97	0.09	--
1	53	27	-9738.33	0.13	19.69	1399.66	1156.76	0.06	>1
2	53	27	-11051.7	0.15	17.35	1399.66	1156.76	0.06	>1
1	55	28	-9644.31	0.13	--	1350.02	1005.52	0.06	--
2	55	28	-11145.7	0.15	--	1350.02	1005.52	0.06	--
1	57	29	-8907.08	0.12	21.53	2404.32	1610.19	0.1	>1
2	57	29	-11882.9	0.16	16.14	2404.32	1610.19	0.1	>1
1	59	30	-8929.87	0.12	--	2230.51	1372.62	0.1	--
2	59	30	-11860.1	0.16	--	2230.51	1372.62	0.1	--
1	61	31	-9965.42	0.14	19.24	1820.21	1745.68	0.08	>1
2	61	31	-10824.6	0.15	17.72	1820.21	1745.68	0.08	>1
1	63	32	-9839.49	0.14	--	1631.48	1489.08	0.07	--
2	63	32	-10950.5	0.15	--	1631.48	1489.08	0.07	--
1	65	33	-7088.17	0.1	27.05	2835.34	80.36	0.1	>1
2	65	33	-11811.8	0.16	16.24	2835.34	80.36	0.1	>1
1	67	34	-7350.23	0.1	26.09	2522.3	113.92	0.09	>1
2	67	34	-11549.8	0.16	16.6	2522.3	113.92	0.09	>1
1	69	35	-7210.76	0.1	26.59	2687.11	10.67	0.1	>1
2	69	35	-11689.2	0.16	16.41	2687.11	10.67	0.1	>1
1	71	36	-7227.63	0.1	26.53	2674.7	204.94	0.1	>1
2	71	36	-11672.4	0.16	16.43	2674.7	204.94	0.1	>1
1	73	37	-7708.69	0.11	--	2089.75	27.34	0.08	--
2	73	37	-11191.3	0.15	--	2089.75	27.34	0.08	--
1	75	38	-7970.75	0.11	--	1776.14	60.89	0.07	--
2	75	38	-10929.2	0.15	--	1776.14	60.89	0.07	--
1	77	39	-7831.29	0.11	--	1943.5	63.69	0.07	--
2	77	39	-11068.7	0.15	--	1943.5	63.69	0.07	--
1	79	40	-7848.16	0.11	--	1928.21	151.92	0.07	--
2	79	40	-11051.8	0.15	--	1928.21	151.92	0.07	--
1	81	41	-7998.04	0.11	--	1743.27	56.42	0.06	--
2	81	41	-10902	0.15	--	1743.27	56.42	0.06	--
1	83	42	-8260.1	0.11	--	1428.06	22.87	0.05	--
2	83	42	-10639.9	0.15	--	1428.06	22.87	0.05	--
1	85	43	-8120.63	0.11	--	1602.04	147.45	0.06	--
2	85	43	-10779.4	0.15	--	1602.04	147.45	0.06	--
1	87	44	-8137.5	0.11	--	1576.47	68.16	0.06	--
2	87	44	-10762.5	0.15	--	1576.47	68.16	0.06	--
1	89	45	-8113.77	0.11	--	1605.99	89.93	0.06	--
2	89	45	-10786.2	0.15	--	1605.99	89.93	0.06	--
1	91	46	-8375.84	0.12	--	1290.23	56.38	0.05	--
2	91	46	-10524.2	0.15	--	1290.23	56.38	0.05	--
1	93	47	-8236.37	0.11	--	1467.55	180.96	0.06	--
2	93	47	-10663.6	0.15	--	1467.55	180.96	0.06	--

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1	95	48	-8253.24	0.11	--	1436.53	34.65	0.05	--
2	95	48	-10646.8	0.15	--	1436.53	34.65	0.05	--

Verifiche in condizioni non drenate

Palo	Caso	CC	N <daN>	Ced <cm>	Sic.V	T <daN>	M <daNm>	Sps <cm>	Sic.O
1	2	1	-7017.91	0.1	28.63	4186.03	1048.84	0.16	>1
2	2	1	-13772.1	0.19	14.59	4186.03	1048.84	0.16	>1
1	4	2	-7306.17	0.1	--	3817.33	912.77	0.15	--
2	4	2	-13483.8	0.19	--	3817.33	912.77	0.15	--
1	6	3	-7086.04	0.1	28.35	3974.74	178.11	0.15	>1
2	6	3	-13704	0.19	14.66	3974.74	178.11	0.15	>1
1	8	4	-7364.72	0.1	--	3640.05	164.39	0.13	--
2	8	4	-13425.3	0.19	--	3640.05	164.39	0.13	--
1	10	5	-10545.7	0.15	19.05	623.97	597.19	0.03	>1
2	10	5	-10244.3	0.14	19.61	623.97	597.19	0.03	>1
1	12	6	-10338.2	0.14	--	528.99	524.58	0.02	--
2	12	6	-10451.8	0.14	--	528.99	524.58	0.02	--
1	14	7	-10613.8	0.15	18.93	379.18	273.54	0.02	>1
2	14	7	-10176.2	0.14	19.74	379.18	273.54	0.02	>1
1	16	8	-10396.8	0.14	--	223.81	223.8	0.01	--
2	16	8	-10393.2	0.14	--	223.81	223.8	0.01	--
1	18	9	-8173.16	0.11	24.58	3277.79	1906.62	0.14	>1
2	18	9	-12616.8	0.17	15.92	3277.79	1906.62	0.14	>1
1	20	10	-8299.08	0.11	--	3008.04	1650.01	0.13	--
2	20	10	-12490.9	0.17	--	3008.04	1650.01	0.13	--
1	22	11	-9231.49	0.13	21.76	2255.28	1771.12	0.1	>1
2	22	11	-11558.5	0.16	17.38	2255.28	1771.12	0.1	>1
1	24	12	-9208.7	0.13	--	2092.44	1533.55	0.09	--
2	24	12	-11581.3	0.16	--	2092.44	1533.55	0.09	--
1	26	13	-8400.25	0.12	23.92	2592.58	995.82	0.1	>1
2	26	13	-12389.8	0.17	16.22	2592.58	995.82	0.1	>1
1	28	14	-8494.26	0.12	--	2432.24	844.58	0.1	--
2	28	14	-12295.7	0.17	--	2432.24	844.58	0.1	--
1	30	15	-9458.58	0.13	21.24	1594.55	1131.32	0.07	>1
2	30	15	-11331.4	0.16	17.73	1594.55	1131.32	0.07	>1
1	32	16	-9403.88	0.13	--	1529.1	961.04	0.07	--
2	32	16	-11386.1	0.16	--	1529.1	961.04	0.07	--
1	34	17	-7524.75	0.1	26.7	3471.6	434.48	0.13	>1
2	34	17	-13265.3	0.18	15.14	3471.6	434.48	0.13	>1
1	36	18	-7741.78	0.11	--	3207.02	384.73	0.12	--
2	36	18	-13048.2	0.18	--	3207.02	384.73	0.12	--
1	38	19	-7592.87	0.1	26.46	3390.74	436.26	0.13	>1
2	38	19	-13197.1	0.18	15.22	3390.74	436.26	0.13	>1
1	40	20	-7800.34	0.11	--	3134.76	363.65	0.12	--
2	40	20	-12989.7	0.18	--	3134.76	363.65	0.12	--
1	42	21	-11052.5	0.15	18.18	789.22	17.18	0.03	>1
2	42	21	-9737.47	0.13	20.63	789.22	17.18	0.03	>1
1	44	22	-10773.8	0.15	--	454.63	3.46	0.02	--
2	44	22	-10016.2	0.14	--	454.63	3.46	0.02	--
1	46	23	-11120.7	0.15	18.07	1243.65	887.91	0.05	>1
2	46	23	-9669.34	0.13	20.78	1243.65	887.91	0.05	>1
1	48	24	-10832.4	0.15	--	916.93	751.83	0.04	--
2	48	24	-9957.6	0.14	--	916.93	751.83	0.04	--
1	50	25	-8679.99	0.12	23.15	2430.09	1292.25	0.1	>1
2	50	25	-12110	0.17	16.59	2430.09	1292.25	0.1	>1
1	52	26	-8734.69	0.12	--	2286.56	1121.97	0.09	--
2	52	26	-12055.3	0.17	--	2286.56	1121.97	0.09	--
1	54	27	-9738.33	0.13	20.63	1399.66	1156.76	0.06	>1
2	54	27	-11051.7	0.15	18.18	1399.66	1156.76	0.06	>1
1	56	28	-9644.31	0.13	--	1350.02	1005.52	0.06	--
2	56	28	-11145.7	0.15	--	1350.02	1005.52	0.06	--
1	58	29	-8907.08	0.12	22.56	2404.32	1610.19	0.1	>1
2	58	29	-11882.9	0.16	16.91	2404.32	1610.19	0.1	>1
1	60	30	-8929.87	0.12	--	2230.51	1372.62	0.1	--
2	60	30	-11860.1	0.16	--	2230.51	1372.62	0.1	--
1	62	31	-9965.42	0.14	20.16	1820.21	1745.68	0.08	>1
2	62	31	-10824.6	0.15	18.56	1820.21	1745.68	0.08	>1
1	64	32	-9839.49	0.14	--	1631.48	1489.08	0.07	--
2	64	32	-10950.5	0.15	--	1631.48	1489.08	0.07	--
1	66	33	-7088.17	0.1	28.34	2835.34	80.36	0.1	>1
2	66	33	-11811.8	0.16	17.01	2835.34	80.36	0.1	>1
1	68	34	-7350.23	0.1	27.33	2522.3	113.92	0.09	>1
2	68	34	-11549.8	0.16	17.39	2522.3	113.92	0.09	>1
1	70	35	-7210.76	0.1	27.86	2687.11	10.67	0.1	>1
2	70	35	-11689.2	0.16	17.19	2687.11	10.67	0.1	>1
1	72	36	-7227.63	0.1	27.8	2674.7	204.94	0.1	>1

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2	72	36	-11672.4	0.16	17.21	2674.7	204.94	0.1	>1
1	74	37	-7708.69	0.11	--	2089.75	27.34	0.08	--
2	74	37	-11191.3	0.15	--	2089.75	27.34	0.08	--
1	76	38	-7970.75	0.11	--	1776.14	60.89	0.07	--
2	76	38	-10929.2	0.15	--	1776.14	60.89	0.07	--
1	78	39	-7831.29	0.11	--	1943.5	63.69	0.07	--
2	78	39	-11068.7	0.15	--	1943.5	63.69	0.07	--
1	80	40	-7848.16	0.11	--	1928.21	151.92	0.07	--
2	80	40	-11051.8	0.15	--	1928.21	151.92	0.07	--
1	82	41	-7998.04	0.11	--	1743.27	56.42	0.06	--
2	82	41	-10902	0.15	--	1743.27	56.42	0.06	--
1	84	42	-8260.1	0.11	--	1428.06	22.87	0.05	--
2	84	42	-10639.9	0.15	--	1428.06	22.87	0.05	--
1	86	43	-8120.63	0.11	--	1602.04	147.45	0.06	--
2	86	43	-10779.4	0.15	--	1602.04	147.45	0.06	--
1	88	44	-8137.5	0.11	--	1576.47	68.16	0.06	--
2	88	44	-10762.5	0.15	--	1576.47	68.16	0.06	--
1	90	45	-8113.77	0.11	--	1605.99	89.93	0.06	--
2	90	45	-10786.2	0.15	--	1605.99	89.93	0.06	--
1	92	46	-8375.84	0.12	--	1290.23	56.38	0.05	--
2	92	46	-10524.2	0.15	--	1290.23	56.38	0.05	--
1	94	47	-8236.37	0.11	--	1467.55	180.96	0.06	--
2	94	47	-10663.6	0.15	--	1467.55	180.96	0.06	--
1	96	48	-8253.24	0.11	--	1436.53	34.65	0.05	--
2	96	48	-10646.8	0.15	--	1436.53	34.65	0.05	--

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Introduzione

Sistemi di riferimento

Le coordinate, i carichi concentrati, i cedimenti, le reazioni vincolari e gli spostamenti dei NODI sono riferiti ad una terna destra cartesiana globale con l'asse Z verticale rivolto verso l'alto.

I carichi in coordinate locali e le sollecitazioni delle ASTE sono riferite ad una terna destra cartesiana locale così definita:

- origine nel nodo iniziale dell'asta;
- asse X coincidente con l'asse dell'asta e con verso dal nodo iniziale al nodo finale;
- immaginando la trave a sezione rettangolare l'asse Y è parallelo alla base e l'asse Z è parallelo all'altezza. La rotazione dell'asta comporta quindi una rotazione di tutta la terna locale.

Si può immaginare la terna locale di un'asta comunque disposta nello spazio come derivante da quella globale dopo una serie di trasformazioni:

- una rotazione intorno all'asse Z che porti l'asse X a coincidere con la proiezione dell'asse dell'asta sul piano orizzontale;
- una traslazione lungo il nuovo asse X così definito in modo da portare l'origine a coincidere con la proiezione del nodo iniziale dell'asta sul piano orizzontale;
- una traslazione lungo l'asse Z che porti l'origine a coincidere con il nodo iniziale dell'asta;
- una rotazione intorno all'asse Y così definito che porti l'asse X a coincidere con l'asse dell'asta;
- una rotazione intorno all'asse X così definito pari alla rotazione dell'asta.

In pratica le travi prive di rotazione avranno sempre l'asse Z rivolto verso l'alto e l'asse Y nel piano del solaio, mentre i pilastri privi di rotazione avranno l'asse Y parallelo all'asse Y globale e l'asse Z parallelo ma controverso all'asse X globale. Da notare quindi che per i pilastri la "base" è il lato parallelo a Y.

Le sollecitazioni ed i carichi in coordinate locali negli ELEMENTI BIDIMENSIONALI e nei MURI sono riferiti ad una terna destra cartesiana locale così definita:

- origine nel primo nodo dell'elemento;
- asse X coincidente con la congiungente il primo ed il secondo nodo dell'elemento;
- asse Y definito come prodotto vettoriale fra il versore dell'asse X e il versore della congiungente il primo e il quarto nodo. Asse Z a formare con gli altri due una terna destrorsa.

Praticamente un elemento verticale con l'asse X locale coincidente con l'asse X globale ha anche gli altri assi locali coincidenti con quelli globali.

Rotazioni e momenti

Seguendo il principio adottato per tutti i carichi che sono positivi se CONTROVERSI agli assi, anche i momenti concentrati e le rotazioni impresse in coordinate globali risultano positivi se CONTROVERSI al segno positivo delle rotazioni. Il segno positivo dei momenti e delle rotazioni è quello orario per l'osservatore posto nell'origine: X ruota su Y, Y ruota su Z, Z ruota su X. In pratica è sufficiente adottare la regola della mano destra: col pollice rivolto nella direzione dell'asse, la rotazione che porta a chiudere il palmo della mano corrisponde al segno positivo.

Normativa di riferimento

La normativa di riferimento è la seguente:

- Legge n. 64 del 2/2/1974 - Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche.
- D.M. del 24/1/1986 - Norme tecniche relative alle costruzioni sismiche.
- Legge n. 1086 del 5/11/1971 - Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso ed a struttura metallica.
- D.M. del 14/2/1992 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.
- D.M. del 9/1/1996 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.
- D.M. del 16/1/1996 - Norme tecniche per le costruzioni in zone sismiche.
- Circolare n. 21745 del 30/7/1981 - Legge n. 219 del 14/5/1981 - Art. 10 - Istruzioni relative al rafforzamento degli edifici in muratura danneggiati dal sisma.
- Regione Autonoma Friuli Venezia Giulia - Legge Regionale n. 30 del 20/6/1977 - Documentazione tecnica per la progettazione e direzione delle opere di riparazione degli edifici - Documento Tecnico n. 2 - Raccomandazioni per la riparazione strutturale degli edifici in muratura.
- D.M. del 20/11/1987 - Norme Tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento.
- Norme Tecniche C.N.R. n. 10011-85 del 18/4/1985 - Costruzioni di acciaio - Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.
- Norme Tecniche C.N.R. n. 10025-84 del 14/12/1984 - Istruzioni per il progetto, l'esecuzione ed il controllo delle strutture prefabbricate in conglomerato cementizio e per le strutture costruite con sistemi industrializzati di acciaio
- Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.

Relazione geotecnica tombino

- Circolare n. 65 del 10/4/1997 - Istruzioni per l'applicazione delle "Norme tecniche per le costruzioni in zone sismiche" di cui al D.M. del 16/1/1996.

- Eurocodice 5 - Progettazione delle strutture di legno.

- DIN 1052 - Metodi di verifica per il legno.

- D.M. del 14/1/2008 - Norme tecniche per le costruzioni. Le verifiche degli elementi di fondazione sono eseguite utilizzando l'Approccio 2.

- Circolare n. 617 del 2/2/2009 - Istruzioni per l'applicazione delle "Nuove norme tecniche per le costruzioni" di cui al D.M. del 14/1/2008.

- Documento Tecnico CNR-DT 200 R1/2012 - Istruzioni per la Progettazione, l'Esecuzione ed il Controllo di Interventi di Consolidamento Statico mediante l'utilizzo di Compositi Fibrorinforzati.

- Eurocodice 3 - Progettazione delle strutture in acciaio.

Unità di misura

Le unità di misura adottate sono le seguenti:

- lunghezze : m
- forze : daN
- masse : kg
- temperature : gradi centigradi
- angoli : gradi sessadecimali o radianti

Geometria

Elenco vincoli nodi

Simbologia

Vn = Numero del vincolo nodo
Comm. = Commento
Sx = Spostamento in dir. X (L=libero, B=bloccato, E=elastico)
Sy = Spostamento in dir. Y (L=libero, B=bloccato, E=elastico)
Sz = Spostamento in dir. Z (L=libero, B=bloccato, E=elastico)
Rx = Rotazione intorno all'asse X (L=libera, B=bloccata, E=elastica)
Ry = Rotazione intorno all'asse Y (L=libera, B=bloccata, E=elastica)
Rz = Rotazione intorno all'asse Z (L=libera, B=bloccata, E=elastica)
RL = Rotazione libera
Ly = Lunghezza (dir. Y locale)
Lz = Larghezza (dir. Z locale)
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Vn	Comm.	Sx	Sy	Sz	Rx	Ry	Rz	RL	Ly	Lz	Kt
									<m>	<m>	<daN/cmc>
1	Libero	L	L	L	L	L	L				

Vn	Comm.	Sx	Sy	Sz	Rx	Ry	Rz	RL	Ly	Lz	Kt
									<m>	<m>	<daN/cmc>
3	El. sew 110001	B	B	L	L	L	B				

Elenco nodi

Simbologia

Nodo = Numero del nodo
X = Coordinata X del nodo
Y = Coordinata Y del nodo
Z = Coordinata Z del nodo
Imp. = Numero dell'impalcato
Vn = Numero del vincolo nodo

Nodo	X	Y	Z	Imp.	Vn
	<m>	<m>	<m>		
-182	12	3.2	2.5	1	1
-178	8	3.2	2.5	1	1
-174	4	3.2	2.5	1	1
-170	0	3.2	2.5	1	1
-166	9	2.4	2.5	1	1
-162	5	2.4	2.5	1	1
-158	1	2.4	2.5	1	1
-154	10	1.6	2.5	1	1
-150	6	1.6	2.5	1	1
-146	2	1.6	2.5	1	1
-142	11	0.8	2.5	1	1
-138	7	0.8	2.5	1	1
-134	3	0.8	2.5	1	1
-130	12	0	2.5	1	1
-126	8	0	2.5	1	1
-122	4	0	2.5	1	1
-118	0	0	2.5	1	1
-114	9	3.2	1.67	0	1
-110	5	3.2	1.67	0	1
-106	1	3.2	1.67	0	1

Nodo	X	Y	Z	Imp.	Vn
	<m>	<m>	<m>		
-181	11	3.2	2.5	1	1
-177	7	3.2	2.5	1	1
-173	3	3.2	2.5	1	1
-169	12	2.4	2.5	1	1
-165	8	2.4	2.5	1	1
-161	4	2.4	2.5	1	1
-157	0	2.4	2.5	1	1
-153	9	1.6	2.5	1	1
-149	5	1.6	2.5	1	1
-145	1	1.6	2.5	1	1
-141	10	0.8	2.5	1	1
-137	6	0.8	2.5	1	1
-133	2	0.8	2.5	1	1
-129	11	0	2.5	1	1
-125	7	0	2.5	1	1
-121	3	0	2.5	1	1
-117	12	3.2	1.67	0	1
-113	8	3.2	1.67	0	1
-109	4	3.2	1.67	0	1
-105	0	3.2	1.67	0	1

Nodo	X	Y	Z	Imp.	Vn
	<m>	<m>	<m>		
-180	10	3.2	2.5	1	1
-176	6	3.2	2.5	1	1
-172	2	3.2	2.5	1	1
-168	11	2.4	2.5	1	1
-164	7	2.4	2.5	1	1
-160	3	2.4	2.5	1	1
-156	12	1.6	2.5	1	1
-152	8	1.6	2.5	1	1
-148	4	1.6	2.5	1	1
-144	0	1.6	2.5	1	1
-140	9	0.8	2.5	1	1
-136	5	0.8	2.5	1	1
-132	1	0.8	2.5	1	1
-128	10	0	2.5	1	1
-124	6	0	2.5	1	1
-120	2	0	2.5	1	1
-116	11	3.2	1.67	0	1
-112	7	3.2	1.67	0	1
-108	3	3.2	1.67	0	1
-104	12	0	1.67	0	1

Nodo	X	Y	Z	Imp.	Vn
	<m>	<m>	<m>		
-179	9	3.2	2.5	1	1
-175	5	3.2	2.5	1	1
-171	1	3.2	2.5	1	1
-167	10	2.4	2.5	1	1
-163	6	2.4	2.5	1	1
-159	2	2.4	2.5	1	1
-155	11	1.6	2.5	1	1
-151	7	1.6	2.5	1	1
-147	3	1.6	2.5	1	1
-143	12	0.8	2.5	1	1
-139	8	0.8	2.5	1	1
-135	4	0.8	2.5	1	1
-131	0	0.8	2.5	1	1
-127	9	0	2.5	1	1
-123	5	0	2.5	1	1
-119	1	0	2.5	1	1
-115	10	3.2	1.67	0	1
-111	6	3.2	1.67	0	1
-107	2	3.2	1.67	0	1
-103	11	0	1.67	0	1

Relazione geotecnica tombino

-102	10	0	1.67	0	1	-101	9	0	1.67	0	1	-100	8	0	1.67	0	1	-99	7	0	1.67	0	1
-98	6	0	1.67	0	1	-97	5	0	1.67	0	1	-96	4	0	1.67	0	1	-95	3	0	1.67	0	1
-94	2	0	1.67	0	1	-93	1	0	1.67	0	1	-92	0	0	1.67	0	1	-91	12	3.2	0.83	0	1
-90	11	3.2	0.83	0	1	-89	10	3.2	0.83	0	1	-88	9	3.2	0.83	0	1	-87	8	3.2	0.83	0	1
-86	7	3.2	0.83	0	1	-85	6	3.2	0.83	0	1	-84	5	3.2	0.83	0	1	-83	4	3.2	0.83	0	1
-82	3	3.2	0.83	0	1	-81	2	3.2	0.83	0	1	-80	1	3.2	0.83	0	1	-79	0	3.2	0.83	0	1
-78	12	0	0.83	0	1	-77	11	0	0.83	0	1	-76	10	0	0.83	0	1	-75	9	0	0.83	0	1
-74	8	0	0.83	0	1	-73	7	0	0.83	0	1	-72	6	0	0.83	0	1	-71	5	0	0.83	0	1
-70	4	0	0.83	0	1	-69	3	0	0.83	0	1	-68	2	0	0.83	0	1	-67	1	0	0.83	0	1
-66	0	0	0.83	0	1	-65	12	3.2	0	0	3	-64	11	3.2	0	0	3	-63	10	3.2	0	0	3
-62	9	3.2	0	0	3	-61	8	3.2	0	0	3	-60	7	3.2	0	0	3	-59	6	3.2	0	0	3
-58	5	3.2	0	0	3	-57	4	3.2	0	0	3	-56	3	3.2	0	0	3	-55	2	3.2	0	0	3
-54	1	3.2	0	0	3	-53	0	3.2	0	0	3	-52	12	2.4	0	0	3	-51	11	2.4	0	0	3
-50	10	2.4	0	0	3	-49	9	2.4	0	0	3	-48	8	2.4	0	0	3	-47	7	2.4	0	0	3
-46	6	2.4	0	0	3	-45	5	2.4	0	0	3	-44	4	2.4	0	0	3	-43	3	2.4	0	0	3
-42	2	2.4	0	0	3	-41	1	2.4	0	0	3	-40	0	2.4	0	0	3	-39	12	1.6	0	0	3
-38	11	1.6	0	0	3	-37	10	1.6	0	0	3	-36	9	1.6	0	0	3	-35	8	1.6	0	0	3
-34	7	1.6	0	0	3	-33	6	1.6	0	0	3	-32	5	1.6	0	0	3	-31	4	1.6	0	0	3
-30	3	1.6	0	0	3	-29	2	1.6	0	0	3	-28	1	1.6	0	0	3	-27	0	1.6	0	0	3
-26	12	0.8	0	0	3	-25	11	0.8	0	0	3	-24	10	0.8	0	0	3	-23	9	0.8	0	0	3
-22	8	0.8	0	0	3	-21	7	0.8	0	0	3	-20	6	0.8	0	0	3	-19	5	0.8	0	0	3
-18	4	0.8	0	0	3	-17	3	0.8	0	0	3	-16	2	0.8	0	0	3	-15	1	0.8	0	0	3
-14	0	0.8	0	0	3	-13	12	0	0	0	3	-12	11	0	0	0	3	-11	10	0	0	0	3
-10	9	0	0	0	3	-9	8	0	0	0	3	-8	7	0	0	0	3	-7	6	0	0	0	3
-6	5	0	0	0	3	-5	4	0	0	0	3	-4	3	0	0	0	3	-3	2	0	0	0	3
-2	1	0	0	0	3	-1	0	0	0	0	3												

Elenco materiali

Simbologia

Mat. =Numero del materiale
Comm. =Commento
P =Peso specifico
E =Modulo elastico
G =Modulo elastico tangenziale
v =Coeff. di Poisson
α =Coeff. di dilatazione termica

Mat.	Comm.	P <daN/mc>	E <daN/cm<	G <daN/cm<	v	α
1	Calcestruzzo	2500	300000	130000	0.1	1.000000E-05

Elenco vincoli aste

Simbologia

Va =Numero del vincolo asta
Comm. =Commento
Tipo =Tipologia
SVI = Definizione di vincolamenti interni
ELA = Vincolo su suolo elastico alla Winkler
BIE-RTC = Biella resistente a trazione e a compressione
BIE-RC = Biella resistente solo a compressione
BIE-RT = Biella resistente solo a trazione
Ni =Sforzo normale nodo iniziale (0=sbloccato, 1=bloccato)
Tyi =Taglio in dir. Y locale nodo iniziale (0=sbloccato, 1=bloccato)
Tzi =Taglio in dir. Z locale nodo iniziale (0=sbloccato, 1=bloccato)
Mxi =Momento intorno all'asse X locale nodo iniziale (0=sbloccato, 1=bloccato)
Myi =Momento intorno all'asse Y locale nodo iniziale (0=sbloccato, 1=bloccato)
Mzi =Momento intorno all'asse Z locale nodo iniziale (0=sbloccato, 1=bloccato)
Nf =Sforzo normale nodo finale (0=sbloccato, 1=bloccato)
Tyf =Taglio in dir. Y locale nodo finale (0=sbloccato, 1=bloccato)
Tzf =Taglio in dir. Z locale nodo finale (0=sbloccato, 1=bloccato)
Mxf =Momento intorno all'asse X locale nodo finale (0=sbloccato, 1=bloccato)
Myf =Momento intorno all'asse Y locale nodo finale (0=sbloccato, 1=bloccato)
Mzf =Momento intorno all'asse Z locale nodo finale (0=sbloccato, 1=bloccato)
Kt =Coeff. di sottofondo su suolo elastico alla Winkler

Va	Comm.	Tipo	Ni	Tyi	Tzi	Mxi	Myi	Mzi	Nf	Tyf	Tzf	Mxf	Myf	Mzf	Kt <daN/cmc>
1	Inc+Inc	SVI	1	1	1	1	1	1	1	1	1	1	1	1	

Elenco aste

Simbologia

Asta=Numero dell'asta
N1 =Nodo iniziale
N2 =Nodo finale
Sez.=Numero della sezione
Va =Numero del vincolo asta
Par.=Numero dei parametri aggiuntivi
Rot.=Rotazione

Relazione geotecnica tombino

FF =Filo fisso
Dy1 =Scost. filo fisso Y1
Dy2 =Scost. filo fisso Y2
Dz1 =Scost. filo fisso Z1
Dz2 =Scost. filo fisso Z2
Kt =Coeff. di sottofondo su suolo elastico alla Winkler

Asta	N1	N2	Sez.	Va	Par.	Rot. <grad>	FF <cm>	Dy1 <cm>	Dy2 <cm>	Dz1 <cm>	Dz2 <cm>	Kt <daN/cmc>
0	-2	-1		1			0 33	0	0	0	0	
0	-3	-2		1			0 33	0	0	0	0	
0	-4	-3		1			0 33	0	0	0	0	
0	-119	-118		1			0 33	0	0	0	0	
0	-5	-4		1			0 33	0	0	0	0	
0	-120	-119		1			0 33	0	0	0	0	
0	-53	-54		1			0 33	0	0	0	0	
0	-6	-5		1			0 33	0	0	0	0	
0	-121	-120		1			0 33	0	0	0	0	
0	-7	-6		1			0 33	0	0	0	0	
0	-122	-121		1			0 33	0	0	0	0	
0	-123	-122		1			0 33	0	0	0	0	
0	-54	-55		1			0 33	0	0	0	0	
0	-55	-56		1			0 33	0	0	0	0	
0	-170	-171		1			0 33	0	0	0	0	
0	-8	-7		1			0 33	0	0	0	0	
0	-124	-123		1			0 33	0	0	0	0	
0	-56	-57		1			0 33	0	0	0	0	
0	-171	-172		1			0 33	0	0	0	0	
0	-57	-58		1			0 33	0	0	0	0	
0	-172	-173		1			0 33	0	0	0	0	
0	-173	-174		1			0 33	0	0	0	0	
0	-9	-8		1			0 33	0	0	0	0	
0	-10	-9		1			0 33	0	0	0	0	
0	-125	-124		1			0 33	0	0	0	0	
0	-11	-10		1			0 33	0	0	0	0	
0	-126	-125		1			0 33	0	0	0	0	
0	-58	-59		1			0 33	0	0	0	0	
0	-174	-175		1			0 33	0	0	0	0	
0	-127	-126		1			0 33	0	0	0	0	
0	-176	-177		1			0 33	0	0	0	0	
0	-12	-11		1			0 33	0	0	0	0	
0	-128	-127		1			0 33	0	0	0	0	
0	-59	-60		1			0 33	0	0	0	0	
0	-129	-128		1			0 33	0	0	0	0	
0	-60	-61		1			0 33	0	0	0	0	
0	-175	-176		1			0 33	0	0	0	0	
0	-13	-12		1			0 33	0	0	0	0	
0	-130	-129		1			0 33	0	0	0	0	
0	-61	-62		1			0 33	0	0	0	0	
0	-62	-63		1			0 33	0	0	0	0	
0	-177	-178		1			0 33	0	0	0	0	
0	-63	-64		1			0 33	0	0	0	0	
0	-178	-179		1			0 33	0	0	0	0	
0	-64	-65		1			0 33	0	0	0	0	
0	-179	-180		1			0 33	0	0	0	0	
0	-180	-181		1			0 33	0	0	0	0	
0	-181	-182		1			0 33	0	0	0	0	

Elenco tipi elementi bidimensionali

Simbologia

Tb =Numero del tipo muro/elemento bidimensionale
Comm. =Commento
Tipo =Tipologia
F = Membranale e Flessionale
M = Membranale
W-RC = Winkler resistente solo a compressione
W-RTC = Winkler resistente a trazione e a compressione
Uso =Utilizzo
G = Generico
P = Parete
S = Soletta/Platea
N = Nucleo
M = Muratura ordinaria
L = Pilastro
MA = Muratura armata
X = Pannello X-LAM
Mat. =Numero del materiale
Crit. =Numero del criterio di progetto
Spess. =Spessore
Kt =Coeff. di sottofondo su suolo elastico alla Winkler

Relazione geotecnica tombino

Tb	Comm.	Tipo	Uso	Mat.	Crit.	Spess. <cm>	Kt <daN/cmc>
1	Pareti	F	P		1	30	
2	Platea	W-RTC	S		1	50	f(strat.)
3	Soletta copertura	F	S		2	50	

Elenco elementi bidimensionali

Simbologia

Bid. = Numero del muro/elemento bidimensionale

Tb = Numero del tipo muro/elemento bidimensionale

FF = Filo fisso

Dy1 = Scost. filo fisso Y1

Dy2 = Scost. filo fisso Y2

Kt = Coeff. di sottofondo su suolo elastico alla Winkler

NN = Nodi

Bid.	Tb	FF	Dy1 <cm>	Dy2 <cm>	Kt <daN/cmc>	NN	Bid.	Tb	FF	Dy1 <cm>	Dy2 <cm>	Kt <daN/cmc>	NN
105	133	0	0			-53 -54 -80 -79	105	133	0	0			-58 -59 -85 -84
105	133	0	0			-59 -60 -86 -85	105	133	0	0			-60 -61 -87 -86
105	133	0	0			-61 -62 -88 -87	105	133	0	0			-62 -63 -89 -88
105	133	0	0			-63 -64 -90 -89	105	133	0	0			-64 -65 -91 -90
105	133	0	0			-79 -80 -106 -105	105	133	0	0			-80 -81 -107 -106
105	133	0	0			-81 -82 -108 -107	105	133	0	0			-82 -83 -109 -108
105	133	0	0			-83 -84 -110 -109	105	133	0	0			-84 -85 -111 -110
105	133	0	0			-85 -86 -112 -111	105	133	0	0			-86 -87 -113 -112
105	133	0	0			-87 -88 -114 -113	105	133	0	0			-88 -89 -115 -114
105	133	0	0			-89 -90 -116 -115	105	133	0	0			-90 -91 -117 -116
105	133	0	0			-105 -106 -171 -170	105	133	0	0			-106 -107 -172 -171
105	133	0	0			-107 -108 -173 -172	105	133	0	0			-108 -109 -174 -173
105	133	0	0			-109 -110 -175 -174	105	133	0	0			-110 -111 -176 -175
105	133	0	0			-111 -112 -177 -176	105	133	0	0			-112 -113 -178 -177
105	133	0	0			-113 -114 -179 -178	105	133	0	0			-114 -115 -180 -179
105	133	0	0			-115 -116 -181 -180	105	133	0	0			-116 -117 -182 -181
105	133	0	0			-57 -58 -84 -83	105	133	0	0			-55 -56 -82 -81
105	133	0	0			-54 -55 -81 -80	105	133	0	0			-56 -57 -83 -82
106	133	0	0			-98 -97 -123 -124	106	133	0	0			-94 -93 -119 -120
106	133	0	0			-93 -92 -118 -119	106	133	0	0			-97 -96 -122 -123
106	133	0	0			-96 -95 -121 -122	106	133	0	0			-95 -94 -120 -121
106	133	0	0			-99 -98 -124 -125	106	133	0	0			-13 -12 -77 -78
106	133	0	0			-70 -69 -95 -96	106	133	0	0			-69 -68 -94 -95
106	133	0	0			-12 -11 -76 -77	106	133	0	0			-11 -10 -75 -76
106	133	0	0			-10 -9 -74 -75	106	133	0	0			-9 -8 -73 -74
106	133	0	0			-8 -7 -72 -73	106	133	0	0			-7 -6 -71 -72
106	133	0	0			-6 -5 -70 -71	106	133	0	0			-5 -4 -69 -70
106	133	0	0			-4 -3 -68 -69	106	133	0	0			-3 -2 -67 -68
106	133	0	0			-2 -1 -66 -67	106	133	0	0			-78 -77 -103 -104
106	133	0	0			-77 -76 -102 -103	106	133	0	0			-76 -75 -101 -102
106	133	0	0			-75 -74 -100 -101	106	133	0	0			-74 -73 -99 -100
106	133	0	0			-73 -72 -98 -99	106	133	0	0			-72 -71 -97 -98
106	133	0	0			-71 -70 -96 -97	106	133	0	0			-103 -102 -128 -129
106	133	0	0			-102 -101 -127 -128	106	133	0	0			-68 -67 -93 -94
106	133	0	0			-67 -66 -92 -93	106	133	0	0			-104 -103 -129 -130
106	133	0	0			-101 -100 -126 -127	106	133	0	0			-100 -99 -125 -126
403	233	0	0	0.19		-65 -52 -51 -64	403	233	0	0	0.19		-50 -37 -36 -49
403	233	0	0	0.19		-30 -17 -16 -29	403	233	0	0	0.19		-17 -4 -3 -16
403	233	0	0	0.19		-55 -42 -41 -54	403	233	0	0	0.19		-42 -29 -28 -41
403	233	0	0	0.19		-29 -16 -15 -28	403	233	0	0	0.19		-16 -3 -2 -15
403	233	0	0	0.19		-54 -41 -40 -53	403	233	0	0	0.19		-41 -28 -27 -40
403	233	0	0	0.19		-28 -15 -14 -27	403	233	0	0	0.19		-15 -2 -1 -14
403	233	0	0	0.19		-38 -25 -24 -37	403	233	0	0	0.19		-25 -12 -11 -24
403	233	0	0	0.19		-63 -50 -49 -62	403	233	0	0	0.19		-32 -19 -18 -31
403	233	0	0	0.19		-37 -24 -23 -36	403	233	0	0	0.19		-24 -11 -10 -23
403	233	0	0	0.19		-62 -49 -48 -61	403	233	0	0	0.19		-49 -36 -35 -48
403	233	0	0	0.19		-36 -23 -22 -35	403	233	0	0	0.19		-23 -10 -9 -22
403	233	0	0	0.19		-61 -48 -47 -60	403	233	0	0	0.19		-48 -35 -34 -47
403	233	0	0	0.19		-35 -22 -21 -34	403	233	0	0	0.19		-22 -9 -8 -21
403	233	0	0	0.19		-60 -47 -46 -59	403	233	0	0	0.19		-47 -34 -33 -46
403	233	0	0	0.19		-34 -21 -20 -33	403	233	0	0	0.19		-21 -8 -7 -20
403	233	0	0	0.19		-59 -46 -45 -58	403	233	0	0	0.19		-46 -33 -32 -45
403	233	0	0	0.19		-33 -20 -19 -32	403	233	0	0	0.19		-20 -7 -6 -19
403	233	0	0	0.19		-58 -45 -44 -57	403	233	0	0	0.19		-45 -32 -31 -44
403	233	0	0	0.19		-18 -5 -4 -17	403	233	0	0	0.19		-19 -6 -5 -18
403	233	0	0	0.19		-57 -44 -43 -56	403	233	0	0	0.19		-44 -31 -30 -43
403	233	0	0	0.19		-31 -18 -17 -30	403	233	0	0	0.19		-26 -13 -12 -25
403	233	0	0	0.19		-56 -43 -42 -55	403	233	0	0	0.19		-43 -30 -29 -42
403	233	0	0	0.19		-52 -39 -38 -51	403	233	0	0	0.19		-39 -26 -25 -38
403	233	0	0	0.19		-51 -38 -37 -50	403	233	0	0	0.19		-64 -51 -50 -63
404	333	0	0			-170 -171 -158 -157	404	333	0	0			-138 -139 -126 -125

Relazione geotecnica tombino

404	3	33	0	0		-139	-140	-127	-126	404	3	33	0	0		-140	-141	-128	-127
404	3	33	0	0		-141	-142	-129	-128	404	3	33	0	0		-142	-143	-130	-129
404	3	33	0	0		-181	-182	-169	-168	404	3	33	0	0		-157	-158	-145	-144
404	3	33	0	0		-158	-159	-146	-145	404	3	33	0	0		-159	-160	-147	-146
404	3	33	0	0		-160	-161	-148	-147	404	3	33	0	0		-161	-162	-149	-148
404	3	33	0	0		-162	-163	-150	-149	404	3	33	0	0		-163	-164	-151	-150
404	3	33	0	0		-164	-165	-152	-151	404	3	33	0	0		-165	-166	-153	-152
404	3	33	0	0		-166	-167	-154	-153	404	3	33	0	0		-167	-168	-155	-154
404	3	33	0	0		-168	-169	-156	-155	404	3	33	0	0		-144	-145	-132	-131
404	3	33	0	0		-145	-146	-133	-132	404	3	33	0	0		-146	-147	-134	-133
404	3	33	0	0		-147	-148	-135	-134	404	3	33	0	0		-148	-149	-136	-135
404	3	33	0	0		-149	-150	-137	-136	404	3	33	0	0		-150	-151	-138	-137
404	3	33	0	0		-151	-152	-139	-138	404	3	33	0	0		-152	-153	-140	-139
404	3	33	0	0		-153	-154	-141	-140	404	3	33	0	0		-154	-155	-142	-141
404	3	33	0	0		-155	-156	-143	-142	404	3	33	0	0		-131	-132	-119	-118
404	3	33	0	0		-132	-133	-120	-119	404	3	33	0	0		-133	-134	-121	-120
404	3	33	0	0		-134	-135	-122	-121	404	3	33	0	0		-135	-136	-123	-122
404	3	33	0	0		-136	-137	-124	-123	404	3	33	0	0		-137	-138	-125	-124
404	3	33	0	0		-171	-172	-159	-158	404	3	33	0	0		-172	-173	-160	-159
404	3	33	0	0		-173	-174	-161	-160	404	3	33	0	0		-174	-175	-162	-161
404	3	33	0	0		-175	-176	-163	-162	404	3	33	0	0		-176	-177	-164	-163
404	3	33	0	0		-177	-178	-165	-164	404	3	33	0	0		-178	-179	-166	-165
404	3	33	0	0		-179	-180	-167	-166	404	3	33	0	0		-180	-181	-168	-167

Carichi

Condizioni di carico elementari

Simbologia

CCE	=	Numero della condizione di carico elementare
Comm.	=	Commento
Tipo CCE	=	Tipo di CCE per calcolo agli stati limite
Sic.	=	Contributo alla sicurezza
		F = a favore
		S = a sfavore
		A = ambigua
Var.	=	Tipo di variabilità
		B = di base
		I = indipendente
		A = ambigua
Dir.	=	Direzione del vento
Tipo	=	Tipologia di pressione vento
		M = Massimizzata
		E = Esterna
		I = Interna
Mx	=	Moltiplicatore della massa in dir. X
My	=	Moltiplicatore della massa in dir. Y
Mz	=	Moltiplicatore della massa in dir. Z
Jpx	=	Moltiplicatore del momento d'inerzia intorno all'asse X
Jpy	=	Moltiplicatore del momento d'inerzia intorno all'asse Y
Jpz	=	Moltiplicatore del momento d'inerzia intorno all'asse Z

CCE	Comm.	Tipo CCE	Sic.	Var.	Dir. <grad>	Tipo	Mx	My	Mz	Jpx	Jpy	Jpz
1	Permanenti strutturali	1 D.M. 08 Permanenti strutturali	S	--	--	--	1	1	0	0	0	1
2	Permanenti non strutturali	2 D.M. 08 Permanenti non strutturali	S	--	--	--	1	1	0	0	0	1
3	Carichi variabili	5 D.M. 08 Variabili Categoria C Ambienti suscettibili di affollamento	S	B	--	--	1	1	0	0	0	1

Elenco peso proprio elementi bidimensionali

Simbologia

Tb	=	Numero del tipo muro/elemento bidimensionale
Comm.	=	Commento
Spess.	=	Spessore
Mat.	=	Materiale
P	=	Peso specifico
PQ	=	Peso specifico per unità di superficie

Tb	Comm.	Spess. <cm>	Mat.	P <daN/mc>	PQ <daN/mq>
1	Pareti	30	Calcestruzzo	2500	750
2	Platea	50	Calcestruzzo	2500	1250
3	Soletta copertura	50	Calcestruzzo	2500	1250

Elenco carichi elementi bidimensionali

Condizione di carico n. 2: Permanenti non strutturali

Carichi uniformi

Simbologia

Bid.	=	Numero del muro/elemento bidimensionale
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Relazione geotecnica tombino

N1 =Nodo1
 N2 =Nodo2
 N3 =Nodo3
 N4 =Nodo4
 T =Tipo di carico
 PP = Peso proprio
 VE = Vento
 M = Manuale
 DC =Direzione del carico
 G = secondo gli assi globali
 L = secondo gli assi locali
 Qx =Carico in dir. X
 Qy =Carico in dir. Y
 Qz =Carico in dir. Z

Bid.	N1	N2	N3	N4	TDC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>
404	-170	-171	-158	-157	MG	0	0	1100
404	-139	-140	-127	-126	MG	0	0	1100
404	-141	-142	-129	-128	MG	0	0	1100
404	-181	-182	-169	-168	MG	0	0	1100
404	-158	-159	-146	-145	MG	0	0	1100
404	-160	-161	-148	-147	MG	0	0	1100
404	-162	-163	-150	-149	MG	0	0	1100
404	-164	-165	-152	-151	MG	0	0	1100
404	-166	-167	-154	-153	MG	0	0	1100
404	-168	-169	-156	-155	MG	0	0	1100
404	-145	-146	-133	-132	MG	0	0	1100
404	-147	-148	-135	-134	MG	0	0	1100
404	-149	-150	-137	-136	MG	0	0	1100
404	-151	-152	-139	-138	MG	0	0	1100
404	-153	-154	-141	-140	MG	0	0	1100
404	-155	-156	-143	-142	MG	0	0	1100
404	-132	-133	-120	-119	MG	0	0	1100
404	-134	-135	-122	-121	MG	0	0	1100
404	-136	-137	-124	-123	MG	0	0	1100
404	-171	-172	-159	-158	MG	0	0	1100
404	-173	-174	-161	-160	MG	0	0	1100
404	-175	-176	-163	-162	MG	0	0	1100
404	-177	-178	-165	-164	MG	0	0	1100
404	-179	-180	-167	-166	MG	0	0	1100

Bid.	N1	N2	N3	N4	TDC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>
404	-138	-139	-126	-125	MG	0	0	1100
404	-140	-141	-128	-127	MG	0	0	1100
404	-142	-143	-130	-129	MG	0	0	1100
404	-157	-158	-145	-144	MG	0	0	1100
404	-159	-160	-147	-146	MG	0	0	1100
404	-161	-162	-149	-148	MG	0	0	1100
404	-163	-164	-151	-150	MG	0	0	1100
404	-165	-166	-153	-152	MG	0	0	1100
404	-167	-168	-155	-154	MG	0	0	1100
404	-144	-145	-132	-131	MG	0	0	1100
404	-146	-147	-134	-133	MG	0	0	1100
404	-148	-149	-136	-135	MG	0	0	1100
404	-150	-151	-138	-137	MG	0	0	1100
404	-152	-153	-140	-139	MG	0	0	1100
404	-154	-155	-142	-141	MG	0	0	1100
404	-131	-132	-119	-118	MG	0	0	1100
404	-133	-134	-121	-120	MG	0	0	1100
404	-135	-136	-123	-122	MG	0	0	1100
404	-137	-138	-125	-124	MG	0	0	1100
404	-172	-173	-160	-159	MG	0	0	1100
404	-174	-175	-162	-161	MG	0	0	1100
404	-176	-177	-164	-163	MG	0	0	1100
404	-178	-179	-166	-165	MG	0	0	1100
404	-180	-181	-168	-167	MG	0	0	1100

Elenco carichi elementi bidimensionali

Condizione di carico n. 2: Permanenti non strutturali

Carichi idrostatici

Simbologia

Bid. =Numero del muro/elemento bidimensionale
 N1 =Nodo1
 N2 =Nodo2
 N3 =Nodo3
 N4 =Nodo4
 Zi =Coordinata Z globale d'inizio carico
 QYi =Componente iniziale del carico in direzione Y locale dell'elemento bidimensionale
 MY =Coordinata Z globale di fine carico
 QYf =Componente finale del carico in direzione Y locale dell'elemento bidimensionale

Bid.	N1	N2	N3	N4	Zi <m>	QYi <daN/m>	MY <m>	QYf <daN/m>
105	-53	-54	-80	-79	0	1020	2.5	0
105	-59	-60	-86	-85	0	1020	2.5	0
105	-61	-62	-88	-87	0	1020	2.5	0
105	-63	-64	-90	-89	0	1020	2.5	0
105	-79	-80	-106	-105	0	1020	2.5	0
105	-81	-82	-108	-107	0	1020	2.5	0
105	-83	-84	-110	-109	0	1020	2.5	0
105	-85	-86	-112	-111	0	1020	2.5	0
105	-87	-88	-114	-113	0	1020	2.5	0
105	-89	-90	-116	-115	0	1020	2.5	0
105	-105	-106	-171	-170	0	1020	2.5	0
105	-107	-108	-173	-172	0	1020	2.5	0
105	-109	-110	-175	-174	0	1020	2.5	0
105	-111	-112	-177	-176	0	1020	2.5	0
105	-113	-114	-179	-178	0	1020	2.5	0
105	-115	-116	-181	-180	0	1020	2.5	0
105	-57	-58	-84	-83	0	1020	2.5	0
105	-54	-55	-81	-80	0	1020	2.5	0
106	-98	-97	-123	-124	0	1020	2.5	0
106	-93	-92	-118	-119	0	1020	2.5	0

Bid.	N1	N2	N3	N4	Zi <m>	QYi <daN/m>	MY <m>	QYf <daN/m>
105	-58	-59	-85	-84	0	1020	2.5	0
105	-60	-61	-87	-86	0	1020	2.5	0
105	-62	-63	-89	-88	0	1020	2.5	0
105	-64	-65	-91	-90	0	1020	2.5	0
105	-80	-81	-107	-106	0	1020	2.5	0
105	-82	-83	-109	-108	0	1020	2.5	0
105	-84	-85	-111	-110	0	1020	2.5	0
105	-86	-87	-113	-112	0	1020	2.5	0
105	-88	-89	-115	-114	0	1020	2.5	0
105	-90	-91	-117	-116	0	1020	2.5	0
105	-106	-107	-172	-171	0	1020	2.5	0
105	-108	-109	-174	-173	0	1020	2.5	0
105	-110	-111	-176	-175	0	1020	2.5	0
105	-112	-113	-178	-177	0	1020	2.5	0
105	-114	-115	-180	-179	0	1020	2.5	0
105	-116	-117	-182	-181	0	1020	2.5	0
105	-55	-56	-82	-81	0	1020	2.5	0
105	-56	-57	-83	-82	0	1020	2.5	0
106	-94	-93	-119	-120	0	1020	2.5	0
106	-97	-96	-122	-123	0	1020	2.5	0

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106	-96	-95	-121	-122	0	1020	2.5	0	106	-95	-94	-120	-121	0	1020	2.5	0
106	-99	-98	-124	-125	0	1020	2.5	0	106	-13	-12	-77	-78	0	1020	2.5	0
106	-70	-69	-95	-96	0	1020	2.5	0	106	-69	-68	-94	-95	0	1020	2.5	0
106	-12	-11	-76	-77	0	1020	2.5	0	106	-11	-10	-75	-76	0	1020	2.5	0
106	-10	-9	-74	-75	0	1020	2.5	0	106	-9	-8	-73	-74	0	1020	2.5	0
106	-8	-7	-72	-73	0	1020	2.5	0	106	-7	-6	-71	-72	0	1020	2.5	0
106	-6	-5	-70	-71	0	1020	2.5	0	106	-5	-4	-69	-70	0	1020	2.5	0
106	-4	-3	-68	-69	0	1020	2.5	0	106	-3	-2	-67	-68	0	1020	2.5	0
106	-2	-1	-66	-67	0	1020	2.5	0	106	-78	-77	-103	-104	0	1020	2.5	0
106	-77	-76	-102	-103	0	1020	2.5	0	106	-76	-75	-101	-102	0	1020	2.5	0
106	-75	-74	-100	-101	0	1020	2.5	0	106	-74	-73	-99	-100	0	1020	2.5	0
106	-73	-72	-98	-99	0	1020	2.5	0	106	-72	-71	-97	-98	0	1020	2.5	0
106	-71	-70	-96	-97	0	1020	2.5	0	106	-103	-102	-128	-129	0	1020	2.5	0
106	-102	-101	-127	-128	0	1020	2.5	0	106	-68	-67	-93	-94	0	1020	2.5	0
106	-67	-66	-92	-93	0	1020	2.5	0	106	-104	-103	-129	-130	0	1020	2.5	0
106	-101	-100	-126	-127	0	1020	2.5	0	106	-100	-99	-125	-126	0	1020	2.5	0

Elenco carichi elementi bidimensionali

Condizione di carico n. 3: Carichi variabili

Carichi uniformi

Bid.	N1	N2	N3	N4	TDC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>	Bid.	N1	N2	N3	N4	TDC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>
403	-65	-52	-51	-64	MG	0	0	1500	403	-50	-37	-36	-49	MG	0	0	1500
403	-30	-17	-16	-29	MG	0	0	1500	403	-17	-4	-3	-16	MG	0	0	1500
403	-55	-42	-41	-54	MG	0	0	1500	403	-42	-29	-28	-41	MG	0	0	1500
403	-29	-16	-15	-28	MG	0	0	1500	403	-16	-3	-2	-15	MG	0	0	1500
403	-54	-41	-40	-53	MG	0	0	1500	403	-41	-28	-27	-40	MG	0	0	1500
403	-28	-15	-14	-27	MG	0	0	1500	403	-15	-2	-1	-14	MG	0	0	1500
403	-38	-25	-24	-37	MG	0	0	1500	403	-25	-12	-11	-24	MG	0	0	1500
403	-63	-50	-49	-62	MG	0	0	1500	403	-32	-19	-18	-31	MG	0	0	1500
403	-37	-24	-23	-36	MG	0	0	1500	403	-24	-11	-10	-23	MG	0	0	1500
403	-62	-49	-48	-61	MG	0	0	1500	403	-49	-36	-35	-48	MG	0	0	1500
403	-36	-23	-22	-35	MG	0	0	1500	403	-23	-10	-9	-22	MG	0	0	1500
403	-61	-48	-47	-60	MG	0	0	1500	403	-48	-35	-34	-47	MG	0	0	1500
403	-35	-22	-21	-34	MG	0	0	1500	403	-22	-9	-8	-21	MG	0	0	1500
403	-60	-47	-46	-59	MG	0	0	1500	403	-47	-34	-33	-46	MG	0	0	1500
403	-34	-21	-20	-33	MG	0	0	1500	403	-21	-8	-7	-20	MG	0	0	1500
403	-59	-46	-45	-58	MG	0	0	1500	403	-46	-33	-32	-45	MG	0	0	1500
403	-33	-20	-19	-32	MG	0	0	1500	403	-20	-7	-6	-19	MG	0	0	1500
403	-58	-45	-44	-57	MG	0	0	1500	403	-45	-32	-31	-44	MG	0	0	1500
403	-18	-5	-4	-17	MG	0	0	1500	403	-19	-6	-5	-18	MG	0	0	1500
403	-57	-44	-43	-56	MG	0	0	1500	403	-44	-31	-30	-43	MG	0	0	1500
403	-31	-18	-17	-30	MG	0	0	1500	403	-26	-13	-12	-25	MG	0	0	1500
403	-56	-43	-42	-55	MG	0	0	1500	403	-43	-30	-29	-42	MG	0	0	1500
403	-52	-39	-38	-51	MG	0	0	1500	403	-39	-26	-25	-38	MG	0	0	1500
403	-51	-38	-37	-50	MG	0	0	1500	403	-64	-51	-50	-63	MG	0	0	1500
404	-170	-171	-158	-157	MG	0	0	3000	404	-138	-139	-126	-125	MG	0	0	3000
404	-139	-140	-127	-126	MG	0	0	3000	404	-140	-141	-128	-127	MG	0	0	3000
404	-141	-142	-129	-128	MG	0	0	3000	404	-142	-143	-130	-129	MG	0	0	3000
404	-181	-182	-169	-168	MG	0	0	3000	404	-157	-158	-145	-144	MG	0	0	3000
404	-158	-159	-146	-145	MG	0	0	3000	404	-159	-160	-147	-146	MG	0	0	3000
404	-160	-161	-148	-147	MG	0	0	3000	404	-161	-162	-149	-148	MG	0	0	3000
404	-162	-163	-150	-149	MG	0	0	3000	404	-163	-164	-151	-150	MG	0	0	3000
404	-164	-165	-152	-151	MG	0	0	3000	404	-165	-166	-153	-152	MG	0	0	3000
404	-166	-167	-154	-153	MG	0	0	3000	404	-167	-168	-155	-154	MG	0	0	3000
404	-168	-169	-156	-155	MG	0	0	3000	404	-144	-145	-132	-131	MG	0	0	3000
404	-145	-146	-133	-132	MG	0	0	3000	404	-146	-147	-134	-133	MG	0	0	3000
404	-147	-148	-135	-134	MG	0	0	3000	404	-148	-149	-136	-135	MG	0	0	3000
404	-149	-150	-137	-136	MG	0	0	3000	404	-150	-151	-138	-137	MG	0	0	3000
404	-151	-152	-139	-138	MG	0	0	3000	404	-152	-153	-140	-139	MG	0	0	3000
404	-153	-154	-141	-140	MG	0	0	3000	404	-154	-155	-142	-141	MG	0	0	3000
404	-155	-156	-143	-142	MG	0	0	3000	404	-131	-132	-119	-118	MG	0	0	3000
404	-132	-133	-120	-119	MG	0	0	3000	404	-133	-134	-121	-120	MG	0	0	3000
404	-134	-135	-122	-121	MG	0	0	3000	404	-135	-136	-123	-122	MG	0	0	3000
404	-136	-137	-124	-123	MG	0	0	3000	404	-137	-138	-125	-124	MG	0	0	3000
404	-171	-172	-159	-158	MG	0	0	3000	404	-172	-173	-160	-159	MG	0	0	3000
404	-173	-174	-161	-160	MG	0	0	3000	404	-174	-175	-162	-161	MG	0	0	3000
404	-175	-176	-163	-162	MG	0	0	3000	404	-176	-177	-164	-163	MG	0	0	3000
404	-177	-178	-165	-164	MG	0	0	3000	404	-178	-179	-166	-165	MG	0	0	3000
404	-179	-180	-167	-166	MG	0	0	3000	404	-180	-181	-168	-167	MG	0	0	3000

Risultati del calcolo

Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:
 ModeSt ver. 8.14, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti:
 Xfinest ver. 2015, prodotto da Ce.A.S. S.r.l. - Milano

Relazione geotecnica tombino

Tipo di normativa: stati limite D.M. 08
Tipo di calcolo: analisi sismica statica
Vincoli esterni: Considera sempre vincoli assegnati in modellazione
Schematizzazione piani rigidi: metodo Master-Slave
Modalità di recupero masse secondarie: trasferire all'impalcato più vicino con modifica XY baricentro

Generazione combinazioni

- Lineari: Sì
- Valuta spostamenti e non sollecitazioni: No
- Buckling: No

Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: No
- Uniformare i carichi variabili: No
- Massimizzare i carichi variabili: No
- Minimo carico da considerare: 0.00 <daN/m>
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: No
- Trascura deformabilità a taglio delle aste: No
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì
- Soluzione matrice con metodo ver. 5.1: No
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No

Dati struttura

- Zona sismica: zona 1
- Sito di costruzione: san bartolomeo in galdo LON. 15.01430 LAT. 41.41160
Contenuto tra ID reticolo: 30548 30770 30547 30769

Simbologia

TCC=Tipo di combinazione di carico
SLU = Stato limite ultimo
SLU S = Stato limite ultimo (azione sismica)
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
SLD = Stato limite di danno
SLV = Stato limite di salvaguardia della vita
SLC = Stato limite di prevenzione del collasso
SLO = Stato limite di operatività
SLU I = Stato limite di resistenza al fuoco
T_R =Periodo di ritorno <anni>
A_g =Accelerazione orizzontale massima al sito
FO =Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
TC* =Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>
S_s =Coefficiente di amplificazione stratigrafica
C_c =Coefficiente funzione della categoria del suolo

TCC	T _R	A _g <g>	FO	TC*	S _s	C _c
SLO	30	0.0508	2.42	0.29	1.5	1.58
SLD	50	0.0630	2.48	0.33	1.5	1.51
SLV	475	0.1598	2.59	0.43	1.45	1.39

- Edificio esistente: No
- Tipo di opera: Opera ordinaria
- Vita nominale V_N: 50.00
- Classe d'uso: Classe II
- Applica semplificazioni per zona 4: No
- SL Esercizio: SLO-Pvr 81.00, SLD-Pvr 63.00
- SL Ultimi: SLV-Pvr 10.00, SLC-Pvr No
- Classe di duttilità: Classe B
- Quota di riferimento: 0.00 <m>
- Altezza della struttura: 2.50 <m>
- Numero piani edificio: 1
- Coefficiente θ : 0.00
- Edificio regolare in altezza: Sì
- Edificio regolare in pianta: No
- Forze orizzontali convenzionali per stati limite non sismici: 1.00%
- Genera stati limite per verifiche di resistenza al fuoco: No

Dati di piano

Simbologia

Imp. = Numero dell'impalcato
 Lx = Dimensione del piano in dir. X
 Ly = Dimensione del piano in dir. Y
 Ex = Eccentricità in dir. X
 Ey = Eccentricità in dir. Y
 Ea = Eccentricità complessiva

Imp.	Lx <m>	Ly <m>	Ex <m>	Ey <m>	Ea <m>
1	12	3.2	0.6	0.16	0.62

Dati di calcolo

- Categoria del suolo di fondazione: C
 - Tipologia edificio: c.a. o prefabbricato a pareti accoppiate
 Coeff. C_1 : 0.05
 Periodo T_1 : 0.09941
 Coeff. λ SLO: 1.00
 Coeff. λ SLD: 1.00
 Coeff. λ SLV: 1.00
 Rapporto di sovraresistenza (α_u/α_1): 1.10
 Valore di riferimento del fattore di struttura (q_0): 3.30
 Fattore riduttivo (K_w): 0.50
 Fattore riduttivo regolarità in altezza (K_R): 1.00
 Fattore di struttura (q): 1.65

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media $i \leq 15^\circ$
 - Coeff. amplificazione topografica S_T : 1.00
 - Fattore di struttura per sisma verticale (q_v): 1.50
 - Smorzamento spettro: 5.00%

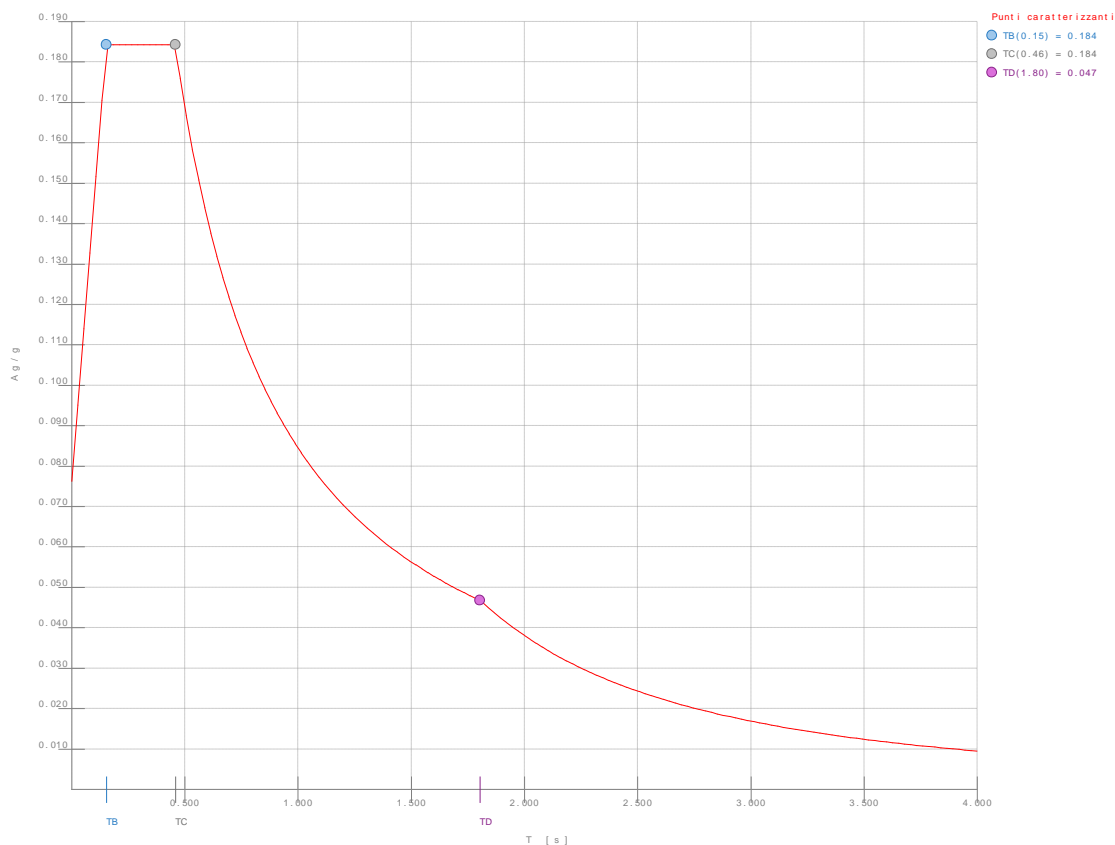


Figura numero 1: Spettro SLO

Relazione geotecnica tombino

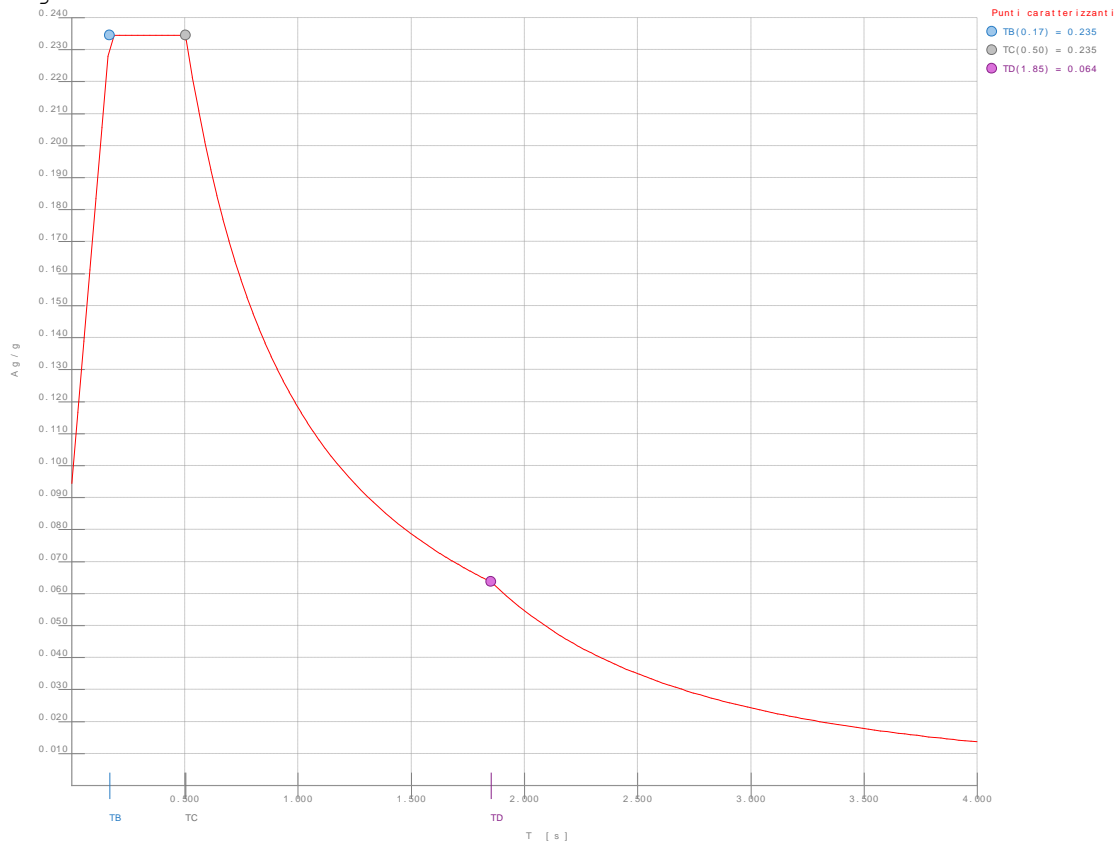


Figura numero 2: Spettro SLD

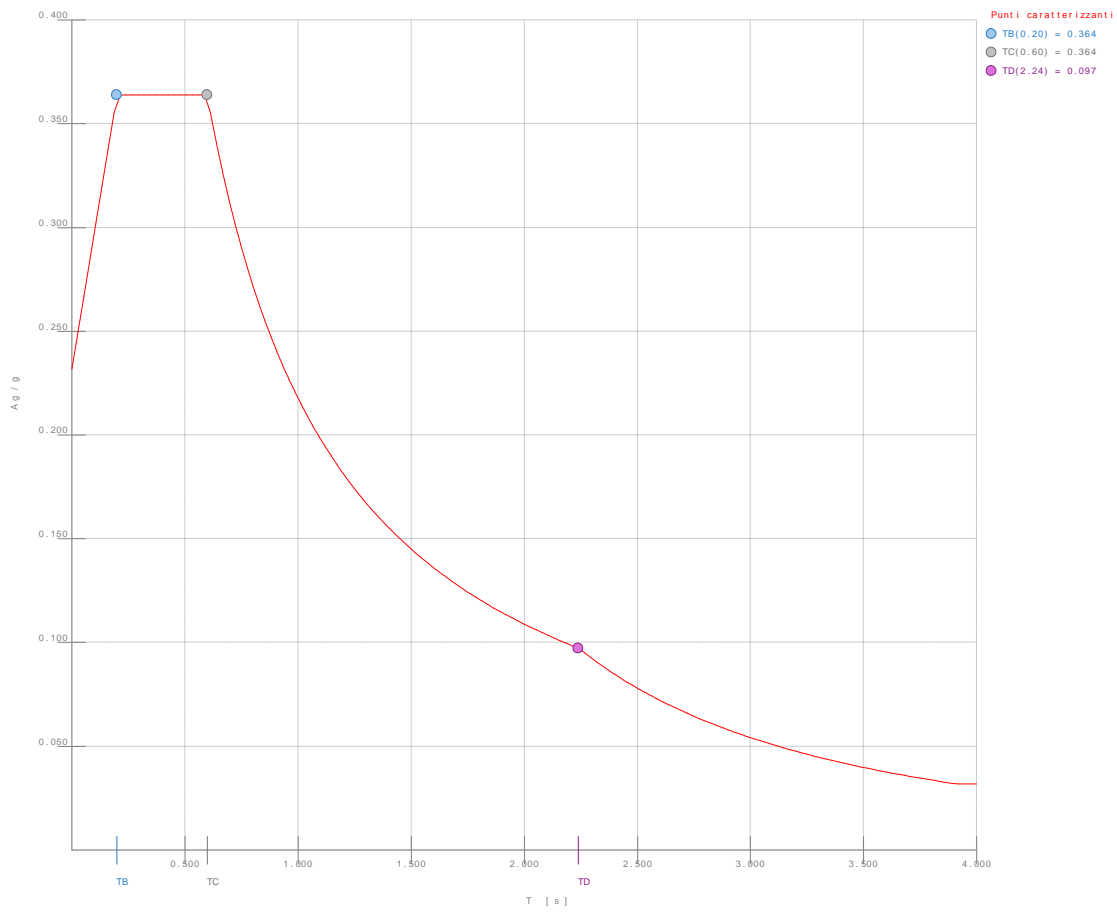


Figura numero 3: Spettro SLV

- Angolo di ingresso del sisma: 0.00 <grad>
- Tipo di combinazione sismica: 30% esteso

Relazione geotecnica tombino

Condizioni di carico elementari

Simbologia

CCE = Numero della condizione di carico elementare
 Comm. = Commento
 Tipo CCE = Tipo di CCE per calcolo agli stati limite
 Sic. = Contributo alla sicurezza
 F = a favore
 S = a sfavore
 A = ambigua
 Var. = Tipo di variabilità
 B = di base
 I = indipendente
 A = ambigua
 Dir. = Direzione del vento
 Tipo = Tipologia di pressione vento
 M = Massimizzata
 E = Esterna
 I = Interna
 Mx = Moltiplicatore della massa in dir. X
 My = Moltiplicatore della massa in dir. Y
 Mz = Moltiplicatore della massa in dir. Z
 Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
 Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
 Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z

CCE	Comm.	Tipo CCE	Sic.	Var.	Dir. <grad>	Tipo	Mx	My	Mz	Jpx	Jpy	Jpz
1	Permanenti strutturali	1	S	--	--	--	1	1	0	0	0	1
2	Permanenti non strutturali	2	S	--	--	--	1	1	0	0	0	1
3	Carichi variabili	5	S	B	--	--	1	1	0	0	0	1

Elenco tipi CCE definiti

Simbologia

Tipo CCE = Tipo condizione di carico elementare
 Comm. = Commento
 Tipo = Tipologia
 G = Permanente
 Qv = Variabile vento
 Q = Variabile
 I = Da ignorare
 A = Azione eccezionale
 P = Precompressione
 Durata = Durata del carico
 N = Non definita
 P = Permanente
 L = Lunga
 M = Media
 B = Breve
 I = Istantanea
 γ_{min} = Coeff. γ_{min}
 γ_{max} = Coeff. γ_{max}
 ψ_0 = Coeff. ψ_0
 ψ_1 = Coeff. ψ_1
 ψ_2 = Coeff. ψ_2
 $\psi_{0,s}$ = Coeff. ψ_0 sismico (D.M. 96)

Tipo CCE	Comm.	Tipo	Durata	γ_{min}	γ_{max}	ψ_0	ψ_1	ψ_2	$\psi_{0,s}$
1	D.M. 08 Permanenti strutturali	G	N	1	1.3				
2	D.M. 08 Permanenti non strutturali	G	N	0	1.5				
5	D.M. 08 Variabili Categoria C Ambienti suscettibili di affollamento	Q	N	0	1.5	0.7	0.7	0.6	0

Ambienti di carico

Simbologia

N = Numero
 Comm. = Commento
 1 = Permanenti strutturali
 2 = Permanenti non strutturali
 3 = Carichi variabili
 F = azioni orizzontali convenzionali
 SLU = Stato limite ultimo
 SLR = Stato limite per combinazioni rare
 SLF = Stato limite per combinazioni frequenti
 SLQ/D = Stato limite per combinazioni quasi permanenti o di danno
 S = Sì
 N = No

N	Comm.	1	2	3	F	S	SLU	SLR	SLF	SLQ
1	Calcolo sismico	S	S	S	N	S	N	N	N	
2	Calcolo statico	S	S	S	N	S	S	S	S	

Elenco combinazioni di carico simboliche

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
 Comm. = Commento
 TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLU S = Stato limite ultimo (azione sismica)
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SLV = Stato limite di salvaguardia della vita
 SLC = Stato limite di prevenzione del collasso
 SLO = Stato limite di operatività
 SLU I = Stato limite di resistenza al fuoco

CC	Comm.	TCC	1	2	3	F	S
1	Amb. 1 (Sisma)	SLU S	1	1	ψ_2	-----	1
2	Amb. 2 (SLU)	SLU	γ_{max}	γ_{max}	γ_{max}	1	-----
3	Amb. 2 (SLE R)	SLE R	1	1	1	1	-----
4	Amb. 2 (SLE F)	SLE F	1	1	ψ_1	1	-----
5	Amb. 2 (SLE Q)	SLE Q	1	1	ψ_2	1	-----

Genera le combinazioni con un solo carico di tipo variabile come di base: No

Considera sollecitazioni dinamiche con segno dei modi principali: No

Combinazioni delle CCE

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
 Comm. = Commento
 TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLU S = Stato limite ultimo (azione sismica)
 SLE R = Stato limite d'esercizio, combinazione rara
 SLE F = Stato limite d'esercizio, combinazione frequente
 SLE Q = Stato limite d'esercizio, combinazione quasi permanente
 SLD = Stato limite di danno
 SLV = Stato limite di salvaguardia della vita
 SLC = Stato limite di prevenzione del collasso
 SLO = Stato limite di operatività
 SLU I = Stato limite di resistenza al fuoco

An. = Tipo di analisi
 L = Lineare
 NL = Non lineare
 Bk = Buckling
 S = Sì
 N = No

CC	Comm.	TCC	An.	Bk	1	2	3	F X	F Y	Mt	S X	S Y
1	CC 1 - Amb. 1 (SLU S) S Mt+X+0.3Y	SLV	L	N	1	1	0.6	0	0	1	1	0.3
2	CC 2 - Amb. 1 (SLE) S Mt+X+0.3Y	SLD	L	N	1	1	0.6	0	0	1	1	0.3
3	CC 3 - Amb. 1 (SLE) S Mt+X+0.3Y	SLO	L	N	1	1	0.6	0	0	1	1	0.3
4	CC 4 - Amb. 1 (SLU S) S Mt+X-0.3Y	SLV	L	N	1	1	0.6	0	0	1	-1	-0.3
5	CC 5 - Amb. 1 (SLE) S Mt+X-0.3Y	SLD	L	N	1	1	0.6	0	0	1	-1	-0.3
6	CC 6 - Amb. 1 (SLE) S Mt+X-0.3Y	SLO	L	N	1	1	0.6	0	0	1	-1	-0.3
7	CC 7 - Amb. 1 (SLU S) S Mt-X+0.3Y	SLV	L	N	1	1	0.6	0	0	1	-1	0.3
8	CC 8 - Amb. 1 (SLE) S Mt-X+0.3Y	SLD	L	N	1	1	0.6	0	0	1	-1	0.3
9	CC 9 - Amb. 1 (SLE) S Mt-X+0.3Y	SLO	L	N	1	1	0.6	0	0	1	-1	0.3
10	CC 10 - Amb. 1 (SLU S) S Mt-X-0.3Y	SLV	L	N	1	1	0.6	0	0	1	-1	-0.3
11	CC 11 - Amb. 1 (SLE) S Mt-X-0.3Y	SLD	L	N	1	1	0.6	0	0	1	-1	-0.3
12	CC 12 - Amb. 1 (SLE) S Mt-X-0.3Y	SLO	L	N	1	1	0.6	0	0	1	-1	-0.3
13	CC 13 - Amb. 1 (SLU S) S Mt+0.3X+Y	SLV	L	N	1	1	0.6	0	0	1	0.3	1
14	CC 14 - Amb. 1 (SLE) S Mt+0.3X+Y	SLD	L	N	1	1	0.6	0	0	1	0.3	1
15	CC 15 - Amb. 1 (SLE) S Mt+0.3X+Y	SLO	L	N	1	1	0.6	0	0	1	0.3	1
16	CC 16 - Amb. 1 (SLU S) S Mt-0.3X+Y	SLV	L	N	1	1	0.6	0	0	1	-0.3	1
17	CC 17 - Amb. 1 (SLE) S Mt-0.3X+Y	SLD	L	N	1	1	0.6	0	0	1	-0.3	1
18	CC 18 - Amb. 1 (SLE) S Mt-0.3X+Y	SLO	L	N	1	1	0.6	0	0	1	-0.3	1
19	CC 19 - Amb. 1 (SLU S) S Mt+0.3X-Y	SLV	L	N	1	1	0.6	0	0	1	0.3	-1
20	CC 20 - Amb. 1 (SLE) S Mt+0.3X-Y	SLD	L	N	1	1	0.6	0	0	1	0.3	-1
21	CC 21 - Amb. 1 (SLE) S Mt+0.3X-Y	SLO	L	N	1	1	0.6	0	0	1	0.3	-1
22	CC 22 - Amb. 1 (SLU S) S Mt-0.3X-Y	SLV	L	N	1	1	0.6	0	0	1	-0.3	-1
23	CC 23 - Amb. 1 (SLE) S Mt-0.3X-Y	SLD	L	N	1	1	0.6	0	0	1	-0.3	-1
24	CC 24 - Amb. 1 (SLE) S Mt-0.3X-Y	SLO	L	N	1	1	0.6	0	0	1	-0.3	-1
25	CC 25 - Amb. 1 (SLU S) S -Mt+X+0.3Y	SLV	L	N	1	1	0.6	0	0	-1	1	0.3
26	CC 26 - Amb. 1 (SLE) S -Mt+X+0.3Y	SLD	L	N	1	1	0.6	0	0	-1	1	0.3
27	CC 27 - Amb. 1 (SLE) S -Mt+X+0.3Y	SLO	L	N	1	1	0.6	0	0	-1	1	0.3
28	CC 28 - Amb. 1 (SLU S) S -Mt+X-0.3Y	SLV	L	N	1	1	0.6	0	0	-1	1	-0.3

Relazione geotecnica tombino

29	CC 29 - Amb. 1 (SLE) S -Mt+X-0.3Y	SLD	L	N	1	1	0.6	0	0	-1	1	-0.3
30	CC 30 - Amb. 1 (SLE) S -Mt+X-0.3Y	SLO	L	N	1	1	0.6	0	0	-1	1	-0.3
31	CC 31 - Amb. 1 (SLU S) S -Mt-X+0.3Y	SLV	L	N	1	1	0.6	0	0	-1	-1	0.3
32	CC 32 - Amb. 1 (SLE) S -Mt-X+0.3Y	SLD	L	N	1	1	0.6	0	0	-1	-1	0.3
33	CC 33 - Amb. 1 (SLE) S -Mt-X+0.3Y	SLO	L	N	1	1	0.6	0	0	-1	-1	0.3
34	CC 34 - Amb. 1 (SLU S) S -Mt-X-0.3Y	SLV	L	N	1	1	0.6	0	0	-1	-1	-0.3
35	CC 35 - Amb. 1 (SLE) S -Mt-X-0.3Y	SLD	L	N	1	1	0.6	0	0	-1	-1	-0.3
36	CC 36 - Amb. 1 (SLE) S -Mt-X-0.3Y	SLO	L	N	1	1	0.6	0	0	-1	-1	-0.3
37	CC 37 - Amb. 1 (SLU S) S -Mt+0.3X+Y	SLV	L	N	1	1	0.6	0	0	-1	0.3	1
38	CC 38 - Amb. 1 (SLE) S -Mt+0.3X+Y	SLD	L	N	1	1	0.6	0	0	-1	0.3	1
39	CC 39 - Amb. 1 (SLE) S -Mt+0.3X+Y	SLO	L	N	1	1	0.6	0	0	-1	0.3	1
40	CC 40 - Amb. 1 (SLU S) S -Mt-0.3X+Y	SLV	L	N	1	1	0.6	0	0	-1	-0.3	1
41	CC 41 - Amb. 1 (SLE) S -Mt-0.3X+Y	SLD	L	N	1	1	0.6	0	0	-1	-0.3	1
42	CC 42 - Amb. 1 (SLE) S -Mt-0.3X+Y	SLO	L	N	1	1	0.6	0	0	-1	-0.3	1
43	CC 43 - Amb. 1 (SLU S) S -Mt+0.3X-Y	SLV	L	N	1	1	0.6	0	0	-1	0.3	-1
44	CC 44 - Amb. 1 (SLE) S -Mt+0.3X-Y	SLD	L	N	1	1	0.6	0	0	-1	0.3	-1
45	CC 45 - Amb. 1 (SLE) S -Mt+0.3X-Y	SLO	L	N	1	1	0.6	0	0	-1	0.3	-1
46	CC 46 - Amb. 1 (SLU S) S -Mt-0.3X-Y	SLV	L	N	1	1	0.6	0	0	-1	-0.3	-1
47	CC 47 - Amb. 1 (SLE) S -Mt-0.3X-Y	SLD	L	N	1	1	0.6	0	0	-1	-0.3	-1
48	CC 48 - Amb. 1 (SLE) S -Mt-0.3X-Y	SLO	L	N	1	1	0.6	0	0	-1	-0.3	-1
49	CC 49 - Amb. 2 (SLU) F X	SLU	L	N	1.3	1.5	1.5	1	0	0	0	0
50	CC 50 - Amb. 2 (SLU) F -X	SLU	L	N	1.3	1.5	1.5	-1	0	0	0	0
51	CC 51 - Amb. 2 (SLU) F Y	SLU	L	N	1.3	1.5	1.5	0	1	0	0	0
52	CC 52 - Amb. 2 (SLU) F -Y	SLU	L	N	1.3	1.5	1.5	0	-1	0	0	0
53	CC 53 - Amb. 2 (SLE R) F X	SLE R	L	N	1	1	1	1	0	0	0	0
54	CC 54 - Amb. 2 (SLE R) F -X	SLE R	L	N	1	1	1	-1	0	0	0	0
55	CC 55 - Amb. 2 (SLE R) F Y	SLE R	L	N	1	1	1	0	1	0	0	0
56	CC 56 - Amb. 2 (SLE R) F -Y	SLE R	L	N	1	1	1	0	-1	0	0	0
57	CC 57 - Amb. 2 (SLE F) F X	SLE F	L	N	1	1	0.7	1	0	0	0	0
58	CC 58 - Amb. 2 (SLE F) F -X	SLE F	L	N	1	1	0.7	-1	0	0	0	0
59	CC 59 - Amb. 2 (SLE F) F Y	SLE F	L	N	1	1	0.7	0	1	0	0	0
60	CC 60 - Amb. 2 (SLE F) F -Y	SLE F	L	N	1	1	0.7	0	-1	0	0	0
61	CC 61 - Amb. 2 (SLE Q) F X	SLE Q	L	N	1	1	0.6	1	0	0	0	0
62	CC 62 - Amb. 2 (SLE Q) F -X	SLE Q	L	N	1	1	0.6	-1	0	0	0	0
63	CC 63 - Amb. 2 (SLE Q) F Y	SLE Q	L	N	1	1	0.6	0	1	0	0	0
64	CC 64 - Amb. 2 (SLE Q) F -Y	SLE Q	L	N	1	1	0.6	0	-1	0	0	0

Elenco baricentri e masse impalcato

Simbologia

Imp. =Numero dell'impalcato

X =Coordinata X

Y =Coordinata Y

Z =Coordinata Z

Mo =Massa orizzontale

Jpz =Momento d'inerzia polare intorno all'asse Z

Imp.	X <m>	Y <m>	Z <m>	Mo <kg>	Jpz <kg*mq>
1	6	1.6	2.5	200673	2695330

Totali masse impalcato

Mo <kg>	Jpz <kg*mq>
200673	2695330

Elenco forze sismiche di impalcato allo SLO

Simbologia

Imp. =Numero dell'impalcato

cx =Coeff. c in dir. X

cy =Coeff. c in dir. Y

Fx =Forza in dir. X

Fy =Forza in dir. Y

Mz =Momento intorno all'asse Z

Imp.	cx	cy	Fx <daN>	Fy <daN>	Mz <daNm>
1	1	1	28857.3	28857.3	17919.4

Totali forze sismiche

Fx <daN>	Fy <daN>	Mz <daNm>
28857.3	28857.3	17919.4

Elenco forze sismiche di impalcato allo SLD

Imp.	cx	cy	Fx <daN>	Fy <daN>	Mz <daNm>
1	1	1	34943.4	34943.4	21698.7

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Totali forze sismiche

Fx <daN>	Fy <daN>	Mz <daNm>
34943.4	34943.4	21698.7

Elenco forze sismiche di impalcato allo SLV

Imp.	cx	cy	Fx <daN>	Fy <daN>	Mz <daNm>
1	1	1	58603.5	58603.5	36390.8

Totali forze sismiche

Fx <daN>	Fy <daN>	Mz <daNm>
58603.5	58603.5	36390.8

Elenco pesi e forze fittizie impalcato

Simbologia

Imp. = Numero dell'impalcato

Peso = Peso

Fx = Forza in dir. X

Fy = Forza in dir. Y

Imp.	Peso <daN>	Fx <daN>	Fy <daN>
1	242940	2429.4	2429.4

Spostamenti dei nodi allo stato limite ultimo

Simbologia

Nodo = Numero del nodo

Sx = Spostamento in dir. X

CC = Numero della combinazione delle condizioni di carico elementari

Sy = Spostamento in dir. Y

Sz = Spostamento in dir. Z

Rx = Rotazione intorno all'asse X

Ry = Rotazione intorno all'asse Y

Rz = Rotazione intorno all'asse Z

Nodo		Sx <cm>	CC	Sy <cm>	CC	Sz <cm>	CC	Rx <rad>	CC	Ry <rad>	CC	Rz <rad>	CC
-182	Max	1.78	25	25.14	13	13.29	22	0.1	19	0.01	28	0	1
-182	Min.	-1.78	7	-25.14	43	-21.14	37	-0.1	40	-0.01	7	0	25
-181	Max	1.78	25	25.14	13	13.07	22	0.1	19	0.01	25	0	1
-181	Min.	-1.78	7	-25.14	43	-20.92	37	-0.1	40	-0.01	10	0	25
-180	Max	1.78	25	25.14	13	12.86	22	0.1	19	0.01	25	0	1
-180	Min.	-1.78	7	-25.14	43	-20.71	37	-0.1	40	-0.01	10	0	25
-179	Max	1.78	25	25.14	13	12.65	22	0.1	19	0.01	28	0	1
-179	Min.	-1.78	7	-25.14	43	-20.5	37	-0.1	40	-0.01	7	0	25
-178	Max	1.78	25	25.14	13	12.43	22	0.1	19	0.01	25	0	1
-178	Min.	-1.78	7	-25.14	43	-20.28	37	-0.1	40	-0.01	10	0	25
-177	Max	1.78	25	25.14	13	12.22	22	0.1	19	0.01	28	0	1
-177	Min.	-1.78	7	-25.14	43	-20.07	37	-0.1	40	-0.01	7	0	25
-176	Max	1.78	25	25.14	13	12.01	19	0.1	19	0.01	25	0	1
-176	Min.	-1.78	7	-25.14	19	-19.86	13	-0.1	13	-0.01	7	0	25
-175	Max	1.78	25	25.14	37	12.22	43	0.1	46	0.01	25	0	1
-175	Min.	-1.78	7	-25.14	19	-20.07	16	-0.1	13	-0.01	10	0	25
-174	Max	1.78	25	25.14	37	12.43	43	0.1	46	0.01	28	0	1
-174	Min.	-1.78	7	-25.14	19	-20.28	16	-0.1	13	-0.01	7	0	25
-173	Max	1.78	25	25.14	37	12.65	43	0.1	46	0.01	25	0	1
-173	Min.	-1.78	7	-25.14	19	-20.5	16	-0.1	13	-0.01	10	0	25
-172	Max	1.78	25	25.14	37	12.86	43	0.1	46	0.01	28	0	1
-172	Min.	-1.78	7	-25.14	19	-20.71	16	-0.1	13	-0.01	7	0	25
-171	Max	1.78	25	25.14	37	13.07	43	0.1	46	0.01	28	0	1
-171	Min.	-1.78	7	-25.14	19	-20.92	16	-0.1	13	-0.01	7	0	25
-170	Max	1.78	25	25.14	37	13.29	43	0.1	46	0.01	25	0	1
-170	Min.	-1.78	7	-25.14	19	-21.14	16	-0.1	13	-0.01	10	0	25
-169	Max	1.78	25	25.14	13	5.3	22	0.1	19	0.01	28	0	1
-169	Min.	-1.78	7	-25.14	43	-13.17	37	-0.1	40	-0.01	7	0	25
-168	Max	1.78	25	25.14	13	5.09	22	0.1	19	0.01	25	0	1
-168	Min.	-1.78	7	-25.14	43	-12.96	37	-0.1	40	-0.01	10	0	25
-167	Max	1.78	25	25.14	13	4.88	22	0.1	19	0.01	25	0	1
-167	Min.	-1.78	7	-25.14	43	-12.75	37	-0.1	40	-0.01	10	0	25
-166	Max	1.78	25	25.14	13	4.66	22	0.1	19	0.01	28	0	1
-166	Min.	-1.78	7	-25.14	43	-12.53	37	-0.1	40	-0.01	7	0	25
-165	Max	1.78	25	25.14	13	4.45	22	0.1	19	0.01	25	0	1
-165	Min.	-1.78	7	-25.14	43	-12.32	37	-0.1	40	-0.01	10	0	25
-164	Max	1.78	25	25.14	13	4.24	22	0.1	19	0.01	25	0	1
-164	Min.	-1.78	7	-25.14	43	-12.11	37	-0.1	40	-0.01	10	0	25
-163	Max	1.78	25	25.14	13	4.02	19	0.1	19	0.01	25	0	1

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-163	Min.	-1.78	7	-25.14	19	-11.89	13	-0.1	13	-0.01	7	0	25
-162	Max	1.78	25	25.14	37	4.24	43	0.1	46	0.01	28	0	1
-162	Min.	-1.78	7	-25.14	19	-12.11	16	-0.1	13	-0.01	7	0	25
-161	Max	1.78	25	25.14	37	4.45	43	0.1	46	0.01	28	0	1
-161	Min.	-1.78	7	-25.14	19	-12.32	16	-0.1	13	-0.01	7	0	25
-160	Max	1.78	25	25.14	37	4.66	43	0.1	46	0.01	25	0	1
-160	Min.	-1.78	7	-25.14	19	-12.53	16	-0.1	13	-0.01	10	0	25
-159	Max	1.78	25	25.14	37	4.88	43	0.1	46	0.01	28	0	1
-159	Min.	-1.78	7	-25.14	19	-12.75	16	-0.1	13	-0.01	7	0	25
-158	Max	1.78	25	25.14	37	5.09	43	0.1	46	0.01	28	0	1
-158	Min.	-1.78	7	-25.14	19	-12.96	16	-0.1	13	-0.01	7	0	25
-157	Max	1.78	25	25.14	37	5.3	43	0.1	46	0.01	25	0	1
-157	Min.	-1.78	7	-25.14	19	-13.17	16	-0.1	13	-0.01	10	0	25
-156	Max	1.78	1	25.14	13	0.32	7	0.1	19	0.01	1	0	1
-156	Min.	-1.78	7	-25.14	43	-8.2	1	-0.1	37	-0.01	7	0	25
-155	Max	1.78	1	25.14	13	-0.39	7	0.1	19	0.01	1	0	1
-155	Min.	-1.78	7	-25.14	43	-7.49	1	-0.1	37	-0.01	7	0	25
-154	Max	1.78	1	25.14	13	-1.1	7	0.1	19	0.01	1	0	1
-154	Min.	-1.78	7	-25.14	43	-6.97	49	-0.1	37	-0.01	7	0	25
-153	Max	1.78	1	25.14	13	-1.81	7	0.1	19	0.01	1	0	1
-153	Min.	-1.78	7	-25.14	43	-6.97	49	-0.1	37	-0.01	7	0	25
-152	Max	1.78	1	25.14	13	-2.52	7	0.1	19	0.01	1	0	1
-152	Min.	-1.78	7	-25.14	43	-6.96	49	-0.1	37	-0.01	7	0	25
-151	Max	1.78	1	25.14	13	-3.23	7	0.1	19	0.01	1	0	1
-151	Min.	-1.78	7	-25.14	43	-6.95	49	-0.1	37	-0.01	7	0	25
-150	Max	1.78	1	25.14	13	-3.94	1	0.1	19	0.01	1	0	1
-150	Min.	-1.78	7	-25.14	19	-6.95	49	-0.1	13	-0.01	7	0	25
-149	Max	1.78	1	25.14	37	-3.23	1	0.1	43	0.01	1	0	1
-149	Min.	-1.78	7	-25.14	19	-6.95	50	-0.1	13	-0.01	7	0	25
-148	Max	1.78	1	25.14	37	-2.52	1	0.1	43	0.01	1	0	1
-148	Min.	-1.78	7	-25.14	19	-6.96	50	-0.1	13	-0.01	7	0	25
-147	Max	1.78	1	25.14	37	-1.81	1	0.1	43	0.01	1	0	1
-147	Min.	-1.78	7	-25.14	19	-6.97	50	-0.1	13	-0.01	7	0	25
-146	Max	1.78	1	25.14	37	-1.1	1	0.1	43	0.01	1	0	1
-146	Min.	-1.78	7	-25.14	19	-6.97	50	-0.1	13	-0.01	7	0	25
-145	Max	1.78	1	25.14	37	-0.39	1	0.1	43	0.01	1	0	1
-145	Min.	-1.78	7	-25.14	19	-7.49	7	-0.1	13	-0.01	7	0	25
-144	Max	1.78	1	25.14	37	0.32	1	0.1	43	0.01	1	0	1
-144	Min.	-1.78	7	-25.14	19	-8.2	7	-0.1	13	-0.01	7	0	25
-143	Max	1.78	1	25.14	13	5.3	40	0.1	22	0.01	1	0	1
-143	Min.	-1.78	31	-25.14	43	-13.17	19	-0.1	37	-0.01	34	0	25
-142	Max	1.78	1	25.14	13	5.09	40	0.1	22	0.01	4	0	1
-142	Min.	-1.78	31	-25.14	43	-12.96	19	-0.1	37	-0.01	31	0	25
-141	Max	1.78	1	25.14	13	4.88	40	0.1	22	0.01	4	0	1
-141	Min.	-1.78	31	-25.14	43	-12.75	19	-0.1	37	-0.01	31	0	25
-140	Max	1.78	1	25.14	13	4.66	40	0.1	22	0.01	1	0	1
-140	Min.	-1.78	31	-25.14	43	-12.53	19	-0.1	37	-0.01	34	0	25
-139	Max	1.78	1	25.14	13	4.45	40	0.1	22	0.01	4	0	1
-139	Min.	-1.78	31	-25.14	43	-12.32	19	-0.1	37	-0.01	31	0	25
-138	Max	1.78	1	25.14	13	4.24	40	0.1	22	0.01	4	0	1
-138	Min.	-1.78	31	-25.14	43	-12.11	19	-0.1	37	-0.01	31	0	25
-137	Max	1.78	1	25.14	13	4.02	13	0.1	19	0.01	1	0	1
-137	Min.	-1.78	31	-25.14	19	-11.89	19	-0.1	13	-0.01	31	0	25
-136	Max	1.78	1	25.14	37	4.24	13	0.1	43	0.01	1	0	1
-136	Min.	-1.78	31	-25.14	19	-12.11	46	-0.1	16	-0.01	34	0	25
-135	Max	1.78	1	25.14	37	4.45	13	0.1	43	0.01	1	0	1
-135	Min.	-1.78	31	-25.14	19	-12.32	46	-0.1	16	-0.01	34	0	25
-134	Max	1.78	1	25.14	37	4.66	13	0.1	43	0.01	4	0	1
-134	Min.	-1.78	31	-25.14	19	-12.53	46	-0.1	16	-0.01	31	0	25
-133	Max	1.78	1	25.14	37	4.88	13	0.1	43	0.01	1	0	1
-133	Min.	-1.78	31	-25.14	19	-12.75	46	-0.1	16	-0.01	34	0	25
-132	Max	1.78	1	25.14	37	5.09	13	0.1	43	0.01	1	0	1
-132	Min.	-1.78	31	-25.14	19	-12.96	46	-0.1	16	-0.01	34	0	25
-131	Max	1.78	1	25.14	37	5.3	13	0.1	43	0.01	4	0	1
-131	Min.	-1.78	31	-25.14	19	-13.17	46	-0.1	16	-0.01	31	0	25
-130	Max	1.78	1	25.14	13	13.29	40	0.1	22	0.01	1	0	1
-130	Min.	-1.78	31	-25.14	43	-21.14	19	-0.1	37	-0.01	34	0	25
-129	Max	1.78	1	25.14	13	13.07	40	0.1	22	0.01	4	0	1
-129	Min.	-1.78	31	-25.14	43	-20.92	19	-0.1	37	-0.01	31	0	25
-128	Max	1.78	1	25.14	13	12.86	40	0.1	22	0.01	4	0	1
-128	Min.	-1.78	31	-25.14	43	-20.71	19	-0.1	37	-0.01	31	0	25
-127	Max	1.78	1	25.14	13	12.65	40	0.1	22	0.01	1	0	1
-127	Min.	-1.78	31	-25.14	43	-20.5	19	-0.1	37	-0.01	34	0	25
-126	Max	1.78	1	25.14	13	12.43	40	0.1	22	0.01	4	0	1
-126	Min.	-1.78	31	-25.14	43	-20.28	19	-0.1	37	-0.01	31	0	25
-125	Max	1.78	1	25.14	13	12.22	40	0.1	22	0.01	1	0	1
-125	Min.	-1.78	31	-25.14	43	-20.07	19	-0.1	37	-0.01	34	0	25
-124	Max	1.78	1	25.14	13	12.01	13	0.1	19	0.01	1	0	1
-124	Min.	-1.78	31	-25.14	19	-19.86	19	-0.1	13	-0.01	31	0	25
-123	Max	1.78	1	25.14	37	12.22	13	0.1	43	0.01	4	0	1
-123	Min.	-1.78	31	-25.14	19	-20.07	46	-0.1	16	-0.01	31	0	25

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-122	Max	1.78	1	25.14	37	12.43	13	0.1	43	0.01	1	0	1
-122	Min.	-1.78	31	-25.14	19	-20.28	46	-0.1	16	-0.01	34	0	25
-121	Max	1.78	1	25.14	37	12.65	13	0.1	43	0.01	4	0	1
-121	Min.	-1.78	31	-25.14	19	-20.5	46	-0.1	16	-0.01	31	0	25
-120	Max	1.78	1	25.14	37	12.86	13	0.1	43	0.01	1	0	1
-120	Min.	-1.78	31	-25.14	19	-20.71	46	-0.1	16	-0.01	34	0	25
-119	Max	1.78	1	25.14	37	13.07	13	0.1	43	0.01	1	0	1
-119	Min.	-1.78	31	-25.14	19	-20.92	46	-0.1	16	-0.01	34	0	25
-118	Max	1.78	1	25.14	37	13.29	13	0.1	43	0.01	4	0	1
-118	Min.	-1.78	31	-25.14	19	-21.14	46	-0.1	16	-0.01	31	0	25
-117	Max	1.19	25	16.79	13	13.29	22	0.1	43	0.01	28	0	13
-117	Min.	-1.19	10	-16.77	46	-21.14	37	-0.1	16	-0.01	7	0	46
-116	Max	1.19	25	16.79	13	13.07	22	0.1	43	0.01	28	0	19
-116	Min.	-1.19	10	-16.77	46	-20.92	37	-0.1	16	-0.01	7	0	40
-115	Max	1.19	25	16.79	13	12.86	22	0.1	43	0.01	28	0	1
-115	Min.	-1.19	10	-16.77	46	-20.71	37	-0.1	16	-0.01	7	0	34
-114	Max	1.19	25	16.78	13	12.65	22	0.1	43	0.01	28	0	4
-114	Min.	-1.19	10	-16.77	46	-20.5	37	-0.1	16	-0.01	7	0	31
-113	Max	1.19	25	16.78	13	12.43	22	0.1	43	0.01	28	0	1
-113	Min.	-1.19	10	-16.77	46	-20.28	37	-0.1	16	-0.01	7	0	34
-112	Max	1.19	25	16.78	13	12.22	22	0.1	43	0.01	28	0	4
-112	Min.	-1.19	10	-16.77	46	-20.07	37	-0.1	16	-0.01	7	0	31
-111	Max	1.19	25	16.78	13	12.01	19	0.1	19	0.01	25	0	1
-111	Min.	-1.19	7	-16.77	19	-19.86	13	-0.1	13	-0.01	7	0	31
-110	Max	1.19	28	16.78	40	12.22	43	0.1	22	0.01	25	0	1
-110	Min.	-1.19	7	-16.77	19	-20.07	16	-0.1	37	-0.01	10	0	34
-109	Max	1.19	28	16.78	40	12.43	43	0.1	22	0.01	25	0	4
-109	Min.	-1.19	7	-16.77	19	-20.28	16	-0.1	37	-0.01	10	0	31
-108	Max	1.19	28	16.78	40	12.65	43	0.1	22	0.01	25	0	1
-108	Min.	-1.19	7	-16.77	19	-20.5	16	-0.1	37	-0.01	10	0	34
-107	Max	1.19	28	16.79	40	12.86	43	0.1	22	0.01	25	0	4
-107	Min.	-1.19	7	-16.77	19	-20.71	16	-0.1	37	-0.01	10	0	31
-106	Max	1.19	28	16.79	40	13.07	43	0.1	22	0.01	25	0	13
-106	Min.	-1.19	7	-16.77	19	-20.92	16	-0.1	37	-0.01	10	0	46
-105	Max	1.19	28	16.79	40	13.29	43	0.1	22	0.01	25	0	19
-105	Min.	-1.19	7	-16.77	19	-21.14	16	-0.1	37	-0.01	10	0	40
-104	Max	1.19	4	16.77	16	13.29	40	0.1	46	0.01	1	0	16
-104	Min.	-1.19	31	-16.79	43	-21.14	19	-0.1	13	-0.01	34	0	43
-103	Max	1.19	4	16.77	16	13.07	40	0.1	46	0.01	1	0	22
-103	Min.	-1.19	31	-16.79	43	-20.92	19	-0.1	13	-0.01	34	0	37
-102	Max	1.19	4	16.77	16	12.86	40	0.1	46	0.01	1	0	7
-102	Min.	-1.19	31	-16.79	43	-20.71	19	-0.1	13	-0.01	34	0	28
-101	Max	1.19	4	16.77	16	12.65	40	0.1	46	0.01	1	0	10
-101	Min.	-1.19	31	-16.78	43	-20.5	19	-0.1	13	-0.01	34	0	25
-100	Max	1.19	4	16.77	16	12.43	40	0.1	46	0.01	1	0	7
-100	Min.	-1.19	31	-16.78	43	-20.28	19	-0.1	13	-0.01	34	0	28
-99	Max	1.19	4	16.77	16	12.22	40	0.1	46	0.01	1	0	10
-99	Min.	-1.19	31	-16.78	43	-20.07	19	-0.1	13	-0.01	34	0	25
-98	Max	1.19	1	16.77	13	12.01	13	0.1	19	0.01	1	0	7
-98	Min.	-1.19	31	-16.78	19	-19.86	19	-0.1	13	-0.01	31	0	25
-97	Max	1.19	1	16.77	37	12.22	13	0.1	19	0.01	4	0	7
-97	Min.	-1.19	34	-16.78	22	-20.07	46	-0.1	40	-0.01	31	0	28
-96	Max	1.19	1	16.77	37	12.43	13	0.1	19	0.01	4	0	10
-96	Min.	-1.19	34	-16.78	22	-20.28	46	-0.1	40	-0.01	31	0	25
-95	Max	1.19	1	16.77	37	12.65	13	0.1	19	0.01	4	0	7
-95	Min.	-1.19	34	-16.78	22	-20.5	46	-0.1	40	-0.01	31	0	28
-94	Max	1.19	1	16.77	37	12.86	13	0.1	19	0.01	4	0	10
-94	Min.	-1.19	34	-16.79	22	-20.71	46	-0.1	40	-0.01	31	0	25
-93	Max	1.19	1	16.77	37	13.07	13	0.1	19	0.01	4	0	16
-93	Min.	-1.19	34	-16.79	22	-20.92	46	-0.1	40	-0.01	31	0	43
-92	Max	1.19	1	16.77	37	13.29	13	0.1	19	0.01	4	0	22
-92	Min.	-1.19	34	-16.79	22	-21.14	46	-0.1	40	-0.01	31	0	37
-91	Max	0.59	25	8.38	13	13.29	22	0.1	46	0.01	25	0	19
-91	Min.	-0.59	10	-8.36	46	-21.13	37	-0.1	13	-0.01	10	0	40
-90	Max	0.59	25	8.38	13	13.07	22	0.1	46	0.01	28	0	13
-90	Min.	-0.59	10	-8.36	46	-20.92	37	-0.1	13	-0.01	7	0	46
-89	Max	0.59	25	8.38	13	12.86	22	0.1	46	0.01	28	0	4
-89	Min.	-0.59	10	-8.36	46	-20.71	37	-0.1	13	-0.01	7	0	31
-88	Max	0.59	25	8.38	13	12.65	22	0.1	46	0.01	28	0	1
-88	Min.	-0.59	10	-8.36	46	-20.49	37	-0.1	13	-0.01	7	0	34
-87	Max	0.59	25	8.37	13	12.43	22	0.1	46	0.01	28	0	4
-87	Min.	-0.59	10	-8.36	46	-20.28	37	-0.1	13	-0.01	7	0	31
-86	Max	0.59	25	8.37	13	12.22	22	0.1	46	0.01	28	0	1
-86	Min.	-0.59	10	-8.36	46	-20.07	37	-0.1	13	-0.01	7	0	34
-85	Max	0.59	25	8.37	13	12.01	19	0.1	19	0.01	25	0	1
-85	Min.	-0.59	7	-8.36	19	-19.85	13	-0.1	13	-0.01	7	0	31
-84	Max	0.59	28	8.37	40	12.22	43	0.1	19	0.01	25	0	4
-84	Min.	-0.59	7	-8.36	19	-20.07	16	-0.1	40	-0.01	10	0	31
-83	Max	0.59	28	8.37	40	12.43	43	0.1	19	0.01	25	0	1
-83	Min.	-0.59	7	-8.36	19	-20.28	16	-0.1	40	-0.01	10	0	34
-82	Max	0.59	28	8.38	40	12.65	43	0.1	19	0.01	25	0	4

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-82	Min.	-0.59	7	-8.36	19	-20.49	16	-0.1	40	-0.01	10	0	31
-81	Max	0.59	28	8.38	40	12.86	43	0.1	19	0.01	25	0	1
-81	Min.	-0.59	7	-8.36	19	-20.71	16	-0.1	40	-0.01	10	0	34
-80	Max	0.59	28	8.38	40	13.07	43	0.1	19	0.01	25	0	19
-80	Min.	-0.59	7	-8.36	19	-20.92	16	-0.1	40	-0.01	10	0	40
-79	Max	0.59	28	8.38	40	13.29	43	0.1	19	0.01	28	0	13
-79	Min.	-0.59	7	-8.36	19	-21.13	16	-0.1	40	-0.01	7	0	46
-78	Max	0.59	4	8.36	16	13.29	40	0.1	43	0.01	4	0	22
-78	Min.	-0.59	31	-8.38	43	-21.13	19	-0.1	16	-0.01	31	0	37
-77	Max	0.59	4	8.36	16	13.07	40	0.1	43	0.01	1	0	16
-77	Min.	-0.59	31	-8.38	43	-20.92	19	-0.1	16	-0.01	34	0	43
-76	Max	0.59	4	8.36	16	12.86	40	0.1	43	0.01	1	0	10
-76	Min.	-0.59	31	-8.38	43	-20.71	19	-0.1	16	-0.01	34	0	25
-75	Max	0.59	4	8.36	16	12.65	40	0.1	43	0.01	1	0	7
-75	Min.	-0.59	31	-8.38	43	-20.49	19	-0.1	16	-0.01	34	0	28
-74	Max	0.59	4	8.36	16	12.43	40	0.1	43	0.01	1	0	10
-74	Min.	-0.59	31	-8.37	43	-20.28	19	-0.1	16	-0.01	34	0	25
-73	Max	0.59	4	8.36	16	12.22	40	0.1	43	0.01	1	0	7
-73	Min.	-0.59	31	-8.37	43	-20.07	19	-0.1	16	-0.01	34	0	28
-72	Max	0.59	1	8.36	13	12.01	13	0.1	19	0.01	1	0	7
-72	Min.	-0.59	31	-8.37	19	-19.85	19	-0.1	13	-0.01	31	0	25
-71	Max	0.59	1	8.36	37	12.22	13	0.1	22	0.01	4	0	10
-71	Min.	-0.59	34	-8.37	22	-20.07	46	-0.1	37	-0.01	31	0	25
-70	Max	0.59	1	8.36	37	12.43	13	0.1	22	0.01	4	0	7
-70	Min.	-0.59	34	-8.37	22	-20.28	46	-0.1	37	-0.01	31	0	28
-69	Max	0.59	1	8.36	37	12.65	13	0.1	22	0.01	4	0	10
-69	Min.	-0.59	34	-8.38	22	-20.49	46	-0.1	37	-0.01	31	0	25
-68	Max	0.59	1	8.36	37	12.86	13	0.1	22	0.01	4	0	7
-68	Min.	-0.59	34	-8.38	22	-20.71	46	-0.1	37	-0.01	31	0	28
-67	Max	0.59	1	8.36	37	13.07	13	0.1	22	0.01	4	0	22
-67	Min.	-0.59	34	-8.38	22	-20.92	46	-0.1	37	-0.01	31	0	37
-66	Max	0.59	1	8.36	37	13.29	13	0.1	22	0.01	1	0	16
-66	Min.	-0.59	34	-8.38	22	-21.13	46	-0.1	37	-0.01	34	0	43
-65	Max	0	1	0	1	13.29	22	0.1	22	0.01	28	0	1
-65	Min.	0	1	0	1	-21.13	37	-0.1	37	-0.01	7	0	1
-64	Max	0	1	0	1	13.07	22	0.1	22	0.01	25	0	1
-64	Min.	0	1	0	1	-20.92	37	-0.1	37	-0.01	10	0	1
-63	Max	0	1	0	1	12.86	22	0.1	22	0.01	28	0	1
-63	Min.	0	1	0	1	-20.71	37	-0.1	37	-0.01	7	0	1
-62	Max	0	1	0	1	12.65	22	0.1	22	0.01	28	0	1
-62	Min.	0	1	0	1	-20.49	37	-0.1	37	-0.01	7	0	1
-61	Max	0	1	0	1	12.43	22	0.1	22	0.01	28	0	1
-61	Min.	0	1	0	1	-20.28	37	-0.1	37	-0.01	7	0	1
-60	Max	0	1	0	1	12.22	22	0.1	22	0.01	28	0	1
-60	Min.	0	1	0	1	-20.07	37	-0.1	37	-0.01	7	0	1
-59	Max	0	1	0	1	12.01	19	0.1	19	0.01	25	0	1
-59	Min.	0	1	0	1	-19.85	13	-0.1	13	-0.01	7	0	1
-58	Max	0	1	0	1	12.22	43	0.1	43	0.01	25	0	1
-58	Min.	0	1	0	1	-20.07	16	-0.1	16	-0.01	10	0	1
-57	Max	0	1	0	1	12.43	43	0.1	43	0.01	25	0	1
-57	Min.	0	1	0	1	-20.28	16	-0.1	16	-0.01	10	0	1
-56	Max	0	1	0	1	12.65	43	0.1	43	0.01	25	0	1
-56	Min.	0	1	0	1	-20.49	16	-0.1	16	-0.01	10	0	1
-55	Max	0	1	0	1	12.86	43	0.1	43	0.01	25	0	1
-55	Min.	0	1	0	1	-20.71	16	-0.1	16	-0.01	10	0	1
-54	Max	0	1	0	1	13.07	43	0.1	43	0.01	28	0	1
-54	Min.	0	1	0	1	-20.92	16	-0.1	16	-0.01	7	0	1
-53	Max	0	1	0	1	13.29	43	0.1	43	0.01	25	0	1
-53	Min.	0	1	0	1	-21.13	16	-0.1	16	-0.01	10	0	1
-52	Max	0	1	0	1	5.32	22	0.1	22	0.01	28	0	1
-52	Min.	0	1	0	1	-13.14	37	-0.1	37	-0.01	7	0	1
-51	Max	0	1	0	1	5.1	22	0.1	22	0.01	25	0	1
-51	Min.	0	1	0	1	-12.93	37	-0.1	37	-0.01	10	0	1
-50	Max	0	1	0	1	4.89	22	0.1	22	0.01	25	0	1
-50	Min.	0	1	0	1	-12.71	37	-0.1	37	-0.01	10	0	1
-49	Max	0	1	0	1	4.68	22	0.1	22	0.01	28	0	1
-49	Min.	0	1	0	1	-12.5	37	-0.1	37	-0.01	7	0	1
-48	Max	0	1	0	1	4.47	22	0.1	22	0.01	28	0	1
-48	Min.	0	1	0	1	-12.29	37	-0.1	37	-0.01	7	0	1
-47	Max	0	1	0	1	4.26	22	0.1	22	0.01	28	0	1
-47	Min.	0	1	0	1	-12.08	37	-0.1	37	-0.01	7	0	1
-46	Max	0	1	0	1	4.04	19	0.1	19	0.01	25	0	1
-46	Min.	0	1	0	1	-11.87	13	-0.1	13	-0.01	7	0	1
-45	Max	0	1	0	1	4.26	43	0.1	43	0.01	25	0	1
-45	Min.	0	1	0	1	-12.08	16	-0.1	16	-0.01	10	0	1
-44	Max	0	1	0	1	4.47	43	0.1	43	0.01	25	0	1
-44	Min.	0	1	0	1	-12.29	16	-0.1	16	-0.01	10	0	1
-43	Max	0	1	0	1	4.68	43	0.1	43	0.01	25	0	1
-43	Min.	0	1	0	1	-12.5	16	-0.1	16	-0.01	10	0	1
-42	Max	0	1	0	1	4.89	43	0.1	43	0.01	28	0	1
-42	Min.	0	1	0	1	-12.71	16	-0.1	16	-0.01	7	0	1

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-41Max	0	1	0	1	5.1	43	0.1	43	0.01	28	0	1
-41Min.	0	1	0	1	-12.93	16	-0.1	16	-0.01	7	0	1
-40Max	0	1	0	1	5.32	43	0.1	43	0.01	25	0	1
-40Min.	0	1	0	1	-13.14	16	-0.1	16	-0.01	10	0	1
-39Max	0	1	0	1	0.33	7	0.1	19	0.01	1	0	1
-39Min.	0	1	0	1	-8.14	1	-0.1	37	-0.01	7	0	1
-38Max	0	1	0	1	-0.38	7	0.1	19	0.01	1	0	1
-38Min.	0	1	0	1	-7.43	1	-0.1	37	-0.01	7	0	1
-37Max	0	1	0	1	-1.09	7	0.1	19	0.01	1	0	1
-37Min.	0	1	0	1	-6.91	49	-0.1	37	-0.01	7	0	1
-36Max	0	1	0	1	-1.79	7	0.1	19	0.01	1	0	1
-36Min.	0	1	0	1	-6.91	49	-0.1	37	-0.01	7	0	1
-35Max	0	1	0	1	-2.5	7	0.1	19	0.01	1	0	1
-35Min.	0	1	0	1	-6.9	49	-0.1	37	-0.01	7	0	1
-34Max	0	1	0	1	-3.2	7	0.1	19	0.01	1	0	1
-34Min.	0	1	0	1	-6.89	49	-0.1	37	-0.01	7	0	1
-33Max	0	1	0	1	-3.91	1	0.1	19	0.01	1	0	1
-33Min.	0	1	0	1	-6.89	49	-0.1	13	-0.01	7	0	1
-32Max	0	1	0	1	-3.2	1	0.1	43	0.01	1	0	1
-32Min.	0	1	0	1	-6.89	50	-0.1	13	-0.01	7	0	1
-31Max	0	1	0	1	-2.5	1	0.1	43	0.01	1	0	1
-31Min.	0	1	0	1	-6.9	50	-0.1	13	-0.01	7	0	1
-30Max	0	1	0	1	-1.79	1	0.1	43	0.01	1	0	1
-30Min.	0	1	0	1	-6.91	50	-0.1	13	-0.01	7	0	1
-29Max	0	1	0	1	-1.09	1	0.1	43	0.01	1	0	1
-29Min.	0	1	0	1	-6.91	50	-0.1	13	-0.01	7	0	1
-28Max	0	1	0	1	-0.38	1	0.1	43	0.01	1	0	1
-28Min.	0	1	0	1	-7.43	7	-0.1	13	-0.01	7	0	1
-27Max	0	1	0	1	0.33	1	0.1	43	0.01	1	0	1
-27Min.	0	1	0	1	-8.14	7	-0.1	13	-0.01	7	0	1
-26Max	0	1	0	1	5.32	40	0.1	19	0.01	1	0	1
-26Min.	0	1	0	1	-13.14	19	-0.1	40	-0.01	34	0	1
-25Max	0	1	0	1	5.1	40	0.1	19	0.01	4	0	1
-25Min.	0	1	0	1	-12.93	19	-0.1	40	-0.01	31	0	1
-24Max	0	1	0	1	4.89	40	0.1	19	0.01	4	0	1
-24Min.	0	1	0	1	-12.71	19	-0.1	40	-0.01	31	0	1
-23Max	0	1	0	1	4.68	40	0.1	19	0.01	1	0	1
-23Min.	0	1	0	1	-12.5	19	-0.1	40	-0.01	34	0	1
-22Max	0	1	0	1	4.47	40	0.1	19	0.01	1	0	1
-22Min.	0	1	0	1	-12.29	19	-0.1	40	-0.01	34	0	1
-21Max	0	1	0	1	4.26	40	0.1	19	0.01	1	0	1
-21Min.	0	1	0	1	-12.08	19	-0.1	40	-0.01	34	0	1
-20Max	0	1	0	1	4.04	13	0.1	19	0.01	1	0	1
-20Min.	0	1	0	1	-11.87	19	-0.1	13	-0.01	31	0	1
-19Max	0	1	0	1	4.26	13	0.1	46	0.01	4	0	1
-19Min.	0	1	0	1	-12.08	46	-0.1	13	-0.01	31	0	1
-18Max	0	1	0	1	4.47	13	0.1	46	0.01	4	0	1
-18Min.	0	1	0	1	-12.29	46	-0.1	13	-0.01	31	0	1
-17Max	0	1	0	1	4.68	13	0.1	46	0.01	4	0	1
-17Min.	0	1	0	1	-12.5	46	-0.1	13	-0.01	31	0	1
-16Max	0	1	0	1	4.89	13	0.1	46	0.01	1	0	1
-16Min.	0	1	0	1	-12.71	46	-0.1	13	-0.01	34	0	1
-15Max	0	1	0	1	5.1	13	0.1	46	0.01	1	0	1
-15Min.	0	1	0	1	-12.93	46	-0.1	13	-0.01	34	0	1
-14Max	0	1	0	1	5.32	13	0.1	46	0.01	4	0	1
-14Min.	0	1	0	1	-13.14	46	-0.1	13	-0.01	31	0	1
-13Max	0	1	0	1	13.29	40	0.1	19	0.01	1	0	1
-13Min.	0	1	0	1	-21.13	19	-0.1	40	-0.01	34	0	1
-12Max	0	1	0	1	13.07	40	0.1	19	0.01	4	0	1
-12Min.	0	1	0	1	-20.92	19	-0.1	40	-0.01	31	0	1
-11Max	0	1	0	1	12.86	40	0.1	19	0.01	1	0	1
-11Min.	0	1	0	1	-20.71	19	-0.1	40	-0.01	34	0	1
-10Max	0	1	0	1	12.65	40	0.1	19	0.01	1	0	1
-10Min.	0	1	0	1	-20.49	19	-0.1	40	-0.01	34	0	1
-9Max	0	1	0	1	12.43	40	0.1	19	0.01	1	0	1
-9Min.	0	1	0	1	-20.28	19	-0.1	40	-0.01	34	0	1
-8Max	0	1	0	1	12.22	40	0.1	19	0.01	1	0	1
-8Min.	0	1	0	1	-20.07	19	-0.1	40	-0.01	34	0	1
-7Max	0	1	0	1	12.01	13	0.1	19	0.01	1	0	1
-7Min.	0	1	0	1	-19.85	19	-0.1	13	-0.01	31	0	1
-6Max	0	1	0	1	12.22	13	0.1	46	0.01	4	0	1
-6Min.	0	1	0	1	-20.07	46	-0.1	13	-0.01	31	0	1
-5Max	0	1	0	1	12.43	13	0.1	46	0.01	4	0	1
-5Min.	0	1	0	1	-20.28	46	-0.1	13	-0.01	31	0	1
-4Max	0	1	0	1	12.65	13	0.1	46	0.01	4	0	1
-4Min.	0	1	0	1	-20.49	46	-0.1	13	-0.01	31	0	1
-3Max	0	1	0	1	12.86	13	0.1	46	0.01	4	0	1
-3Min.	0	1	0	1	-20.71	46	-0.1	13	-0.01	31	0	1
-2Max	0	1	0	1	13.07	13	0.1	46	0.01	1	0	1
-2Min.	0	1	0	1	-20.92	46	-0.1	13	-0.01	34	0	1
-1Max	0	1	0	1	13.29	13	0.1	46	0.01	4	0	1

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-1	Min.	0	1	0	1	-21.13	46	-0.1	13	-0.01	31	0	1
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Min = -25.14

Max = 25.14

Reazioni vincolari

Simbologia

Nodo=Numero del nodo

Rx =Reazione vincolare (forza) in dir. X

CC =Numero della combinazione delle condizioni di carico elementari

Ry =Reazione vincolare (forza) in dir. Y

Rz =Reazione vincolare (forza) in dir. Z

Mx =Reazione vincolare (momento) intorno all'asse X

My =Reazione vincolare (momento) intorno all'asse Y

Mz =Reazione vincolare (momento) intorno all'asse Z

Nodo		Rx <daN>	CC	Ry <daN>	CC	Rz <daN>	CC	Mx <daNm>	CC	My <daNm>	CC	Mz <daNm>	CC
-65	Max	158.38	10	1824.76	43	0	4	0	40	0	51	31.47	16
-65	Min.	-1140.82	25	-895.93	16	0	31	0	19	0	31	-120.59	43
-64	Max	1150.11	10	3973.08	43	0	16	0	49	0	46	17.52	34
-64	Min.	-1844.94	25	-1851.19	16	0	43	0	19	0	51	-44.71	1
-63	Max	2304.43	10	3691.97	43	0	16	0	37	0	7	32.29	31
-63	Min.	-2516.85	25	-1668.32	16	0	43	0	22	0	55	-33.77	4
-62	Max	3174.41	10	3665.1	43	0	46	0	43	0	22	37.68	31
-62	Min.	-3242.06	25	-1638.99	16	0	13	0	16	0	51	-35.79	4
-61	Max	3770.53	10	3592.22	43	0	46	0	51	0	22	39.98	34
-61	Min.	-3806.82	25	-1560.38	16	0	13	0	56	0	51	-38.12	1
-60	Max	4129.89	10	3524.47	43	0	22	0	37	0	16	40.65	31
-60	Min.	-4145.17	25	-1493.87	16	0	52	0	22	0	43	-39.64	4
-59	Max	4253.83	7	3457.64	19	0	40	0	16	0	22	40.48	31
-59	Min.	-4253.83	25	-1427.6	13	0	19	0	43	0	37	-40.48	1
-58	Max	4145.17	7	3524.47	22	0	51	0	52	0	37	39.64	34
-58	Min.	-4129.89	28	-1493.87	37	0	43	0	46	0	22	-40.65	1
-57	Max	3806.82	7	3592.22	22	0	19	0	51	0	16	38.12	31
-57	Min.	-3770.53	28	-1560.38	37	0	40	0	40	0	43	-39.98	4
-56	Max	3242.06	7	3665.1	22	0	16	0	7	0	37	35.79	34
-56	Min.	-3174.41	28	-1638.99	37	0	43	0	28	0	51	-37.68	1
-55	Max	2516.85	7	3691.97	22	0	37	0	16	0	52	33.77	34
-55	Min.	-2304.43	28	-1668.32	37	0	22	0	43	0	63	-32.29	1
-54	Max	1844.94	7	3973.08	22	0	46	0	52	0	43	44.71	31
-54	Min.	-1150.11	28	-1851.19	37	0	13	0	19	0	16	-17.52	4
-53	Max	1140.82	7	1824.76	22	0	43	0	51	0	43	120.59	22
-53	Min.	-158.38	28	-895.93	37	0	16	0	16	0	16	-31.47	37
-52	Max	0	1	0	1	0	13	0	40	0	31	0	1
-52	Min.	0	1	0	1	0	46	0	19	0	4	0	1
-51	Max	0	1	0	1	0	40	0	22	0	51	0	1
-51	Min.	0	1	0	1	0	19	0	50	0	64	0	1
-50	Max	0	1	0	1	0	43	0	46	0	52	0	1
-50	Min.	0	1	0	1	0	51	0	51	0	43	0	1
-49	Max	0	1	0	1	0	37	0	16	0	43	0	1
-49	Min.	0	1	0	1	0	22	0	43	0	16	0	1
-48	Max	0	1	0	1	0	50	0	19	0	43	0	1
-48	Min.	0	1	0	1	0	43	0	52	0	50	0	1
-47	Max	0	1	0	1	0	16	0	22	0	37	0	1
-47	Min.	0	1	0	1	0	43	0	37	0	52	0	1
-46	Max	0	1	0	1	0	37	0	16	0	46	0	1
-46	Min.	0	1	0	1	0	52	0	43	0	13	0	1
-45	Max	0	1	0	1	0	37	0	22	0	22	0	1
-45	Min.	0	1	0	1	0	22	0	37	0	52	0	1
-44	Max	0	1	0	1	0	16	0	19	0	51	0	1
-44	Min.	0	1	0	1	0	43	0	40	0	13	0	1
-43	Max	0	1	0	1	0	13	0	19	0	37	0	1
-43	Min.	0	1	0	1	0	49	0	40	0	51	0	1
-42	Max	0	1	0	1	0	52	0	40	0	7	0	1
-42	Min.	0	1	0	1	0	25	0	19	0	51	0	1
-41	Max	0	1	0	1	0	46	0	19	0	16	0	1
-41	Min.	0	1	0	1	0	13	0	51	0	52	0	1
-40	Max	0	1	0	1	0	43	0	13	0	13	0	1
-40	Min.	0	1	0	1	0	16	0	51	0	46	0	1
-39	Max	0	1	0	1	0	7	0	52	0	52	0	1
-39	Min.	0	1	0	1	0	49	0	13	0	25	0	1
-38	Max	0	1	0	1	0	7	0	43	0	28	0	1
-38	Min.	0	1	0	1	0	49	0	16	0	7	0	1
-37	Max	0	1	0	1	0	16	0	28	0	16	0	1
-37	Min.	0	1	0	1	0	43	0	7	0	52	0	1
-36	Max	0	1	0	1	0	13	0	51	0	37	0	1
-36	Min.	0	1	0	1	0	49	0	4	0	22	0	1
-35	Max	0	1	0	1	0	22	0	40	0	37	0	1
-35	Min.	0	1	0	1	0	37	0	19	0	51	0	1

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-34	Max	0	1	0	1	0	19	0	43	0	22	0	1
-34	Min.	0	1	0	1	0	51	0	16	0	52	0	1
-33	Max	0	1	0	1	0	43	0	19	0	22	0	1
-33	Min.	0	1	0	1	0	51	0	40	0	37	0	1
-32	Max	0	1	0	1	0	13	0	43	0	40	0	1
-32	Min.	0	1	0	1	0	49	0	51	0	51	0	1
-31	Max	0	1	0	1	0	55	0	13	0	43	0	1
-31	Min.	0	1	0	1	0	52	0	46	0	51	0	1
-30	Max	0	1	0	1	0	43	0	37	0	40	0	1
-30	Min.	0	1	0	1	0	50	0	22	0	49	0	1
-29	Max	0	1	0	1	0	25	0	16	0	51	0	1
-29	Min.	0	1	0	1	0	50	0	43	0	28	0	1
-28	Max	0	1	0	1	0	46	0	16	0	31	0	1
-28	Min.	0	1	0	1	0	51	0	52	0	4	0	1
-27	Max	0	1	0	1	0	22	0	4	0	50	0	1
-27	Min.	0	1	0	1	0	37	0	31	0	43	0	1
-26	Max	0	1	0	1	0	51	0	22	0	19	0	1
-26	Min.	0	1	0	1	0	37	0	37	0	40	0	1
-25	Max	0	1	0	1	0	49	0	46	0	16	0	1
-25	Min.	0	1	0	1	0	19	0	49	0	43	0	1
-24	Max	0	1	0	1	0	52	0	22	0	34	0	1
-24	Min.	0	1	0	1	0	16	0	52	0	51	0	1
-23	Max	0	1	0	1	0	46	0	43	0	34	0	1
-23	Min.	0	1	0	1	0	13	0	16	0	1	0	1
-22	Max	0	1	0	1	0	22	0	46	0	19	0	1
-22	Min.	0	1	0	1	0	52	0	13	0	51	0	1
-21	Max	0	1	0	1	0	51	0	56	0	52	0	1
-21	Min.	0	1	0	1	0	46	0	51	0	1	0	1
-20	Max	0	1	0	1	0	52	0	52	0	40	0	1
-20	Min.	0	1	0	1	0	16	0	43	0	49	0	1
-19	Max	0	1	0	1	0	40	0	52	0	46	0	1
-19	Min.	0	1	0	1	0	19	0	19	0	51	0	1
-18	Max	0	1	0	1	0	51	0	22	0	43	0	1
-18	Min.	0	1	0	1	0	16	0	37	0	16	0	1
-17	Max	0	1	0	1	0	22	0	37	0	28	0	1
-17	Min.	0	1	0	1	0	37	0	51	0	51	0	1
-16	Max	0	1	0	1	0	50	0	40	0	7	0	1
-16	Min.	0	1	0	1	0	16	0	19	0	28	0	1
-15	Max	0	1	0	1	0	52	0	43	0	4	0	1
-15	Min.	0	1	0	1	0	40	0	16	0	49	0	1
-14	Max	0	1	0	1	0	52	0	46	0	46	0	1
-14	Min.	0	1	0	1	0	31	0	13	0	52	0	1
-13	Max	158.38	31	895.93	46	0	34	0	13	0	51	120.59	13
-13	Min.	-1140.82	4	-1824.76	13	0	1	0	46	0	31	-31.47	46
-12	Max	1150.11	31	1851.19	46	0	16	0	34	0	16	44.71	28
-12	Min.	-1844.94	4	-3973.08	13	0	43	0	1	0	43	-17.52	7
-11	Max	2304.43	31	1668.32	46	0	46	0	46	0	16	33.77	25
-11	Min.	-2516.85	4	-3691.97	13	0	49	0	13	0	43	-32.29	10
-10	Max	3174.41	31	1638.99	46	0	40	0	19	0	46	35.79	25
-10	Min.	-3242.06	4	-3665.1	13	0	19	0	40	0	13	-37.68	10
-9	Max	3770.53	31	1560.38	46	0	16	0	22	0	52	38.12	28
-9	Min.	-3806.82	4	-3592.22	13	0	43	0	37	0	46	-39.98	7
-8	Max	4129.89	31	1493.87	46	0	40	0	52	0	56	39.64	25
-8	Min.	-4145.17	4	-3524.47	13	0	19	0	43	0	34	-40.65	10
-7	Max	4253.83	31	1427.6	19	0	40	0	22	0	52	40.48	25
-7	Min.	-4253.83	1	-3457.64	13	0	52	0	56	0	37	-40.48	7
-6	Max	4145.17	34	1493.87	19	0	13	0	19	0	52	40.65	28
-6	Min.	-4129.89	1	-3524.47	40	0	46	0	40	0	16	-39.64	7
-5	Max	3806.82	34	1560.38	19	0	16	0	16	0	13	39.98	25
-5	Min.	-3770.53	1	-3592.22	40	0	43	0	52	0	46	-38.12	10
-4	Max	3242.06	34	1638.99	19	0	13	0	43	0	13	37.68	28
-4	Min.	-3174.41	1	-3665.1	40	0	46	0	16	0	46	-35.79	7
-3	Max	2516.85	34	1668.32	19	0	4	0	13	0	16	32.29	28
-3	Min.	-2304.43	1	-3691.97	40	0	52	0	52	0	43	-33.77	7
-2	Max	1844.94	34	1851.19	19	0	40	0	16	0	40	17.52	25
-2	Min.	-1150.11	1	-3973.08	40	0	52	0	52	0	19	-44.71	10
-1	Max	1140.82	34	895.93	19	0	13	0	46	0	19	31.47	19
-1	Min.	-158.38	1	-1824.76	40	0	46	0	52	0	40	-120.59	40

Tensioni sul terreno

Simbologia

Nodo = Numero del nodo

σ_t = Tensione sul terreno

CC = Numero della combinazione delle condizioni di carico elementari

Nodo		σ_t <daN/cm ² >	CC	Nodo		σ_t <daN/cm ² >	CC	Nodo		σ_t <daN/cm ² >	CC	Nodo		σ_t <daN/cm ² >	CC	Nodo		σ_t <daN/cm ² >	CC
-65	Max	1.52	37	-65	Min.	-0.02	22	-64	Max	1.51	37	-64	Min.	-0.01	22	-63	Max	1.5	37
-63	Min.	-0.01	22	-62	Max	1.49	37	-62	Min.	0	22	-61	Max	1.48	37	-61	Min.	0.01	22
-60	Max	1.47	37	-60	Min.	0.02	22	-59	Max	1.46	13	-59	Min.	0.03	19	-58	Max	1.47	16

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-58	Min.	0.02	43	-57	Max	1.48	16	-57	Min.	0.01	43	-56	Max	1.49	16	-56	Min.	0	43
-55	Max	1.5	16	-55	Min.	-0.01	43	-54	Max	1.51	16	-54	Min.	-0.01	43	-53	Max	1.52	16
-53	Min.	-0.02	43	-52	Max	1.33	51	-52	Min.	0.33	22	-51	Max	1.33	51	-51	Min.	0.34	22
-50	Max	1.33	51	-50	Min.	0.35	22	-49	Max	1.33	51	-49	Min.	0.36	22	-48	Max	1.33	51
-48	Min.	0.37	22	-47	Max	1.33	51	-47	Min.	0.38	22	-46	Max	1.33	51	-46	Min.	0.39	19
-45	Max	1.33	51	-45	Min.	0.38	43	-44	Max	1.33	51	-44	Min.	0.37	43	-43	Max	1.33	51
-43	Min.	0.36	43	-42	Max	1.33	51	-42	Min.	0.35	43	-41	Max	1.33	51	-41	Min.	0.34	43
-40	Max	1.33	51	-40	Min.	0.33	43	-39	Max	1.32	49	-39	Min.	0.56	7	-38	Max	1.32	49
-38	Min.	0.59	7	-37	Max	1.32	49	-37	Min.	0.62	7	-36	Max	1.32	49	-36	Min.	0.65	7
-35	Max	1.32	49	-35	Min.	0.68	7	-34	Max	1.32	49	-34	Min.	0.71	7	-33	Max	1.32	49
-33	Min.	0.75	1	-32	Max	1.32	50	-32	Min.	0.71	1	-31	Max	1.32	50	-31	Min.	0.68	1
-30	Max	1.32	50	-30	Min.	0.65	1	-29	Max	1.32	50	-29	Min.	0.62	1	-28	Max	1.32	50
-28	Min.	0.59	1	-27	Max	1.32	50	-27	Min.	0.56	1	-26	Max	1.33	52	-26	Min.	0.33	40
-25	Max	1.33	52	-25	Min.	0.34	40	-24	Max	1.33	52	-24	Min.	0.35	40	-23	Max	1.33	52
-23	Min.	0.36	40	-22	Max	1.33	52	-22	Min.	0.37	40	-21	Max	1.33	52	-21	Min.	0.38	40
-20	Max	1.33	52	-20	Min.	0.39	13	-19	Max	1.33	52	-19	Min.	0.38	13	-18	Max	1.33	52
-18	Min.	0.37	13	-17	Max	1.33	52	-17	Min.	0.36	13	-16	Max	1.33	52	-16	Min.	0.35	13
-15	Max	1.33	52	-15	Min.	0.34	13	-14	Max	1.33	52	-14	Min.	0.33	13	-13	Max	1.52	19
-13	Min.	-0.02	40	-12	Max	1.51	19	-12	Min.	-0.01	40	-11	Max	1.5	19	-11	Min.	-0.01	40
-10	Max	1.49	19	-10	Min.	0	40	-9	Max	1.48	19	-9	Min.	0.01	40	-8	Max	1.47	19
-8	Min.	0.02	40	-7	Max	1.46	19	-7	Min.	0.03	13	-6	Max	1.47	46	-6	Min.	0.02	13
-5	Max	1.48	46	-5	Min.	0.01	13	-4	Max	1.49	46	-4	Min.	0	13	-3	Max	1.5	46
-3	Min.	-0.01	13	-2	Max	1.51	46	-2	Min.	-0.01	13	-1	Max	1.52	46	-1	Min.	-0.02	13

Sollecitazioni elementi bidimensionali

Simbologia

Bid. = Numero del muro/elemento bidimensionale

Nodo = Numero del nodo

σ_{xx} = Tensione normale sulle facce perp. all'asse X

CC = Numero della combinazione delle condizioni di carico elementari

σ_{zz} = Tensione normale sulle facce perp. all'asse Z

τ_{xz} = Tensione in dir. Z sulle facce perp. all'asse X

Mxx = Momento che provoca variazione di tensione sulle facce perp. all'asse X

Mzz = Momento che provoca variazione di tensione sulle facce perp. all'asse Z

Mxz = Momento che provoca variazione di tensione tangenziale sulle facce perp. all'asse X

τ_{zy} = Tensione in dir. Y sulle facce perp. all'asse Z

τ_{xy} = Tensione in dir. Y sulle facce perp. all'asse X

Bid.		Nodo	σ_{xx} <daN/mq>	CC	σ_{zz} <daN/mq>	CC	τ_{xz} <daN/mq>	CC	Mxx <daNm/m>	CC	Mzz <daNm/m>	CC	Mxz <daNm/m>	CC	τ_{zy} <daN/mq>	CC	τ_{xy} <daN/mq>	CC
105	Max	-53	-889.12	28	-16778.2	28	2204.13	28	281.4	22	3334.5	22	54.82	34	7308.35	37	507.07	43
105	Max	-54	-889.12	28	-16778.2	28	2204.13	28	281.4	22	3334.5	22	54.82	34	7308.35	37	507.07	43
105	Max	-80	-889.12	28	-16778.2	28	2204.13	28	281.4	22	3334.5	22	54.82	34	7308.35	37	507.07	43
105	Max	-79	-889.12	28	-16778.2	28	2204.13	28	281.4	22	3334.5	22	54.82	34	7308.35	37	507.07	43
105	Min.	-53	-3071.41	50	-49465.5	50	-5044.45	7	-134.59	37	-1379.3	37	-4.39	1	-11536.8	22	-302.44	16
105	Min.	-54	-3071.41	50	-49465.5	50	-5044.45	7	-134.59	37	-1379.3	37	-4.39	1	-11536.8	22	-302.44	16
105	Min.	-80	-3071.41	50	-49465.5	50	-5044.45	7	-134.59	37	-1379.3	37	-4.39	1	-11536.8	22	-302.44	16
105	Min.	-79	-3071.41	50	-49465.5	50	-5044.45	7	-134.59	37	-1379.3	37	-4.39	1	-11536.8	22	-302.44	16
105	Max	-58	-2056.06	43	-20681.1	43	14180.9	28	300.65	22	3004.33	22	37.4	31	6052.06	37	183.45	28
105	Max	-59	-2056.06	43	-20681.1	43	14180.9	28	300.65	22	3004.33	22	37.4	31	6052.06	37	183.45	28
105	Max	-85	-2056.06	43	-20681.1	43	14180.9	28	300.65	22	3004.33	22	37.4	31	6052.06	37	183.45	28
105	Max	-84	-2056.06	43	-20681.1	43	14180.9	28	300.65	22	3004.33	22	37.4	31	6052.06	37	183.45	28
105	Min.	-58	-4826.48	51	-48529.6	51	-14199.8	7	-107.28	37	-1074.32	37	-37.79	4	-10458	22	-182.66	7
105	Min.	-59	-4826.48	51	-48529.6	51	-14199.8	7	-107.28	37	-1074.32	37	-37.79	4	-10458	22	-182.66	7
105	Min.	-85	-4826.48	51	-48529.6	51	-14199.8	7	-107.28	37	-1074.32	37	-37.79	4	-10458	22	-182.66	7
105	Min.	-84	-4826.48	51	-48529.6	51	-14199.8	7	-107.28	37	-1074.32	37	-37.79	4	-10458	22	-182.66	7
105	Max	-59	-2056.06	22	-20681.1	22	14199.8	25	300.65	43	3004.33	43	37.79	34	6052.06	16	182.66	25
105	Max	-60	-2056.06	22	-20681.1	22	14199.8	25	300.65	43	3004.33	43	37.79	34	6052.06	16	182.66	25
105	Max	-86	-2056.06	22	-20681.1	22	14199.8	25	300.65	43	3004.33	43	37.79	34	6052.06	16	182.66	25
105	Max	-85	-2056.06	22	-20681.1	22	14199.8	25	300.65	43	3004.33	43	37.79	34	6052.06	16	182.66	25
105	Min.	-59	-4826.48	51	-48529.6	51	-14180.9	10	-107.28	16	-1074.32	16	-37.4	1	-10458	43	-183.45	10
105	Min.	-60	-4826.48	51	-48529.6	51	-14180.9	10	-107.28	16	-1074.32	16	-37.4	1	-10458	43	-183.45	10
105	Min.	-86	-4826.48	51	-48529.6	51	-14180.9	10	-107.28	16	-1074.32	16	-37.4	1	-10458	43	-183.45	10
105	Min.	-85	-4826.48	51	-48529.6	51	-14180.9	10	-107.28	16	-1074.32	16	-37.4	1	-10458	43	-183.45	10
105	Max	-60	-1993.3	22	-20169.7	22	13447.1	25	306.93	43	3068.1	43	37.75	31	6264.57	16	179.7	28
105	Max	-61	-1993.3	22	-20169.7	22	13447.1	25	306.93	43	3068.1	43	37.75	31	6264.57	16	179.7	28
105	Max	-87	-1993.3	22	-20169.7	22	13447.1	25	306.93	43	3068.1	43	37.75	31	6264.57	16	179.7	28
105	Max	-86	-1993.3	22	-20169.7	22	13447.1	25	306.93	43	3068.1	43	37.75	31	6264.57	16	179.7	28
105	Min.	-60	-4798.61	51	-48534.3	51	-13380.9	10	-113.58	16	-1139.07	16	-36.43	4	-10670.8	43	-183.23	7
105	Min.	-61	-4798.61	51	-48534.3	51	-13380.9	10	-113.58	16	-1139.07	16	-36.43	4	-10670.8	43	-183.23	7
105	Min.	-87	-4798.61	51	-48534.3	51	-13380.9	10	-113.58	16	-1139.07	16	-36.43	4	-10670.8	43	-183.23	7
105	Min.	-86	-4798.61	51	-48534.3	51	-13380.9	10	-113.58	16	-1139.07	16	-36.43	4	-10670.8	43	-183.23	7
105	Max	-61	-1913.75	22	-19605.2	22	11934	25	314.15	43	3130.65	43	36.86	34	6524.52	16	178.13	28
105	Max	-62	-1913.75	22	-19605.2	22	11934	25	314.15	43	3130.65	43	36.86	34	6524.52	16	178.13	28
105	Max	-88	-1913.75	22	-19605.2	22	11934	25	314.15	43	3130.65	43	36.86	34	6524.52	16	178.13	28
105	Max	-87	-1913.75	22	-19605.2	22	11934	25	314.15	43	3130.65	43	36.86	34	6524.52	16	178.13	28
105	Min.	-61	-4729.07	51	-48463.7	51	-11796.2	10	-121.52	16	-1204.47	16	-35.1	1	-10944.7	43	-186.96	7
105	Min.	-62	-4729.07	51	-48463.7	51	-11796.2	10	-121.52	16	-1204.47	16	-35.1	1	-10944.7	43	-186.96	7
105	Min.	-88	-4729.07	51	-48463.7	51	-11796.2	10	-121.52	16	-1204.47	16	-35.1	1	-10944.7	43	-186.96	7

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105	Min.	-87	-4729.07	51	-48463.7	51	-11796.2	10	-121.52	16	-1204.47	16	-35.1	1	-10944.7	43	-186.96	7
105	Max	-62	-1861.84	22	-18957	22	9694.19	25	315.23	43	3193.21	43	34.38	31	6686.34	16	161.88	25
105	Max	-63	-1861.84	22	-18957	22	9694.19	25	315.23	43	3193.21	43	34.38	31	6686.34	16	161.88	25
105	Max	-89	-1861.84	22	-18957	22	9694.19	25	315.23	43	3193.21	43	34.38	31	6686.34	16	161.88	25
105	Max	-88	-1861.84	22	-18957	22	9694.19	25	315.23	43	3193.21	43	34.38	31	6686.34	16	161.88	25
105	Min.	-62	-4607.61	51	-48335.7	51	-9409.19	10	-124.11	16	-1272.06	16	-33	4	-11008.3	43	-170.16	10
105	Min.	-63	-4607.61	51	-48335.7	51	-9409.19	10	-124.11	16	-1272.06	16	-33	4	-11008.3	43	-170.16	10
105	Min.	-89	-4607.61	51	-48335.7	51	-9409.19	10	-124.11	16	-1272.06	16	-33	4	-11008.3	43	-170.16	10
105	Min.	-88	-4607.61	51	-48335.7	51	-9409.19	10	-124.11	16	-1272.06	16	-33	4	-11008.3	43	-170.16	10
105	Max	-63	-1554.47	10	-18739.8	22	7179.3	25	338.02	43	3263.15	43	28.63	34	6998.19	16	263.03	43
105	Max	-64	-1554.47	10	-18739.8	22	7179.3	25	338.02	43	3263.15	43	28.63	34	6998.19	16	263.03	43
105	Max	-90	-1554.47	10	-18739.8	22	7179.3	25	338.02	43	3263.15	43	28.63	34	6998.19	16	263.03	43
105	Max	-89	-1554.47	10	-18739.8	22	7179.3	25	338.02	43	3263.15	43	28.63	34	6998.19	16	263.03	43
105	Min.	-63	-4213.33	49	-47755.4	51	-6096.09	10	-146.41	16	-1334.04	16	-32.88	1	-11641.8	43	-246.82	16
105	Min.	-64	-4213.33	49	-47755.4	51	-6096.09	10	-146.41	16	-1334.04	16	-32.88	1	-11641.8	43	-246.82	16
105	Min.	-90	-4213.33	49	-47755.4	51	-6096.09	10	-146.41	16	-1334.04	16	-32.88	1	-11641.8	43	-246.82	16
105	Min.	-89	-4213.33	49	-47755.4	51	-6096.09	10	-146.41	16	-1334.04	16	-32.88	1	-11641.8	43	-246.82	16
105	Max	-64	-889.12	10	-16778.2	10	5044.45	25	281.4	43	3334.5	43	4.39	31	7308.35	16	302.44	37
105	Max	-65	-889.12	10	-16778.2	10	5044.45	25	281.4	43	3334.5	43	4.39	31	7308.35	16	302.44	37
105	Max	-91	-889.12	10	-16778.2	10	5044.45	25	281.4	43	3334.5	43	4.39	31	7308.35	16	302.44	37
105	Max	-90	-889.12	10	-16778.2	10	5044.45	25	281.4	43	3334.5	43	4.39	31	7308.35	16	302.44	37
105	Min.	-64	-3071.41	49	-49465.5	49	-2204.13	10	-134.59	16	-1379.3	16	-54.82	4	-11536.8	43	-507.07	22
105	Min.	-65	-3071.41	49	-49465.5	49	-2204.13	10	-134.59	16	-1379.3	16	-54.82	4	-11536.8	43	-507.07	22
105	Min.	-91	-3071.41	49	-49465.5	49	-2204.13	10	-134.59	16	-1379.3	16	-54.82	4	-11536.8	43	-507.07	22
105	Min.	-90	-3071.41	49	-49465.5	49	-2204.13	10	-134.59	16	-1379.3	16	-54.82	4	-11536.8	43	-507.07	22
105	Max	-79	-369.37	28	-17477.4	43	2922.79	28	42.18	50	1252.65	50	41.68	37	9228.08	37	299.39	50
105	Max	-80	-369.37	28	-17477.4	43	2922.79	28	42.18	50	1252.65	50	41.68	37	9228.08	37	299.39	50
105	Max	-106	-369.37	28	-17477.4	43	2922.79	28	42.18	50	1252.65	50	41.68	37	9228.08	37	299.39	50
105	Max	-105	-369.37	28	-17477.4	43	2922.79	28	42.18	50	1252.65	50	41.68	37	9228.08	37	299.39	50
105	Min.	-79	-912.39	50	-45554.1	51	-2918.18	7	13.24	28	531.4	28	-44.86	22	-9880.64	22	151.85	28
105	Min.	-80	-912.39	50	-45554.1	51	-2918.18	7	13.24	28	531.4	28	-44.86	22	-9880.64	22	151.85	28
105	Min.	-106	-912.39	50	-45554.1	51	-2918.18	7	13.24	28	531.4	28	-44.86	22	-9880.64	22	151.85	28
105	Min.	-105	-912.39	50	-45554.1	51	-2918.18	7	13.24	28	531.4	28	-44.86	22	-9880.64	22	151.85	28
105	Max	-80	-1421.84	43	-17802.9	43	6818.15	28	118.11	50	1222.93	50	37.55	28	8649.15	37	85.32	25
105	Max	-81	-1421.84	43	-17802.9	43	6818.15	28	118.11	50	1222.93	50	37.55	28	8649.15	37	85.32	25
105	Max	-107	-1421.84	43	-17802.9	43	6818.15	28	118.11	50	1222.93	50	37.55	28	8649.15	37	85.32	25
105	Max	-106	-1421.84	43	-17802.9	43	6818.15	28	118.11	50	1222.93	50	37.55	28	8649.15	37	85.32	25
105	Min.	-80	-3464.24	51	-46149.9	51	-6890.36	7	46.19	28	530.53	28	-37.15	7	-9252.61	22	-78.71	10
105	Min.	-81	-3464.24	51	-46149.9	51	-6890.36	7	46.19	28	530.53	28	-37.15	7	-9252.61	22	-78.71	10
105	Min.	-107	-3464.24	51	-46149.9	51	-6890.36	7	46.19	28	530.53	28	-37.15	7	-9252.61	22	-78.71	10
105	Min.	-106	-3464.24	51	-46149.9	51	-6890.36	7	46.19	28	530.53	28	-37.15	7	-9252.61	22	-78.71	10
105	Max	-81	-1652.89	43	-17797.8	43	9632.01	25	121.59	50	1224.05	50	37.25	25	8733.32	37	99.19	25
105	Max	-82	-1652.89	43	-17797.8	43	9632.01	25	121.59	50	1224.05	50	37.25	25	8733.32	37	99.19	25
105	Max	-108	-1652.89	43	-17797.8	43	9632.01	25	121.59	50	1224.05	50	37.25	25	8733.32	37	99.19	25
105	Max	-107	-1652.89	43	-17797.8	43	9632.01	25	121.59	50	1224.05	50	37.25	25	8733.32	37	99.19	25
105	Min.	-81	-4111.56	51	-45574	51	-9644.88	10	52.25	28	550.47	28	-37.45	10	-9367.28	22	-94.85	10
105	Min.	-82	-4111.56	51	-45574	51	-9644.88	10	52.25	28	550.47	28	-37.45	10	-9367.28	22	-94.85	10
105	Min.	-108	-4111.56	51	-45574	51	-9644.88	10	52.25	28	550.47	28	-37.45	10	-9367.28	22	-94.85	10
105	Min.	-107	-4111.56	51	-45574	51	-9644.88	10	52.25	28	550.47	28	-37.45	10	-9367.28	22	-94.85	10
105	Max	-82	-1734.99	43	-18184.1	43	11945.4	28	122.14	50	1223.48	50	36.34	28	8345.7	37	110.76	28
105	Max	-83	-1734.99	43	-18184.1	43	11945.4	28	122.14	50	1223.48	50	36.34	28	8345.7	37	110.76	28
105	Max	-109	-1734.99	43	-18184.1	43	11945.4	28	122.14	50	1223.48	50	36.34	28	8345.7	37	110.76	28
105	Max	-108	-1734.99	43	-18184.1	43	11945.4	28	122.14	50	1223.48	50	36.34	28	8345.7	37	110.76	28
105	Min.	-82	-4349.06	51	-45817.1	51	-11944.2	7	56.28	28	574.58	28	-36.12	7	-8963.47	22	-92.79	7
105	Min.	-83	-4349.06	51	-45817.1	51	-11944.2	7	56.28	28	574.58	28	-36.12	7	-8963.47	22	-92.79	7
105	Min.	-109	-4349.06	51	-45817.1	51	-11944.2	7	56.28	28	574.58	28	-36.12	7	-8963.47	22	-92.79	7
105	Min.	-108	-4349.06	51	-45817.1	51	-11944.2	7	56.28	28	574.58	28	-36.12	7	-8963.47	22	-92.79	7
105	Max	-83	-1801.7	43	-18471.2	43	13506.7	28	123.26	50	1223.94	50	36.64	25	8179.66	37	109.42	28
105	Max	-84	-1801.7	43	-18471.2	43	13506.7	28	123.26	50	1223.94	50	36.64	25	8179.66	37	109.42	28
105	Max	-110	-1801.7	43	-18471.2	43	13506.7	28	123.26	50	1223.94	50	36.64	25	8179.66	37	109.42	28
105	Max	-109	-1801.7	43	-18471.2	43	13506.7	28	123.26	50	1223.94	50	36.64	25	8179.66	37	109.42	28
105	Min.	-83	-4473.92	51	-45837.7	51	-13506.2	7	60.03	28	601.18	28	-36.61	10	-8806.49	22	-103.1	7
105	Min.	-84	-4473.92	51	-45837.7	51	-13506.2	7	60.03	28	601.18	28	-36.61	10	-8806.49	22	-103.1	7
105	Min.	-110	-4473.92	51	-45837.7	51	-13506.2	7	60.03	28	601.18	28	-36.61	10	-8806.49	22	-103.1	7
105	Min.	-109	-4473.92	51	-45837.7	51	-13506.2	7	60.03	28	601.18	28	-36.61	10	-8806.49	22	-103.1	7
105	Max	-84	-1849.08	43	-18733	43	14286.2	28	123.12	51	1224.71	51	36.56	28	7936.22	37	108.29	25
105	Max	-85	-1849.08	43	-18733	43	14286.2	28	123.12	51	1224.71	51	36.56	28	7936.22	37	108.29	25
105	Max	-111	-1849.08	43	-18733	43	14286.2	28	123.12	51	1224.71	51	36.56	28	7936.22	37	108.29	25
105	Max	-110	-1849.08	43	-18733	43	14286.2	28	123.12	51	1224.71	51	36.56	28	7936.22	37	108.29	25
105	Min.	-84	-4530.9	51	-45838.3	51	-14285.8	7	62.15	43	618.41	43	-36.54	7	-8561.32	22	-107.11	10
105	Min.	-85	-4530.9	51	-45838.3	51	-14285.8	7	62.15	43	618.41	43	-36.54	7	-8561.32	22	-107.11	10
105	Min.	-111	-4530.9	51	-45838.3	51	-14285.8	7	62.15	43	618.41	43	-36.54	7	-8561.32			

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105	Max	-86	-1801.7	22	-18471.2	22	13506.2	25	123.26	49	1223.94	49	36.61	28	8179.66	16	103.1	25
105	Max	-87	-1801.7	22	-18471.2	22	13506.2	25	123.26	49	1223.94	49	36.61	28	8179.66	16	103.1	25
105	Max	-113	-1801.7	22	-18471.2	22	13506.2	25	123.26	49	1223.94	49	36.61	28	8179.66	16	103.1	25
105	Max	-112	-1801.7	22	-18471.2	22	13506.2	25	123.26	49	1223.94	49	36.61	28	8179.66	16	103.1	25
105	Min.	-86	-4473.92	51	-45837.7	51	-13506.7	10	60.03	10	601.18	10	-36.64	7	-8806.49	43	-109.42	10
105	Min.	-87	-4473.92	51	-45837.7	51	-13506.7	10	60.03	10	601.18	10	-36.64	7	-8806.49	43	-109.42	10
105	Min.	-113	-4473.92	51	-45837.7	51	-13506.7	10	60.03	10	601.18	10	-36.64	7	-8806.49	43	-109.42	10
105	Min.	-112	-4473.92	51	-45837.7	51	-13506.7	10	60.03	10	601.18	10	-36.64	7	-8806.49	43	-109.42	10
105	Max	-87	-1734.99	22	-18184.1	22	11944.2	25	122.14	49	1223.48	49	36.12	25	8345.7	16	92.79	25
105	Max	-88	-1734.99	22	-18184.1	22	11944.2	25	122.14	49	1223.48	49	36.12	25	8345.7	16	92.79	25
105	Max	-114	-1734.99	22	-18184.1	22	11944.2	25	122.14	49	1223.48	49	36.12	25	8345.7	16	92.79	25
105	Max	-113	-1734.99	22	-18184.1	22	11944.2	25	122.14	49	1223.48	49	36.12	25	8345.7	16	92.79	25
105	Min.	-87	-4349.06	51	-45817.1	51	-11945.4	10	56.28	10	574.58	10	-36.34	10	-8963.47	43	-110.76	10
105	Min.	-88	-4349.06	51	-45817.1	51	-11945.4	10	56.28	10	574.58	10	-36.34	10	-8963.47	43	-110.76	10
105	Min.	-114	-4349.06	51	-45817.1	51	-11945.4	10	56.28	10	574.58	10	-36.34	10	-8963.47	43	-110.76	10
105	Min.	-113	-4349.06	51	-45817.1	51	-11945.4	10	56.28	10	574.58	10	-36.34	10	-8963.47	43	-110.76	10
105	Max	-88	-1652.89	22	-17797.8	22	9644.88	28	121.59	49	1224.05	49	37.45	28	8733.32	16	94.85	28
105	Max	-89	-1652.89	22	-17797.8	22	9644.88	28	121.59	49	1224.05	49	37.45	28	8733.32	16	94.85	28
105	Max	-115	-1652.89	22	-17797.8	22	9644.88	28	121.59	49	1224.05	49	37.45	28	8733.32	16	94.85	28
105	Max	-114	-1652.89	22	-17797.8	22	9644.88	28	121.59	49	1224.05	49	37.45	28	8733.32	16	94.85	28
105	Min.	-88	-4111.56	51	-45574.51	51	-9632.01	7	52.25	10	550.47	10	-37.25	7	-9367.28	43	-99.19	7
105	Min.	-89	-4111.56	51	-45574.51	51	-9632.01	7	52.25	10	550.47	10	-37.25	7	-9367.28	43	-99.19	7
105	Min.	-115	-4111.56	51	-45574.51	51	-9632.01	7	52.25	10	550.47	10	-37.25	7	-9367.28	43	-99.19	7
105	Min.	-114	-4111.56	51	-45574.51	51	-9632.01	7	52.25	10	550.47	10	-37.25	7	-9367.28	43	-99.19	7
105	Max	-89	-1421.84	22	-17802.9	22	6890.36	25	118.11	49	1222.93	49	37.15	25	8649.15	16	78.71	28
105	Max	-90	-1421.84	22	-17802.9	22	6890.36	25	118.11	49	1222.93	49	37.15	25	8649.15	16	78.71	28
105	Max	-116	-1421.84	22	-17802.9	22	6890.36	25	118.11	49	1222.93	49	37.15	25	8649.15	16	78.71	28
105	Max	-115	-1421.84	22	-17802.9	22	6890.36	25	118.11	49	1222.93	49	37.15	25	8649.15	16	78.71	28
105	Min.	-89	-3464.24	51	-46149.9	51	-6818.15	10	46.19	10	530.53	10	-37.55	10	-9252.61	43	-85.32	7
105	Min.	-90	-3464.24	51	-46149.9	51	-6818.15	10	46.19	10	530.53	10	-37.55	10	-9252.61	43	-85.32	7
105	Min.	-116	-3464.24	51	-46149.9	51	-6818.15	10	46.19	10	530.53	10	-37.55	10	-9252.61	43	-85.32	7
105	Min.	-115	-3464.24	51	-46149.9	51	-6818.15	10	46.19	10	530.53	10	-37.55	10	-9252.61	43	-85.32	7
105	Max	-90	-369.37	10	-17477.4	22	2918.18	25	42.18	49	1252.65	49	44.86	43	9228.08	16	-151.85	10
105	Max	-91	-369.37	10	-17477.4	22	2918.18	25	42.18	49	1252.65	49	44.86	43	9228.08	16	-151.85	10
105	Max	-117	-369.37	10	-17477.4	22	2918.18	25	42.18	49	1252.65	49	44.86	43	9228.08	16	-151.85	10
105	Max	-116	-369.37	10	-17477.4	22	2918.18	25	42.18	49	1252.65	49	44.86	43	9228.08	16	-151.85	10
105	Min.	-90	-912.39	49	-45554.1	51	-2922.79	10	13.24	10	531.4	10	-41.68	16	-9880.64	43	-299.39	49
105	Min.	-91	-912.39	49	-45554.1	51	-2922.79	10	13.24	10	531.4	10	-41.68	16	-9880.64	43	-299.39	49
105	Min.	-117	-912.39	49	-45554.1	51	-2922.79	10	13.24	10	531.4	10	-41.68	16	-9880.64	43	-299.39	49
105	Min.	-116	-912.39	49	-45554.1	51	-2922.79	10	13.24	10	531.4	10	-41.68	16	-9880.64	43	-299.39	49
105	Max	-105	-1192.8	22	-16219.1	19	4164.66	28	254.36	37	3032.92	37	-3.2	28	9939.11	37	472.3	16
105	Max	-106	-1192.8	22	-16219.1	19	4164.66	28	254.36	37	3032.92	37	-3.2	28	9939.11	37	472.3	16
105	Max	-171	-1192.8	22	-16219.1	19	4164.66	28	254.36	37	3032.92	37	-3.2	28	9939.11	37	472.3	16
105	Max	-170	-1192.8	22	-16219.1	19	4164.66	28	254.36	37	3032.92	37	-3.2	28	9939.11	37	472.3	16
105	Min.	-105	-2609.28	51	-43845.1	51	-1671.96	7	-156.14	22	-1634.24	22	-44.01	7	-8868.89	22	-352.14	43
105	Min.	-106	-2609.28	51	-43845.1	51	-1671.96	7	-156.14	22	-1634.24	22	-44.01	7	-8868.89	22	-352.14	43
105	Min.	-171	-2609.28	51	-43845.1	51	-1671.96	7	-156.14	22	-1634.24	22	-44.01	7	-8868.89	22	-352.14	43
105	Min.	-170	-2609.28	51	-43845.1	51	-1671.96	7	-156.14	22	-1634.24	22	-44.01	7	-8868.89	22	-352.14	43
105	Max	-106	-1340.24	19	-15237.3	19	7156.25	25	306.63	37	2975.92	37	20.6	25	10036.2	37	240.05	22
105	Max	-107	-1340.24	19	-15237.3	19	7156.25	25	306.63	37	2975.92	37	20.6	25	10036.2	37	240.05	22
105	Max	-172	-1340.24	19	-15237.3	19	7156.25	25	306.63	37	2975.92	37	20.6	25	10036.2	37	240.05	22
105	Max	-171	-1340.24	19	-15237.3	19	7156.25	25	306.63	37	2975.92	37	20.6	25	10036.2	37	240.05	22
105	Min.	-106	-3661.1	51	-42449.8	51	-6204.4	10	-172.05	22	-1594.74	22	-25.04	10	-8553.82	22	-217.23	37
105	Min.	-107	-3661.1	51	-42449.8	51	-6204.4	10	-172.05	22	-1594.74	22	-25.04	10	-8553.82	22	-217.23	37
105	Min.	-172	-3661.1	51	-42449.8	51	-6204.4	10	-172.05	22	-1594.74	22	-25.04	10	-8553.82	22	-217.23	37
105	Min.	-171	-3661.1	51	-42449.8	51	-6204.4	10	-172.05	22	-1594.74	22	-25.04	10	-8553.82	22	-217.23	37
105	Max	-107	-1518.59	19	-16124.9	19	9816	25	287.86	37	2920.82	37	25.75	28	9455.31	37	90.11	13
105	Max	-108	-1518.59	19	-16124.9	19	9816	25	287.86	37	2920.82	37	25.75	28	9455.31	37	90.11	13
105	Max	-173	-1518.59	19	-16124.9	19	9816	25	287.86	37	2920.82	37	25.75	28	9455.31	37	90.11	13
105	Max	-172	-1518.59	19	-16124.9	19	9816	25	287.86	37	2920.82	37	25.75	28	9455.31	37	90.11	13
105	Min.	-107	-4075.15	51	-42950.3	51	-9555.24	10	-150.47	22	-1546.4	22	-24.26	7	-8244.56	22	-94.05	46
105	Min.	-108	-4075.15	51	-42950.3	51	-9555.24	10	-150.47	22	-1546.4	22	-24.26	7	-8244.56	22	-94.05	46
105	Min.	-173	-4075.15	51	-42950.3	51	-9555.24	10	-150.47	22	-1546.4	22	-24.26	7	-8244.56	22	-94.05	46
105	Min.	-172	-4075.15	51	-42950.3	51	-9555.24	10	-150.47	22	-1546.4	22	-24.26	7	-8244.56	22	-94.05	46
105	Max	-108	-1594.43	19	-16292.1	19	12047.1	25	287.93	37	2872.48	37	27.65	25	9370.04	37	85.43	10
105	Max	-109	-1594.43	19	-16292.1	19	12047.1	25	287.93	37	2872.48	37	27.65	25	9370.04	37	85.43	10
105	Max	-174	-1594.43	19	-16292.1	19	12047.1	25	287.93	37	2872.48	37	27.65	25	9370.04	37	85.43	10
105	Max	-173	-1594.43	19	-16292.1	19	12047.1	25	287.93	37	2872.48	37	27.65	25	9370.04	37	85.43	10
105	Min.	-108	-4189.27	51	-43046.2	51	-11912.7	10	-150.37	22	-1494.13	22	-26.11	10	-8094.37	22	-76.29	25
105	Min.	-109	-4189.27	51	-43046.2	51	-11912.7	10	-150.37	22	-1494.13	22	-26.11	10	-8094.37	22	-76.29	25
105	Min.	-174	-4189.27	51	-43046.2	51	-11912.7	10	-150.37	22	-1494.13	22	-26.11	10	-8094.37	22	-76.29	25
105	Min.	-173	-4189.27	51	-43046.2	51	-11912.7	10										

Relazione geotecnica tombino

105	Max	-111	-1656.16	19	-16684.1	19	14334.4	25	277.92	37	2777.59	37	27.96	25	8887.42	37	75.57	7
105	Max	-176	-1656.16	19	-16684.1	19	14334.4	25	277.92	37	2777.59	37	27.96	25	8887.42	37	75.57	7
105	Max	-175	-1656.16	19	-16684.1	19	14334.4	25	277.92	37	2777.59	37	27.96	25	8887.42	37	75.57	7
105	Min.	-110	-4284.73	51	-43111.8	51	-14314.5	10	-139.46	22	-1396.48	22	-27.59	10	-7622.28	22	-75.17	28
105	Min.	-111	-4284.73	51	-43111.8	51	-14314.5	10	-139.46	22	-1396.48	22	-27.59	10	-7622.28	22	-75.17	28
105	Min.	-176	-4284.73	51	-43111.8	51	-14314.5	10	-139.46	22	-1396.48	22	-27.59	10	-7622.28	22	-75.17	28
105	Min.	-175	-4284.73	51	-43111.8	51	-14314.5	10	-139.46	22	-1396.48	22	-27.59	10	-7622.28	22	-75.17	28
105	Max	-111	-1656.16	46	-16684.1	46	14314.5	28	277.92	16	2777.59	16	27.59	28	8887.42	16	75.17	10
105	Max	-112	-1656.16	46	-16684.1	46	14314.5	28	277.92	16	2777.59	16	27.59	28	8887.42	16	75.17	10
105	Max	-177	-1656.16	46	-16684.1	46	14314.5	28	277.92	16	2777.59	16	27.59	28	8887.42	16	75.17	10
105	Max	-176	-1656.16	46	-16684.1	46	14314.5	28	277.92	16	2777.59	16	27.59	28	8887.42	16	75.17	10
105	Min.	-111	-4284.73	51	-43111.8	51	-14334.4	7	-139.46	43	-1396.48	43	-27.96	7	-7622.28	43	-75.57	25
105	Min.	-112	-4284.73	51	-43111.8	51	-14334.4	7	-139.46	43	-1396.48	43	-27.96	7	-7622.28	43	-75.57	25
105	Min.	-177	-4284.73	51	-43111.8	51	-14334.4	7	-139.46	43	-1396.48	43	-27.96	7	-7622.28	43	-75.57	25
105	Min.	-176	-4284.73	51	-43111.8	51	-14334.4	7	-139.46	43	-1396.48	43	-27.96	7	-7622.28	43	-75.57	25
105	Max	-112	-1628.03	46	-16506.2	46	13504.8	28	282.5	16	2825.26	16	26.75	25	9101.05	16	73.83	7
105	Max	-113	-1628.03	46	-16506.2	46	13504.8	28	282.5	16	2825.26	16	26.75	25	9101.05	16	73.83	7
105	Max	-178	-1628.03	46	-16506.2	46	13504.8	28	282.5	16	2825.26	16	26.75	25	9101.05	16	73.83	7
105	Max	-177	-1628.03	46	-16506.2	46	13504.8	28	282.5	16	2825.26	16	26.75	25	9101.05	16	73.83	7
105	Min.	-112	-4256.75	51	-43117.8	51	-13572.6	7	-143.98	43	-1444.84	43	-28.04	10	-7831.5	43	-76.63	28
105	Min.	-113	-4256.75	51	-43117.8	51	-13572.6	7	-143.98	43	-1444.84	43	-28.04	10	-7831.5	43	-76.63	28
105	Min.	-178	-4256.75	51	-43117.8	51	-13572.6	7	-143.98	43	-1444.84	43	-28.04	10	-7831.5	43	-76.63	28
105	Min.	-177	-4256.75	51	-43117.8	51	-13572.6	7	-143.98	43	-1444.84	43	-28.04	10	-7831.5	43	-76.63	28
105	Max	-113	-1594.43	46	-16292.1	46	11912.7	28	287.93	16	2872.48	16	26.11	28	9370.04	16	76.29	7
105	Max	-114	-1594.43	46	-16292.1	46	11912.7	28	287.93	16	2872.48	16	26.11	28	9370.04	16	76.29	7
105	Max	-179	-1594.43	46	-16292.1	46	11912.7	28	287.93	16	2872.48	16	26.11	28	9370.04	16	76.29	7
105	Max	-178	-1594.43	46	-16292.1	46	11912.7	28	287.93	16	2872.48	16	26.11	28	9370.04	16	76.29	7
105	Min.	-113	-4189.27	51	-43046.2	51	-12047.1	7	-150.37	43	-1494.13	43	-27.65	7	-8094.37	43	-85.43	28
105	Min.	-114	-4189.27	51	-43046.2	51	-12047.1	7	-150.37	43	-1494.13	43	-27.65	7	-8094.37	43	-85.43	28
105	Min.	-179	-4189.27	51	-43046.2	51	-12047.1	7	-150.37	43	-1494.13	43	-27.65	7	-8094.37	43	-85.43	28
105	Min.	-178	-4189.27	51	-43046.2	51	-12047.1	7	-150.37	43	-1494.13	43	-27.65	7	-8094.37	43	-85.43	28
105	Max	-114	-1518.59	46	-16124.9	46	9555.24	28	287.86	16	2920.82	16	24.26	25	9455.31	16	94.05	19
105	Max	-115	-1518.59	46	-16124.9	46	9555.24	28	287.86	16	2920.82	16	24.26	25	9455.31	16	94.05	19
105	Max	-180	-1518.59	46	-16124.9	46	9555.24	28	287.86	16	2920.82	16	24.26	25	9455.31	16	94.05	19
105	Max	-179	-1518.59	46	-16124.9	46	9555.24	28	287.86	16	2920.82	16	24.26	25	9455.31	16	94.05	19
105	Min.	-114	-4075.15	51	-42950.3	51	-9816	7	-150.47	43	-1546.4	43	-25.75	10	-8244.56	43	-90.11	40
105	Min.	-115	-4075.15	51	-42950.3	51	-9816	7	-150.47	43	-1546.4	43	-25.75	10	-8244.56	43	-90.11	40
105	Min.	-180	-4075.15	51	-42950.3	51	-9816	7	-150.47	43	-1546.4	43	-25.75	10	-8244.56	43	-90.11	40
105	Min.	-179	-4075.15	51	-42950.3	51	-9816	7	-150.47	43	-1546.4	43	-25.75	10	-8244.56	43	-90.11	40
105	Max	-115	-1340.24	46	-15237.3	46	6204.39	28	306.63	16	2975.92	16	25.04	28	10036.2	16	217.24	16
105	Max	-116	-1340.24	46	-15237.3	46	6204.39	28	306.63	16	2975.92	16	25.04	28	10036.2	16	217.24	16
105	Max	-181	-1340.24	46	-15237.3	46	6204.39	28	306.63	16	2975.92	16	25.04	28	10036.2	16	217.24	16
105	Max	-180	-1340.24	46	-15237.3	46	6204.39	28	306.63	16	2975.92	16	25.04	28	10036.2	16	217.24	16
105	Min.	-115	-3661.1	51	-42449.8	51	-7156.26	7	-172.05	43	-1594.74	43	-20.6	7	-8553.82	43	-240.05	43
105	Min.	-116	-3661.1	51	-42449.8	51	-7156.26	7	-172.05	43	-1594.74	43	-20.6	7	-8553.82	43	-240.05	43
105	Min.	-181	-3661.1	51	-42449.8	51	-7156.26	7	-172.05	43	-1594.74	43	-20.6	7	-8553.82	43	-240.05	43
105	Min.	-180	-3661.1	51	-42449.8	51	-7156.26	7	-172.05	43	-1594.74	43	-20.6	7	-8553.82	43	-240.05	43
105	Max	-116	-1192.8	43	-16219.1	46	1671.96	25	254.36	16	3032.92	16	44.01	25	9939.11	16	352.14	22
105	Max	-117	-1192.8	43	-16219.1	46	1671.96	25	254.36	16	3032.92	16	44.01	25	9939.11	16	352.14	22
105	Max	-182	-1192.8	43	-16219.1	46	1671.96	25	254.36	16	3032.92	16	44.01	25	9939.11	16	352.14	22
105	Max	-181	-1192.8	43	-16219.1	46	1671.96	25	254.36	16	3032.92	16	44.01	25	9939.11	16	352.14	22
105	Min.	-116	-2609.28	51	-43845.1	51	-4164.66	10	-156.14	43	-1634.24	43	3.2	10	-8868.89	43	-472.3	37
105	Min.	-117	-2609.28	51	-43845.1	51	-4164.66	10	-156.14	43	-1634.24	43	3.2	10	-8868.89	43	-472.3	37
105	Min.	-182	-2609.28	51	-43845.1	51	-4164.66	10	-156.14	43	-1634.24	43	3.2	10	-8868.89	43	-472.3	37
105	Min.	-181	-2609.28	51	-43845.1	51	-4164.66	10	-156.14	43	-1634.24	43	3.2	10	-8868.89	43	-472.3	37
105	Max	-57	-1993.3	43	-20169.7	43	13380.9	28	306.93	22	3068.1	22	36.43	34	6264.57	37	183.23	25
105	Max	-58	-1993.3	43	-20169.7	43	13380.9	28	306.93	22	3068.1	22	36.43	34	6264.57	37	183.23	25
105	Max	-84	-1993.3	43	-20169.7	43	13380.9	28	306.93	22	3068.1	22	36.43	34	6264.57	37	183.23	25
105	Max	-83	-1993.3	43	-20169.7	43	13380.9	28	306.93	22	3068.1	22	36.43	34	6264.57	37	183.23	25
105	Min.	-57	-4798.61	51	-48534.3	51	-13447.1	7	-113.58	37	-1139.07	37	-37.75	1	-10670.8	22	-179.7	10
105	Min.	-58	-4798.61	51	-48534.3	51	-13447.1	7	-113.58	37	-1139.07	37	-37.75	1	-10670.8	22	-179.7	10
105	Min.	-84	-4798.61	51	-48534.3	51	-13447.1	7	-113.58	37	-1139.07	37	-37.75	1	-10670.8	22	-179.7	10
105	Min.	-83	-4798.61	51	-48534.3	51	-13447.1	7	-113.58	37	-1139.07	37	-37.75	1	-10670.8	22	-179.7	10
105	Max	-55	-1861.84	43	-18957	43	9409.19	28	315.23	22	3193.21	22	33	34	6686.34	37	170.16	28
105	Max	-56	-1861.84	43	-18957	43	9409.19	28	315.23	22	3193.21	22	33	34	6686.34	37	170.16	28
105	Max	-82	-1861.84	43	-18957	43	9409.19	28	315.23	22	3193.21	22	33	34	6686.34	37	170.16	28
105	Max	-81	-1861.84	43	-18957	43	9409.19	28	315.23	22	3193.21	22	33	34	6686.34	37	170.16	28
105	Min.	-55	-4607.61	51	-48335.7	51	-9694.19	7	-124.11	37	-1272.06	37	-34.38	1	-11008.3	22	-161.88	7
105	Min.	-56	-4607.61	51	-48335.7	51	-9694.19	7	-124.11	37	-1272.06	37	-34.38	1	-11008.3	22	-161.88	7
105	Min.	-82	-4607.61	51	-48335.7	51	-9694.19	7	-124.11	37	-1272.06	37	-34.38	1	-11008.3	22	-161.88	7
105	Min.	-81	-4607.61	51	-48335.7	51	-9694.19	7	-124.11	37	-1272.06	37	-34.38	1	-11008.3	22	-161.88	7
105	Max	-54	-1554.47	28	-18739.8	43	6096.09	28	338									

Relazione geotecnica tombino

105	Max	-83	-1913.75	43	-19605.2	43	11796.2	28	314.15	22	3130.65	22	35.1	31	6524.52	37	186.96	25
105	Max	-82	-1913.75	43	-19605.2	43	11796.2	28	314.15	22	3130.65	22	35.1	31	6524.52	37	186.96	25
105	Min.	-56	-4729.07	51	-48463.7	51	-11934	7	-121.52	37	-1204.47	37	-36.86	4	-10944.7	22	-178.13	10
105	Min.	-57	-4729.07	51	-48463.7	51	-11934	7	-121.52	37	-1204.47	37	-36.86	4	-10944.7	22	-178.13	10
105	Min.	-83	-4729.07	51	-48463.7	51	-11934	7	-121.52	37	-1204.47	37	-36.86	4	-10944.7	22	-178.13	10
105	Min.	-82	-4729.07	51	-48463.7	51	-11934	7	-121.52	37	-1204.47	37	-36.86	4	-10944.7	22	-178.13	10
106	Max	-98	-1656.16	37	-16684.1	37	14314.5	31	277.92	19	2777.59	19	27.59	31	8887.42	19	75.17	1
106	Max	-97	-1656.16	37	-16684.1	37	14314.5	31	277.92	19	2777.59	19	27.59	31	8887.42	19	75.17	1
106	Max	-123	-1656.16	37	-16684.1	37	14314.5	31	277.92	19	2777.59	19	27.59	31	8887.42	19	75.17	1
106	Max	-124	-1656.16	37	-16684.1	37	14314.5	31	277.92	19	2777.59	19	27.59	31	8887.42	19	75.17	1
106	Min.	-98	-4284.73	52	-43111.8	52	-14334.4	4	-139.46	40	-1396.48	40	-27.96	4	-7622.28	40	-75.57	34
106	Min.	-97	-4284.73	52	-43111.8	52	-14334.4	4	-139.46	40	-1396.48	40	-27.96	4	-7622.28	40	-75.57	34
106	Min.	-123	-4284.73	52	-43111.8	52	-14334.4	4	-139.46	40	-1396.48	40	-27.96	4	-7622.28	40	-75.57	34
106	Min.	-124	-4284.73	52	-43111.8	52	-14334.4	4	-139.46	40	-1396.48	40	-27.96	4	-7622.28	40	-75.57	34
106	Max	-94	-1340.24	37	-15237.3	37	6204.39	31	306.63	19	2975.92	19	25.04	31	10036.2	19	217.24	19
106	Max	-93	-1340.24	37	-15237.3	37	6204.39	31	306.63	19	2975.92	19	25.04	31	10036.2	19	217.24	19
106	Max	-119	-1340.24	37	-15237.3	37	6204.39	31	306.63	19	2975.92	19	25.04	31	10036.2	19	217.24	19
106	Max	-120	-1340.24	37	-15237.3	37	6204.39	31	306.63	19	2975.92	19	25.04	31	10036.2	19	217.24	19
106	Min.	-94	-3661.1	52	-42449.8	52	-7156.26	4	-172.05	40	-1594.74	40	-20.6	4	-8553.82	40	-240.05	40
106	Min.	-93	-3661.1	52	-42449.8	52	-7156.26	4	-172.05	40	-1594.74	40	-20.6	4	-8553.82	40	-240.05	40
106	Min.	-119	-3661.1	52	-42449.8	52	-7156.26	4	-172.05	40	-1594.74	40	-20.6	4	-8553.82	40	-240.05	40
106	Min.	-120	-3661.1	52	-42449.8	52	-7156.26	4	-172.05	40	-1594.74	40	-20.6	4	-8553.82	40	-240.05	40
106	Max	-93	-1192.8	40	-16219.1	37	1671.96	34	254.36	19	3032.92	19	44.01	34	9939.11	19	352.14	13
106	Max	-92	-1192.8	40	-16219.1	37	1671.96	34	254.36	19	3032.92	19	44.01	34	9939.11	19	352.14	13
106	Max	-118	-1192.8	40	-16219.1	37	1671.96	34	254.36	19	3032.92	19	44.01	34	9939.11	19	352.14	13
106	Max	-119	-1192.8	40	-16219.1	37	1671.96	34	254.36	19	3032.92	19	44.01	34	9939.11	19	352.14	13
106	Min.	-93	-2609.28	52	-43845.1	52	-4164.66	1	-156.14	40	-1634.24	40	3.2	1	-8868.89	40	-472.3	46
106	Min.	-92	-2609.28	52	-43845.1	52	-4164.66	1	-156.14	40	-1634.24	40	3.2	1	-8868.89	40	-472.3	46
106	Min.	-118	-2609.28	52	-43845.1	52	-4164.66	1	-156.14	40	-1634.24	40	3.2	1	-8868.89	40	-472.3	46
106	Min.	-119	-2609.28	52	-43845.1	52	-4164.66	1	-156.14	40	-1634.24	40	3.2	1	-8868.89	40	-472.3	46
106	Max	-97	-1628.03	37	-16506.2	37	13504.8	31	282.5	19	2825.26	19	26.75	34	9101.05	19	73.83	4
106	Max	-96	-1628.03	37	-16506.2	37	13504.8	31	282.5	19	2825.26	19	26.75	34	9101.05	19	73.83	4
106	Max	-122	-1628.03	37	-16506.2	37	13504.8	31	282.5	19	2825.26	19	26.75	34	9101.05	19	73.83	4
106	Max	-123	-1628.03	37	-16506.2	37	13504.8	31	282.5	19	2825.26	19	26.75	34	9101.05	19	73.83	4
106	Min.	-97	-4256.75	52	-43117.8	52	-13572.6	4	-143.98	40	-1444.84	40	-28.04	1	-7831.5	40	-76.63	31
106	Min.	-96	-4256.75	52	-43117.8	52	-13572.6	4	-143.98	40	-1444.84	40	-28.04	1	-7831.5	40	-76.63	31
106	Min.	-122	-4256.75	52	-43117.8	52	-13572.6	4	-143.98	40	-1444.84	40	-28.04	1	-7831.5	40	-76.63	31
106	Min.	-123	-4256.75	52	-43117.8	52	-13572.6	4	-143.98	40	-1444.84	40	-28.04	1	-7831.5	40	-76.63	31
106	Max	-96	-1594.43	37	-16292.1	37	11912.7	31	287.93	19	2872.48	19	26.11	31	9370.04	19	76.29	4
106	Max	-95	-1594.43	37	-16292.1	37	11912.7	31	287.93	19	2872.48	19	26.11	31	9370.04	19	76.29	4
106	Max	-121	-1594.43	37	-16292.1	37	11912.7	31	287.93	19	2872.48	19	26.11	31	9370.04	19	76.29	4
106	Max	-122	-1594.43	37	-16292.1	37	11912.7	31	287.93	19	2872.48	19	26.11	31	9370.04	19	76.29	4
106	Min.	-96	-4189.27	52	-43046.2	52	-12047.1	4	-150.37	40	-1494.13	40	-27.65	4	-8094.37	40	-85.43	31
106	Min.	-95	-4189.27	52	-43046.2	52	-12047.1	4	-150.37	40	-1494.13	40	-27.65	4	-8094.37	40	-85.43	31
106	Min.	-121	-4189.27	52	-43046.2	52	-12047.1	4	-150.37	40	-1494.13	40	-27.65	4	-8094.37	40	-85.43	31
106	Min.	-122	-4189.27	52	-43046.2	52	-12047.1	4	-150.37	40	-1494.13	40	-27.65	4	-8094.37	40	-85.43	31
106	Max	-95	-1518.59	37	-16124.9	37	9555.24	31	287.86	19	2920.82	19	24.26	34	9455.31	19	94.05	16
106	Max	-94	-1518.59	37	-16124.9	37	9555.24	31	287.86	19	2920.82	19	24.26	34	9455.31	19	94.05	16
106	Max	-120	-1518.59	37	-16124.9	37	9555.24	31	287.86	19	2920.82	19	24.26	34	9455.31	19	94.05	16
106	Max	-121	-1518.59	37	-16124.9	37	9555.24	31	287.86	19	2920.82	19	24.26	34	9455.31	19	94.05	16
106	Min.	-95	-4075.15	52	-42950.3	52	-9816	4	-150.47	40	-1546.4	40	-25.75	1	-8244.56	40	-90.11	43
106	Min.	-94	-4075.15	52	-42950.3	52	-9816	4	-150.47	40	-1546.4	40	-25.75	1	-8244.56	40	-90.11	43
106	Min.	-120	-4075.15	52	-42950.3	52	-9816	4	-150.47	40	-1546.4	40	-25.75	1	-8244.56	40	-90.11	43
106	Min.	-121	-4075.15	52	-42950.3	52	-9816	4	-150.47	40	-1546.4	40	-25.75	1	-8244.56	40	-90.11	43
106	Max	-99	-1656.16	16	-16684.1	16	14334.4	34	277.92	46	2777.59	46	27.96	34	8887.42	46	75.57	4
106	Max	-98	-1656.16	16	-16684.1	16	14334.4	34	277.92	46	2777.59	46	27.96	34	8887.42	46	75.57	4
106	Max	-124	-1656.16	16	-16684.1	16	14334.4	34	277.92	46	2777.59	46	27.96	34	8887.42	46	75.57	4
106	Max	-125	-1656.16	16	-16684.1	16	14334.4	34	277.92	46	2777.59	46	27.96	34	8887.42	46	75.57	4
106	Min.	-99	-4284.73	52	-43111.8	52	-14314.5	1	-139.46	13	-1396.48	13	-27.59	1	-7622.28	13	-75.17	31
106	Min.	-98	-4284.73	52	-43111.8	52	-14314.5	1	-139.46	13	-1396.48	13	-27.59	1	-7622.28	13	-75.17	31
106	Min.	-124	-4284.73	52	-43111.8	52	-14314.5	1	-139.46	13	-1396.48	13	-27.59	1	-7622.28	13	-75.17	31
106	Min.	-125	-4284.73	52	-43111.8	52	-14314.5	1	-139.46	13	-1396.48	13	-27.59	1	-7622.28	13	-75.17	31
106	Max	-13	-889.12	31	-16778.2	31	2204.13	31	281.4	13	3334.5	13	54.82	25	7308.35	46	507.07	40
106	Max	-12	-889.12	31	-16778.2	31	2204.13	31	281.4	13	3334.5	13	54.82	25	7308.35	46	507.07	40
106	Max	-77	-889.12	31	-16778.2	31	2204.13	31	281.4	13	3334.5	13	54.82	25	7308.35	46	507.07	40
106	Max	-78	-889.12	31	-16778.2	31	2204.13	31	281.4	13	3334.5	13	54.82	25	7308.35	46	507.07	40
106	Min.	-13	-3071.41	49	-49465.5	49	-5044.45	4	-134.59	46	-1379.3	46	-4.39	10	-11536.8	13	-302.44	19
106	Min.	-12	-3071.41	49	-49465.5	49	-5044.45	4	-134.59	46	-1379.3	46	-4.39	10	-11536.8	13	-302.44	19
106	Min.	-77	-3071.41	49	-49465.5	49	-5044.45	4	-134.59	46	-1379.3	46	-4.39	10	-11536.8	13	-302.44	19
106	Min.	-78	-3071.41	49	-49465.5	49	-5044.45	4	-134.59	46	-1379.3	46	-4.39	10	-11536.8	13	-302.44	19
106	Max	-70	-1734.99	13	-18184.1	13	11944.2	34	122.14	50	1223.48	50	36.12	34	8345.7	19	92.79	34
106	Max	-69	-1734.99	13	-18184.1	13	11944.2	34	122.14	50	1223.48	50	36.12	34				

Relazione geotecnica tombino

106	Max	-95	-1652.89	13	-17797.8	13	9644.88	31	121.59	50	1224.05	50	37.45	31	8733.32	19	94.85	31
106	Min.	-69	-4111.56	52	-45574	52	-9632.01	4	52.25	1	550.47	1	-37.25	4	-9367.28	40	-99.19	4
106	Min.	-68	-4111.56	52	-45574	52	-9632.01	4	52.25	1	550.47	1	-37.25	4	-9367.28	40	-99.19	4
106	Min.	-94	-4111.56	52	-45574	52	-9632.01	4	52.25	1	550.47	1	-37.25	4	-9367.28	40	-99.19	4
106	Min.	-95	-4111.56	52	-45574	52	-9632.01	4	52.25	1	550.47	1	-37.25	4	-9367.28	40	-99.19	4
106	Max	-12	-1554.47	31	-18739.8	40	6096.09	31	338.02	13	3263.15	13	32.88	28	6998.19	46	246.82	46
106	Max	-11	-1554.47	31	-18739.8	40	6096.09	31	338.02	13	3263.15	13	32.88	28	6998.19	46	246.82	46
106	Max	-76	-1554.47	31	-18739.8	40	6096.09	31	338.02	13	3263.15	13	32.88	28	6998.19	46	246.82	46
106	Max	-77	-1554.47	31	-18739.8	40	6096.09	31	338.02	13	3263.15	13	32.88	28	6998.19	46	246.82	46
106	Min.	-12	-4213.33	49	-47755.4	52	-7179.3	4	-146.41	46	-1334.04	46	-28.63	7	-11641.8	13	-263.03	13
106	Min.	-11	-4213.33	49	-47755.4	52	-7179.3	4	-146.41	46	-1334.04	46	-28.63	7	-11641.8	13	-263.03	13
106	Min.	-76	-4213.33	49	-47755.4	52	-7179.3	4	-146.41	46	-1334.04	46	-28.63	7	-11641.8	13	-263.03	13
106	Min.	-77	-4213.33	49	-47755.4	52	-7179.3	4	-146.41	46	-1334.04	46	-28.63	7	-11641.8	13	-263.03	13
106	Max	-11	-1861.84	40	-18957	40	9409.19	31	315.23	13	3193.21	13	33	25	6686.34	46	170.16	31
106	Max	-10	-1861.84	40	-18957	40	9409.19	31	315.23	13	3193.21	13	33	25	6686.34	46	170.16	31
106	Max	-75	-1861.84	40	-18957	40	9409.19	31	315.23	13	3193.21	13	33	25	6686.34	46	170.16	31
106	Max	-76	-1861.84	40	-18957	40	9409.19	31	315.23	13	3193.21	13	33	25	6686.34	46	170.16	31
106	Min.	-11	-4607.61	52	-48335.7	52	-9694.19	4	-124.11	46	-1272.06	46	-34.38	10	-11008.3	13	-161.88	4
106	Min.	-10	-4607.61	52	-48335.7	52	-9694.19	4	-124.11	46	-1272.06	46	-34.38	10	-11008.3	13	-161.88	4
106	Min.	-75	-4607.61	52	-48335.7	52	-9694.19	4	-124.11	46	-1272.06	46	-34.38	10	-11008.3	13	-161.88	4
106	Min.	-76	-4607.61	52	-48335.7	52	-9694.19	4	-124.11	46	-1272.06	46	-34.38	10	-11008.3	13	-161.88	4
106	Max	-10	-1913.75	40	-19605.2	40	11796.2	31	314.15	13	3130.65	13	35.1	28	6524.52	46	186.96	34
106	Max	-9	-1913.75	40	-19605.2	40	11796.2	31	314.15	13	3130.65	13	35.1	28	6524.52	46	186.96	34
106	Max	-74	-1913.75	40	-19605.2	40	11796.2	31	314.15	13	3130.65	13	35.1	28	6524.52	46	186.96	34
106	Max	-75	-1913.75	40	-19605.2	40	11796.2	31	314.15	13	3130.65	13	35.1	28	6524.52	46	186.96	34
106	Min.	-10	-4729.07	52	-48463.7	52	-11934	4	-121.52	46	-1204.47	46	-36.86	7	-10944.7	13	-178.13	1
106	Min.	-9	-4729.07	52	-48463.7	52	-11934	4	-121.52	46	-1204.47	46	-36.86	7	-10944.7	13	-178.13	1
106	Min.	-74	-4729.07	52	-48463.7	52	-11934	4	-121.52	46	-1204.47	46	-36.86	7	-10944.7	13	-178.13	1
106	Min.	-75	-4729.07	52	-48463.7	52	-11934	4	-121.52	46	-1204.47	46	-36.86	7	-10944.7	13	-178.13	1
106	Max	-9	-1993.3	40	-20169.7	40	13380.9	31	306.93	13	3068.1	13	36.43	25	6264.57	46	183.23	34
106	Max	-8	-1993.3	40	-20169.7	40	13380.9	31	306.93	13	3068.1	13	36.43	25	6264.57	46	183.23	34
106	Max	-73	-1993.3	40	-20169.7	40	13380.9	31	306.93	13	3068.1	13	36.43	25	6264.57	46	183.23	34
106	Max	-74	-1993.3	40	-20169.7	40	13380.9	31	306.93	13	3068.1	13	36.43	25	6264.57	46	183.23	34
106	Min.	-9	-4798.61	52	-48534.3	52	-13447.1	4	-113.58	46	-1139.07	46	-37.75	10	-10670.8	13	-179.7	1
106	Min.	-8	-4798.61	52	-48534.3	52	-13447.1	4	-113.58	46	-1139.07	46	-37.75	10	-10670.8	13	-179.7	1
106	Min.	-73	-4798.61	52	-48534.3	52	-13447.1	4	-113.58	46	-1139.07	46	-37.75	10	-10670.8	13	-179.7	1
106	Min.	-74	-4798.61	52	-48534.3	52	-13447.1	4	-113.58	46	-1139.07	46	-37.75	10	-10670.8	13	-179.7	1
106	Max	-8	-2056.06	40	-20681.1	40	14180.9	31	300.65	13	3004.33	13	37.4	28	6052.06	46	183.45	31
106	Max	-7	-2056.06	40	-20681.1	40	14180.9	31	300.65	13	3004.33	13	37.4	28	6052.06	46	183.45	31
106	Max	-72	-2056.06	40	-20681.1	40	14180.9	31	300.65	13	3004.33	13	37.4	28	6052.06	46	183.45	31
106	Max	-73	-2056.06	40	-20681.1	40	14180.9	31	300.65	13	3004.33	13	37.4	28	6052.06	46	183.45	31
106	Min.	-8	-4826.48	52	-48529.6	52	-14199.8	4	-107.28	46	-1074.32	46	-37.79	7	-10458	13	-182.66	4
106	Min.	-7	-4826.48	52	-48529.6	52	-14199.8	4	-107.28	46	-1074.32	46	-37.79	7	-10458	13	-182.66	4
106	Min.	-72	-4826.48	52	-48529.6	52	-14199.8	4	-107.28	46	-1074.32	46	-37.79	7	-10458	13	-182.66	4
106	Min.	-73	-4826.48	52	-48529.6	52	-14199.8	4	-107.28	46	-1074.32	46	-37.79	7	-10458	13	-182.66	4
106	Max	-7	-2056.06	13	-20681.1	13	14199.8	34	300.65	40	3004.33	40	37.79	25	6052.06	19	182.66	34
106	Max	-6	-2056.06	13	-20681.1	13	14199.8	34	300.65	40	3004.33	40	37.79	25	6052.06	19	182.66	34
106	Max	-71	-2056.06	13	-20681.1	13	14199.8	34	300.65	40	3004.33	40	37.79	25	6052.06	19	182.66	34
106	Max	-72	-2056.06	13	-20681.1	13	14199.8	34	300.65	40	3004.33	40	37.79	25	6052.06	19	182.66	34
106	Min.	-7	-4826.48	52	-48529.6	52	-14180.9	1	-107.28	19	-1074.32	19	-37.4	10	-10458	40	-183.45	1
106	Min.	-6	-4826.48	52	-48529.6	52	-14180.9	1	-107.28	19	-1074.32	19	-37.4	10	-10458	40	-183.45	1
106	Min.	-71	-4826.48	52	-48529.6	52	-14180.9	1	-107.28	19	-1074.32	19	-37.4	10	-10458	40	-183.45	1
106	Min.	-72	-4826.48	52	-48529.6	52	-14180.9	1	-107.28	19	-1074.32	19	-37.4	10	-10458	40	-183.45	1
106	Max	-6	-1993.3	13	-20169.7	13	13447.1	34	306.93	40	3068.1	40	37.75	28	6264.57	19	179.7	31
106	Max	-5	-1993.3	13	-20169.7	13	13447.1	34	306.93	40	3068.1	40	37.75	28	6264.57	19	179.7	31
106	Max	-70	-1993.3	13	-20169.7	13	13447.1	34	306.93	40	3068.1	40	37.75	28	6264.57	19	179.7	31
106	Max	-71	-1993.3	13	-20169.7	13	13447.1	34	306.93	40	3068.1	40	37.75	28	6264.57	19	179.7	31
106	Min.	-6	-4798.61	52	-48534.3	52	-13380.9	1	-113.58	19	-1139.07	19	-36.43	7	-10670.8	40	-183.23	4
106	Min.	-5	-4798.61	52	-48534.3	52	-13380.9	1	-113.58	19	-1139.07	19	-36.43	7	-10670.8	40	-183.23	4
106	Min.	-70	-4798.61	52	-48534.3	52	-13380.9	1	-113.58	19	-1139.07	19	-36.43	7	-10670.8	40	-183.23	4
106	Min.	-71	-4798.61	52	-48534.3	52	-13380.9	1	-113.58	19	-1139.07	19	-36.43	7	-10670.8	40	-183.23	4
106	Max	-5	-1913.75	13	-19605.2	13	11934	34	314.15	40	3130.65	40	36.86	25	6524.52	19	178.13	31
106	Max	-4	-1913.75	13	-19605.2	13	11934	34	314.15	40	3130.65	40	36.86	25	6524.52	19	178.13	31
106	Max	-69	-1913.75	13	-19605.2	13	11934	34	314.15	40	3130.65	40	36.86	25	6524.52	19	178.13	31
106	Max	-70	-1913.75	13	-19605.2	13	11934	34	314.15	40	3130.65	40	36.86	25	6524.52	19	178.13	31
106	Min.	-5	-4729.07	52	-48463.7	52	-11796.2	1	-121.52	19	-1204.47	19	-35.1	10	-10944.7	40	-186.96	4
106	Min.	-4	-4729.07	52	-48463.7	52	-11796.2	1	-121.52	19	-1204.47	19	-35.1	10	-10944.7	40	-186.96	4
106	Min.	-69	-4729.07	52	-48463.7	52	-11796.2	1	-121.52	19	-1204.47	19	-35.1	10	-10944.7	40	-186.96	4
106	Min.	-70	-4729.07	52	-48463.7	52	-11796.2	1	-121.52	19	-1204.47	19	-35.1	10	-10944.7	40	-186.96	4
106	Max	-4	-1861.84	13	-18957	13	9694.19	34	315.23	40	3193.21	40	34.38	28	6686.34	19	161.88	34
106	Max	-3	-1861.84	13	-18957	13	9694.19	34	315.23	40	3193.21	40	34.38	28	6686.34	19	161.88	34
106	Max	-68	-1861.84	13	-18957	13	9694.19	34	315.23	40	3193.21	40	34.38	28	6686.34	19	161.88	34
106	Max	-69	-18															

Relazione geotecnica tombino

106	Min.	-3	-4213.33	50	-47755.4	52	-6096.09	1	-146.41	19	-1334.04	19	-32.88	10	-11641.8	40	-246.82	19
106	Min.	-2	-4213.33	50	-47755.4	52	-6096.09	1	-146.41	19	-1334.04	19	-32.88	10	-11641.8	40	-246.82	19
106	Min.	-67	-4213.33	50	-47755.4	52	-6096.09	1	-146.41	19	-1334.04	19	-32.88	10	-11641.8	40	-246.82	19
106	Min.	-68	-4213.33	50	-47755.4	52	-6096.09	1	-146.41	19	-1334.04	19	-32.88	10	-11641.8	40	-246.82	19
106	Max	-2	-889.12	1	-16778.2	1	5044.45	34	281.4	40	3334.5	40	4.39	28	7308.35	19	302.44	46
106	Max	-1	-889.12	1	-16778.2	1	5044.45	34	281.4	40	3334.5	40	4.39	28	7308.35	19	302.44	46
106	Max	-66	-889.12	1	-16778.2	1	5044.45	34	281.4	40	3334.5	40	4.39	28	7308.35	19	302.44	46
106	Max	-67	-889.12	1	-16778.2	1	5044.45	34	281.4	40	3334.5	40	4.39	28	7308.35	19	302.44	46
106	Min.	-2	-3071.41	50	-49465.5	50	-2204.13	1	-134.59	19	-1379.3	19	-54.82	7	-11536.8	40	-507.07	13
106	Min.	-1	-3071.41	50	-49465.5	50	-2204.13	1	-134.59	19	-1379.3	19	-54.82	7	-11536.8	40	-507.07	13
106	Min.	-66	-3071.41	50	-49465.5	50	-2204.13	1	-134.59	19	-1379.3	19	-54.82	7	-11536.8	40	-507.07	13
106	Min.	-67	-3071.41	50	-49465.5	50	-2204.13	1	-134.59	19	-1379.3	19	-54.82	7	-11536.8	40	-507.07	13
106	Max	-78	-369.37	31	-17477.4	40	2922.79	31	42.18	49	1252.65	49	41.68	46	9228.08	46	299.39	49
106	Max	-77	-369.37	31	-17477.4	40	2922.79	31	42.18	49	1252.65	49	41.68	46	9228.08	46	299.39	49
106	Max	-103	-369.37	31	-17477.4	40	2922.79	31	42.18	49	1252.65	49	41.68	46	9228.08	46	299.39	49
106	Max	-104	-369.37	31	-17477.4	40	2922.79	31	42.18	49	1252.65	49	41.68	46	9228.08	46	299.39	49
106	Min.	-78	-912.39	49	-45554.1	52	-2918.18	4	13.24	31	531.4	31	-44.86	13	-9880.64	13	151.85	31
106	Min.	-77	-912.39	49	-45554.1	52	-2918.18	4	13.24	31	531.4	31	-44.86	13	-9880.64	13	151.85	31
106	Min.	-103	-912.39	49	-45554.1	52	-2918.18	4	13.24	31	531.4	31	-44.86	13	-9880.64	13	151.85	31
106	Min.	-104	-912.39	49	-45554.1	52	-2918.18	4	13.24	31	531.4	31	-44.86	13	-9880.64	13	151.85	31
106	Max	-77	-1421.84	40	-17802.9	40	6818.15	31	118.11	49	1222.93	49	37.55	31	8649.15	46	85.32	34
106	Max	-76	-1421.84	40	-17802.9	40	6818.15	31	118.11	49	1222.93	49	37.55	31	8649.15	46	85.32	34
106	Max	-102	-1421.84	40	-17802.9	40	6818.15	31	118.11	49	1222.93	49	37.55	31	8649.15	46	85.32	34
106	Max	-103	-1421.84	40	-17802.9	40	6818.15	31	118.11	49	1222.93	49	37.55	31	8649.15	46	85.32	34
106	Min.	-77	-3464.24	52	-46149.9	52	-6890.36	4	46.19	31	530.53	31	-37.15	4	-9252.61	13	-78.71	1
106	Min.	-76	-3464.24	52	-46149.9	52	-6890.36	4	46.19	31	530.53	31	-37.15	4	-9252.61	13	-78.71	1
106	Min.	-102	-3464.24	52	-46149.9	52	-6890.36	4	46.19	31	530.53	31	-37.15	4	-9252.61	13	-78.71	1
106	Min.	-103	-3464.24	52	-46149.9	52	-6890.36	4	46.19	31	530.53	31	-37.15	4	-9252.61	13	-78.71	1
106	Max	-76	-1652.89	40	-17797.8	40	9632.01	34	121.59	49	1224.05	49	37.25	34	8733.32	46	99.19	34
106	Max	-75	-1652.89	40	-17797.8	40	9632.01	34	121.59	49	1224.05	49	37.25	34	8733.32	46	99.19	34
106	Max	-101	-1652.89	40	-17797.8	40	9632.01	34	121.59	49	1224.05	49	37.25	34	8733.32	46	99.19	34
106	Max	-102	-1652.89	40	-17797.8	40	9632.01	34	121.59	49	1224.05	49	37.25	34	8733.32	46	99.19	34
106	Min.	-76	-4111.56	52	-45574	52	-9644.88	1	52.25	31	550.47	31	-37.45	1	-9367.28	13	-94.85	1
106	Min.	-75	-4111.56	52	-45574	52	-9644.88	1	52.25	31	550.47	31	-37.45	1	-9367.28	13	-94.85	1
106	Min.	-101	-4111.56	52	-45574	52	-9644.88	1	52.25	31	550.47	31	-37.45	1	-9367.28	13	-94.85	1
106	Min.	-102	-4111.56	52	-45574	52	-9644.88	1	52.25	31	550.47	31	-37.45	1	-9367.28	13	-94.85	1
106	Max	-75	-1734.99	40	-18184.1	40	11945.4	31	122.14	49	1223.48	49	36.34	31	8345.7	46	110.76	31
106	Max	-74	-1734.99	40	-18184.1	40	11945.4	31	122.14	49	1223.48	49	36.34	31	8345.7	46	110.76	31
106	Max	-100	-1734.99	40	-18184.1	40	11945.4	31	122.14	49	1223.48	49	36.34	31	8345.7	46	110.76	31
106	Max	-101	-1734.99	40	-18184.1	40	11945.4	31	122.14	49	1223.48	49	36.34	31	8345.7	46	110.76	31
106	Min.	-75	-4349.06	52	-45817.1	52	-11944.2	4	56.28	31	574.58	31	-36.12	4	-8963.47	13	-92.79	4
106	Min.	-74	-4349.06	52	-45817.1	52	-11944.2	4	56.28	31	574.58	31	-36.12	4	-8963.47	13	-92.79	4
106	Min.	-100	-4349.06	52	-45817.1	52	-11944.2	4	56.28	31	574.58	31	-36.12	4	-8963.47	13	-92.79	4
106	Min.	-101	-4349.06	52	-45817.1	52	-11944.2	4	56.28	31	574.58	31	-36.12	4	-8963.47	13	-92.79	4
106	Max	-74	-1801.7	40	-18471.2	40	13506.7	31	123.26	49	1223.94	49	36.64	34	8179.66	46	109.42	31
106	Max	-73	-1801.7	40	-18471.2	40	13506.7	31	123.26	49	1223.94	49	36.64	34	8179.66	46	109.42	31
106	Max	-99	-1801.7	40	-18471.2	40	13506.7	31	123.26	49	1223.94	49	36.64	34	8179.66	46	109.42	31
106	Max	-100	-1801.7	40	-18471.2	40	13506.7	31	123.26	49	1223.94	49	36.64	34	8179.66	46	109.42	31
106	Min.	-74	-4473.92	52	-45837.7	52	-13506.2	4	60.03	31	601.18	31	-36.61	1	-8806.49	13	-103.1	4
106	Min.	-73	-4473.92	52	-45837.7	52	-13506.2	4	60.03	31	601.18	31	-36.61	1	-8806.49	13	-103.1	4
106	Min.	-99	-4473.92	52	-45837.7	52	-13506.2	4	60.03	31	601.18	31	-36.61	1	-8806.49	13	-103.1	4
106	Min.	-100	-4473.92	52	-45837.7	52	-13506.2	4	60.03	31	601.18	31	-36.61	1	-8806.49	13	-103.1	4
106	Max	-73	-1849.08	40	-18733	40	14286.2	31	123.12	52	1224.71	52	36.56	31	7936.22	46	108.29	34
106	Max	-72	-1849.08	40	-18733	40	14286.2	31	123.12	52	1224.71	52	36.56	31	7936.22	46	108.29	34
106	Max	-98	-1849.08	40	-18733	40	14286.2	31	123.12	52	1224.71	52	36.56	31	7936.22	46	108.29	34
106	Max	-99	-1849.08	40	-18733	40	14286.2	31	123.12	52	1224.71	52	36.56	31	7936.22	46	108.29	34
106	Min.	-73	-4530.9	52	-45838.3	52	-14285.8	4	62.15	40	618.41	40	-36.54	4	-8561.32	13	-107.11	1
106	Min.	-72	-4530.9	52	-45838.3	52	-14285.8	4	62.15	40	618.41	40	-36.54	4	-8561.32	13	-107.11	1
106	Min.	-98	-4530.9	52	-45838.3	52	-14285.8	4	62.15	40	618.41	40	-36.54	4	-8561.32	13	-107.11	1
106	Min.	-99	-4530.9	52	-45838.3	52	-14285.8	4	62.15	40	618.41	40	-36.54	4	-8561.32	13	-107.11	1
106	Max	-72	-1849.08	13	-18733	13	14285.8	34	123.12	52	1224.71	52	36.54	34	7936.22	19	107.11	31
106	Max	-71	-1849.08	13	-18733	13	14285.8	34	123.12	52	1224.71	52	36.54	34	7936.22	19	107.11	31
106	Max	-97	-1849.08	13	-18733	13	14285.8	34	123.12	52	1224.71	52	36.54	34	7936.22	19	107.11	31
106	Max	-98	-1849.08	13	-18733	13	14285.8	34	123.12	52	1224.71	52	36.54	34	7936.22	19	107.11	31
106	Min.	-72	-4530.9	52	-45838.3	52	-14286.2	1	62.15	13	618.41	13	-36.56	1	-8561.32	40	-108.29	4
106	Min.	-71	-4530.9	52	-45838.3	52	-14286.2	1	62.15	13	618.41	13	-36.56	1	-8561.32	40	-108.29	4
106	Min.	-97	-4530.9	52	-45838.3	52	-14286.2	1	62.15	13	618.41	13	-36.56	1	-8561.32	40	-108.29	4
106	Min.	-98	-4530.9	52	-45838.3	52	-14286.2	1	62.15	13	618.41	13	-36.56	1	-8561.32	40	-108.29	4
106	Max	-71	-1801.7	13	-18471.2	13	13506.2	34	123.26	50	1223.94	50	36.61	31	8179.66	19	103.1	34
106	Max	-70	-1801.7	13	-18471.2	13	13506.2	34	123.26	50	1223.94	50	36.61	31	8179.66	19	103.1	34
106	Max	-96	-1801.7	13	-18471.2	13	13506.2	34	123.26	50	1223.94	50	36.61	31	8179.66	19	103.1	34
106	Max	-97	-1801.7	13	-18471.2	13	13506.2	34	123.26	50	1223.94	50	36.61	31	8179.66	19	103.1	34
106	Min.	-71	-4473.92															

Relazione geotecnica tombino

106	Min.	-102	-3661.1	52	-42449.8	52	-6204.4	1	-172.05	13	-1594.74	13	-25.04	1	-8553.82	13	-217.23	46
106	Min.	-128	-3661.1	52	-42449.8	52	-6204.4	1	-172.05	13	-1594.74	13	-25.04	1	-8553.82	13	-217.23	46
106	Min.	-129	-3661.1	52	-42449.8	52	-6204.4	1	-172.05	13	-1594.74	13	-25.04	1	-8553.82	13	-217.23	46
106	Max	-102	-1518.59	16	-16124.9	16	9816	34	287.86	46	2920.82	46	25.75	31	9455.31	46	90.11	22
106	Max	-101	-1518.59	16	-16124.9	16	9816	34	287.86	46	2920.82	46	25.75	31	9455.31	46	90.11	22
106	Max	-127	-1518.59	16	-16124.9	16	9816	34	287.86	46	2920.82	46	25.75	31	9455.31	46	90.11	22
106	Max	-128	-1518.59	16	-16124.9	16	9816	34	287.86	46	2920.82	46	25.75	31	9455.31	46	90.11	22
106	Min.	-102	-4075.15	52	-42950.3	52	-9555.24	1	-150.47	13	-1546.4	13	-24.26	4	-8244.56	13	-94.05	37
106	Min.	-101	-4075.15	52	-42950.3	52	-9555.24	1	-150.47	13	-1546.4	13	-24.26	4	-8244.56	13	-94.05	37
106	Min.	-127	-4075.15	52	-42950.3	52	-9555.24	1	-150.47	13	-1546.4	13	-24.26	4	-8244.56	13	-94.05	37
106	Min.	-128	-4075.15	52	-42950.3	52	-9555.24	1	-150.47	13	-1546.4	13	-24.26	4	-8244.56	13	-94.05	37
106	Max	-68	-1421.84	13	-17802.9	13	6890.36	34	118.11	50	1222.93	50	37.15	34	8649.15	19	78.71	31
106	Max	-67	-1421.84	13	-17802.9	13	6890.36	34	118.11	50	1222.93	50	37.15	34	8649.15	19	78.71	31
106	Max	-93	-1421.84	13	-17802.9	13	6890.36	34	118.11	50	1222.93	50	37.15	34	8649.15	19	78.71	31
106	Max	-94	-1421.84	13	-17802.9	13	6890.36	34	118.11	50	1222.93	50	37.15	34	8649.15	19	78.71	31
106	Min.	-68	-3464.24	52	-46149.9	52	-6818.15	1	46.19	1	530.53	1	-37.55	1	-9252.61	40	-85.32	4
106	Min.	-67	-3464.24	52	-46149.9	52	-6818.15	1	46.19	1	530.53	1	-37.55	1	-9252.61	40	-85.32	4
106	Min.	-93	-3464.24	52	-46149.9	52	-6818.15	1	46.19	1	530.53	1	-37.55	1	-9252.61	40	-85.32	4
106	Min.	-94	-3464.24	52	-46149.9	52	-6818.15	1	46.19	1	530.53	1	-37.55	1	-9252.61	40	-85.32	4
106	Max	-67	-369.37	1	-17477.4	13	2918.18	34	42.18	50	1252.65	50	44.86	40	9228.08	19	-151.85	1
106	Max	-66	-369.37	1	-17477.4	13	2918.18	34	42.18	50	1252.65	50	44.86	40	9228.08	19	-151.85	1
106	Max	-92	-369.37	1	-17477.4	13	2918.18	34	42.18	50	1252.65	50	44.86	40	9228.08	19	-151.85	1
106	Max	-93	-369.37	1	-17477.4	13	2918.18	34	42.18	50	1252.65	50	44.86	40	9228.08	19	-151.85	1
106	Min.	-67	-912.39	50	-45554.1	52	-2922.79	1	13.24	1	531.4	1	-41.68	19	-9880.64	40	-299.39	50
106	Min.	-66	-912.39	50	-45554.1	52	-2922.79	1	13.24	1	531.4	1	-41.68	19	-9880.64	40	-299.39	50
106	Min.	-92	-912.39	50	-45554.1	52	-2922.79	1	13.24	1	531.4	1	-41.68	19	-9880.64	40	-299.39	50
106	Min.	-93	-912.39	50	-45554.1	52	-2922.79	1	13.24	1	531.4	1	-41.68	19	-9880.64	40	-299.39	50
106	Max	-104	-1192.8	13	-16219.1	16	4164.66	31	254.36	46	3032.92	46	-3.2	31	9939.11	46	472.3	19
106	Max	-103	-1192.8	13	-16219.1	16	4164.66	31	254.36	46	3032.92	46	-3.2	31	9939.11	46	472.3	19
106	Max	-129	-1192.8	13	-16219.1	16	4164.66	31	254.36	46	3032.92	46	-3.2	31	9939.11	46	472.3	19
106	Max	-130	-1192.8	13	-16219.1	16	4164.66	31	254.36	46	3032.92	46	-3.2	31	9939.11	46	472.3	19
106	Min.	-104	-2609.28	52	-43845.1	52	-1671.96	4	-156.14	13	-1634.24	13	-44.01	4	-8868.89	13	-352.14	40
106	Min.	-103	-2609.28	52	-43845.1	52	-1671.96	4	-156.14	13	-1634.24	13	-44.01	4	-8868.89	13	-352.14	40
106	Min.	-129	-2609.28	52	-43845.1	52	-1671.96	4	-156.14	13	-1634.24	13	-44.01	4	-8868.89	13	-352.14	40
106	Min.	-130	-2609.28	52	-43845.1	52	-1671.96	4	-156.14	13	-1634.24	13	-44.01	4	-8868.89	13	-352.14	40
106	Max	-101	-1594.43	16	-16292.1	16	12047.1	34	287.93	46	2872.48	46	27.65	34	9370.04	46	85.43	1
106	Max	-100	-1594.43	16	-16292.1	16	12047.1	34	287.93	46	2872.48	46	27.65	34	9370.04	46	85.43	1
106	Max	-126	-1594.43	16	-16292.1	16	12047.1	34	287.93	46	2872.48	46	27.65	34	9370.04	46	85.43	1
106	Max	-127	-1594.43	16	-16292.1	16	12047.1	34	287.93	46	2872.48	46	27.65	34	9370.04	46	85.43	1
106	Min.	-101	-4189.27	52	-43046.2	52	-11912.7	1	-150.37	13	-1494.13	13	-26.11	1	-8094.37	13	-76.29	34
106	Min.	-100	-4189.27	52	-43046.2	52	-11912.7	1	-150.37	13	-1494.13	13	-26.11	1	-8094.37	13	-76.29	34
106	Min.	-126	-4189.27	52	-43046.2	52	-11912.7	1	-150.37	13	-1494.13	13	-26.11	1	-8094.37	13	-76.29	34
106	Min.	-127	-4189.27	52	-43046.2	52	-11912.7	1	-150.37	13	-1494.13	13	-26.11	1	-8094.37	13	-76.29	34
106	Max	-100	-1628.03	16	-16506.2	16	13572.6	34	282.5	46	2825.26	46	28.04	31	9101.05	46	76.63	1
106	Max	-99	-1628.03	16	-16506.2	16	13572.6	34	282.5	46	2825.26	46	28.04	31	9101.05	46	76.63	1
106	Max	-125	-1628.03	16	-16506.2	16	13572.6	34	282.5	46	2825.26	46	28.04	31	9101.05	46	76.63	1
106	Max	-126	-1628.03	16	-16506.2	16	13572.6	34	282.5	46	2825.26	46	28.04	31	9101.05	46	76.63	1
106	Min.	-100	-4256.75	52	-43117.8	52	-13504.8	1	-143.98	13	-1444.84	13	-26.75	4	-7831.5	13	-73.83	34
106	Min.	-99	-4256.75	52	-43117.8	52	-13504.8	1	-143.98	13	-1444.84	13	-26.75	4	-7831.5	13	-73.83	34
106	Min.	-125	-4256.75	52	-43117.8	52	-13504.8	1	-143.98	13	-1444.84	13	-26.75	4	-7831.5	13	-73.83	34
106	Min.	-126	-4256.75	52	-43117.8	52	-13504.8	1	-143.98	13	-1444.84	13	-26.75	4	-7831.5	13	-73.83	34
403	Max	-65	0	1	0	1	0	1	4543.75	13	199.63	13	312.99	25	1485.55	25	23147.8	49
403	Max	-52	0	1	0	1	0	1	4543.75	13	199.63	13	312.99	25	1485.55	25	23147.8	49
403	Max	-51	0	1	0	1	0	1	4543.75	13	199.63	13	312.99	25	1485.55	25	23147.8	49
403	Max	-64	0	1	0	1	0	1	4543.75	13	199.63	13	312.99	25	1485.55	25	23147.8	49
403	Min.	-65	0	1	0	1	0	1	-1885.42	46	-197.87	46	-68.68	10	-528.88	10	8062.09	7
403	Min.	-52	0	1	0	1	0	1	-1885.42	46	-197.87	46	-68.68	10	-528.88	10	8062.09	7
403	Min.	-51	0	1	0	1	0	1	-1885.42	46	-197.87	46	-68.68	10	-528.88	10	8062.09	7
403	Min.	-64	0	1	0	1	0	1	-1885.42	46	-197.87	46	-68.68	10	-528.88	10	8062.09	7
403	Max	-50	0	1	0	1	0	1	8355.44	51	830.51	49	156.33	25	621.28	34	11475.9	43
403	Max	-37	0	1	0	1	0	1	8355.44	51	830.51	49	156.33	25	621.28	34	11475.9	43
403	Max	-36	0	1	0	1	0	1	8355.44	51	830.51	49	156.33	25	621.28	34	11475.9	43
403	Max	-49	0	1	0	1	0	1	8355.44	51	830.51	49	156.33	25	621.28	34	11475.9	43
403	Min.	-50	0	1	0	1	0	1	3037.67	46	251.45	34	-162.43	10	-510.51	1	-2984.09	16
403	Min.	-37	0	1	0	1	0	1	3037.67	46	251.45	34	-162.43	10	-510.51	1	-2984.09	16
403	Min.	-36	0	1	0	1	0	1	3037.67	46	251.45	34	-162.43	10	-510.51	1	-2984.09	16
403	Min.	-49	0	1	0	1	0	1	3037.67	46	251.45	34	-162.43	10	-510.51	1	-2984.09	16
403	Max	-30	0	1	0	1	0	1	8355.44	52	830.51	50	156.33	34	510.51	10	2984.09	19
403	Max	-17	0	1	0	1	0	1	8355.44	52	830.51	50	156.33	34	510.51	10	2984.09	19
403	Max	-16	0	1	0	1	0	1	8355.44	52	830.51	50	156.33	34	510.51	10	2984.09	19
403	Max	-29	0	1	0	1	0	1	8355.44	52	830.51	50	156.33	34	510.51	10	2984.09	19
403	Min.	-30	0	1	0	1	0	1	3037.67	37	251.45	25	-162.43	1	-621.28	25	-11475.9	40
403	Min.	-17	0	1	0	1	0	1	3037.67	37	251.45	25	-162.43	1	-621.28	25	-11475.9	40
403	Min.	-16	0	1	0	1	0	1	3037.67	37	251.45	25	-162.43	1	-621.28	25	-11475.9	40
403	Min.	-29	0	1	0	1	0	1	3037.67									

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403	Min.	-3	0	1	0	1	0	1	-1774.15	37	-197.37	37	-212.54	4	-554.73	31	-22317.4	50
403	Min.	-16	0	1	0	1	0	1	-1774.15	37	-197.37	37	-212.54	4	-554.73	31	-22317.4	50
403	Max	-55	0	1	0	1	0	1	4455.46	40	433.79	40	171.12	28	472.15	28	21894.4	50
403	Max	-42	0	1	0	1	0	1	4455.46	40	433.79	40	171.12	28	472.15	28	21894.4	50
403	Max	-41	0	1	0	1	0	1	4455.46	40	433.79	40	171.12	28	472.15	28	21894.4	50
403	Max	-54	0	1	0	1	0	1	4455.46	40	433.79	40	171.12	28	472.15	28	21894.4	50
403	Min.	-55	0	1	0	1	0	1	-1848.22	19	-248.63	19	-219.2	7	-895.39	7	8717.42	25
403	Min.	-42	0	1	0	1	0	1	-1848.22	19	-248.63	19	-219.2	7	-895.39	7	8717.42	25
403	Min.	-41	0	1	0	1	0	1	-1848.22	19	-248.63	19	-219.2	7	-895.39	7	8717.42	25
403	Min.	-54	0	1	0	1	0	1	-1848.22	19	-248.63	19	-219.2	7	-895.39	7	8717.42	25
403	Max	-42	0	1	0	1	0	1	8372.16	51	720.49	50	147.39	28	272.41	34	11254.7	22
403	Max	-29	0	1	0	1	0	1	8372.16	51	720.49	50	147.39	28	272.41	34	11254.7	22
403	Max	-28	0	1	0	1	0	1	8372.16	51	720.49	50	147.39	28	272.41	34	11254.7	22
403	Max	-41	0	1	0	1	0	1	8372.16	51	720.49	50	147.39	28	272.41	34	11254.7	22
403	Min.	-42	0	1	0	1	0	1	2973.38	19	168.14	4	-172.05	7	-566.56	1	-3012.44	37
403	Min.	-29	0	1	0	1	0	1	2973.38	19	168.14	4	-172.05	7	-566.56	1	-3012.44	37
403	Min.	-28	0	1	0	1	0	1	2973.38	19	168.14	4	-172.05	7	-566.56	1	-3012.44	37
403	Min.	-41	0	1	0	1	0	1	2973.38	19	168.14	4	-172.05	7	-566.56	1	-3012.44	37
403	Max	-29	0	1	0	1	0	1	8372.16	52	720.49	50	172.05	34	272.41	7	3012.44	19
403	Max	-16	0	1	0	1	0	1	8372.16	52	720.49	50	172.05	34	272.41	7	3012.44	19
403	Max	-15	0	1	0	1	0	1	8372.16	52	720.49	50	172.05	34	272.41	7	3012.44	19
403	Max	-28	0	1	0	1	0	1	8372.16	52	720.49	50	172.05	34	272.41	7	3012.44	19
403	Min.	-29	0	1	0	1	0	1	2973.38	37	168.14	25	-147.39	1	-566.56	28	-11254.7	40
403	Min.	-16	0	1	0	1	0	1	2973.38	37	168.14	25	-147.39	1	-566.56	28	-11254.7	40
403	Min.	-15	0	1	0	1	0	1	2973.38	37	168.14	25	-147.39	1	-566.56	28	-11254.7	40
403	Min.	-28	0	1	0	1	0	1	2973.38	37	168.14	25	-147.39	1	-566.56	28	-11254.7	40
403	Max	-16	0	1	0	1	0	1	4455.46	22	433.79	22	219.2	34	472.15	1	-8717.42	4
403	Max	-3	0	1	0	1	0	1	4455.46	22	433.79	22	219.2	34	472.15	1	-8717.42	4
403	Max	-2	0	1	0	1	0	1	4455.46	22	433.79	22	219.2	34	472.15	1	-8717.42	4
403	Max	-15	0	1	0	1	0	1	4455.46	22	433.79	22	219.2	34	472.15	1	-8717.42	4
403	Min.	-16	0	1	0	1	0	1	-1848.22	37	-248.63	37	-171.12	1	-895.39	34	-21894.4	50
403	Min.	-3	0	1	0	1	0	1	-1848.22	37	-248.63	37	-171.12	1	-895.39	34	-21894.4	50
403	Min.	-2	0	1	0	1	0	1	-1848.22	37	-248.63	37	-171.12	1	-895.39	34	-21894.4	50
403	Min.	-15	0	1	0	1	0	1	-1848.22	37	-248.63	37	-171.12	1	-895.39	34	-21894.4	50
403	Max	-54	0	1	0	1	0	1	4543.75	40	199.63	40	68.68	28	528.88	28	23147.8	50
403	Max	-41	0	1	0	1	0	1	4543.75	40	199.63	40	68.68	28	528.88	28	23147.8	50
403	Max	-40	0	1	0	1	0	1	4543.75	40	199.63	40	68.68	28	528.88	28	23147.8	50
403	Max	-53	0	1	0	1	0	1	4543.75	40	199.63	40	68.68	28	528.88	28	23147.8	50
403	Min.	-54	0	1	0	1	0	1	-1885.42	19	-197.87	19	-312.99	7	-1485.55	7	8062.09	25
403	Min.	-41	0	1	0	1	0	1	-1885.42	19	-197.87	19	-312.99	7	-1485.55	7	8062.09	25
403	Min.	-40	0	1	0	1	0	1	-1885.42	19	-197.87	19	-312.99	7	-1485.55	7	8062.09	25
403	Min.	-53	0	1	0	1	0	1	-1885.42	19	-197.87	19	-312.99	7	-1485.55	7	8062.09	25
403	Max	-41	0	1	0	1	0	1	8486.63	51	368.12	50	98.54	25	-77.28	22	12174	22
403	Max	-28	0	1	0	1	0	1	8486.63	51	368.12	50	98.54	25	-77.28	22	12174	22
403	Max	-27	0	1	0	1	0	1	8486.63	51	368.12	50	98.54	25	-77.28	22	12174	22
403	Max	-40	0	1	0	1	0	1	8486.63	51	368.12	50	98.54	25	-77.28	22	12174	22
403	Min.	-41	0	1	0	1	0	1	2954.85	19	80.35	4	-228.16	10	-487.09	51	-3374.26	37
403	Min.	-28	0	1	0	1	0	1	2954.85	19	80.35	4	-228.16	10	-487.09	51	-3374.26	37
403	Min.	-27	0	1	0	1	0	1	2954.85	19	80.35	4	-228.16	10	-487.09	51	-3374.26	37
403	Min.	-40	0	1	0	1	0	1	2954.85	19	80.35	4	-228.16	10	-487.09	51	-3374.26	37
403	Max	-28	0	1	0	1	0	1	8486.63	52	368.12	50	228.16	31	-77.28	40	3374.26	19
403	Max	-15	0	1	0	1	0	1	8486.63	52	368.12	50	228.16	31	-77.28	40	3374.26	19
403	Max	-14	0	1	0	1	0	1	8486.63	52	368.12	50	228.16	31	-77.28	40	3374.26	19
403	Max	-27	0	1	0	1	0	1	8486.63	52	368.12	50	228.16	31	-77.28	40	3374.26	19
403	Min.	-28	0	1	0	1	0	1	2954.85	37	80.35	25	-98.54	4	-487.09	52	-12174	40
403	Min.	-15	0	1	0	1	0	1	2954.85	37	80.35	25	-98.54	4	-487.09	52	-12174	40
403	Min.	-14	0	1	0	1	0	1	2954.85	37	80.35	25	-98.54	4	-487.09	52	-12174	40
403	Min.	-27	0	1	0	1	0	1	2954.85	37	80.35	25	-98.54	4	-487.09	52	-12174	40
403	Max	-15	0	1	0	1	0	1	4543.75	22	199.63	22	312.99	34	528.88	1	-8062.09	4
403	Max	-2	0	1	0	1	0	1	4543.75	22	199.63	22	312.99	34	528.88	1	-8062.09	4
403	Max	-1	0	1	0	1	0	1	4543.75	22	199.63	22	312.99	34	528.88	1	-8062.09	4
403	Max	-14	0	1	0	1	0	1	4543.75	22	199.63	22	312.99	34	528.88	1	-8062.09	4
403	Min.	-15	0	1	0	1	0	1	-1885.42	37	-197.87	37	-68.68	1	-1485.55	34	-23147.8	50
403	Min.	-2	0	1	0	1	0	1	-1885.42	37	-197.87	37	-68.68	1	-1485.55	34	-23147.8	50
403	Min.	-1	0	1	0	1	0	1	-1885.42	37	-197.87	37	-68.68	1	-1485.55	34	-23147.8	50
403	Min.	-14	0	1	0	1	0	1	-1885.42	37	-197.87	37	-68.68	1	-1485.55	34	-23147.8	50
403	Max	-38	0	1	0	1	0	1	8372.16	52	720.49	49	147.39	31	566.56	10	3012.44	46
403	Max	-25	0	1	0	1	0	1	8372.16	52	720.49	49	147.39	31	566.56	10	3012.44	46
403	Max	-24	0	1	0	1	0	1	8372.16	52	720.49	49	147.39	31	566.56	10	3012.44	46
403	Max	-37	0	1	0	1	0	1	8372.16	52	720.49	49	147.39	31	566.56	10	3012.44	46
403	Min.	-38	0	1	0	1	0	1	2973.38	16	168.14	7	-172.05	4	-272.41	25	-11254.7	13
403	Min.	-25	0	1	0	1	0	1	2973.38	16	168.14	7	-172.05	4	-272.41	25	-11254.7	13
403	Min.	-24	0	1	0	1	0	1	2973.38	16	168.14	7	-172.05	4	-272.41	25	-11254.7	13
403	Min.	-37	0	1	0	1	0	1	2973.38	16	168.14	7	-172.05	4	-272.41	25	-11254.7	13
403	Max	-25	0	1	0	1	0	1	4455.46	43	433.79	43	171.12	31	895.39	4	-8717.42	34
403	Max	-12	0	1	0	1	0	1	4455.46	43	433.79	43	171.12	31	895.39	4	-8717.42	34
403	Max	-11	0	1	0	1	0	1	4455.46	43	433.79	43	171.12	31	895.39	4	-8717.42	34
403	Max	-24	0	1	0	1	0	1	4455.46	43	433.79	43	171.12	31	895.39	4	-8717.42	34
403	Min.	-25	0	1	0	1	0	1	-1848.22	16	-248.63	16	-219.2	4	-472.15	31	-21894.4	49
403	Min.	-12	0	1	0	1	0	1	-1848.22	16	-248.63	16	-219.2	4	-472.15	31	-21894.4	49
403	Min.	-11	0	1	0	1	0	1	-1848.22	16	-248.63	16	-219.2	4	-472.15	31	-218	

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403	Min.	-24	0	1	0	1	0	1	-1848.22	16	-248.63	16	-219.2	4	-472.15	31	-21894.4	49
403	Max	-63	0	1	0	1	0	1	4386	13	453.57	13	195.7	28	554.73	28	22317.4	49
403	Max	-50	0	1	0	1	0	1	4386	13	453.57	13	195.7	28	554.73	28	22317.4	49
403	Max	-49	0	1	0	1	0	1	4386	13	453.57	13	195.7	28	554.73	28	22317.4	49
403	Max	-62	0	1	0	1	0	1	4386	13	453.57	13	195.7	28	554.73	28	22317.4	49
403	Min.	-63	0	1	0	1	0	1	-1774.15	46	-197.37	46	-212.54	7	-518.34	7	9557.24	7
403	Min.	-50	0	1	0	1	0	1	-1774.15	46	-197.37	46	-212.54	7	-518.34	7	9557.24	7
403	Min.	-49	0	1	0	1	0	1	-1774.15	46	-197.37	46	-212.54	7	-518.34	7	9557.24	7
403	Min.	-62	0	1	0	1	0	1	-1774.15	46	-197.37	46	-212.54	7	-518.34	7	9557.24	7
403	Max	-32	0	1	0	1	0	1	8386.15	52	845.62	52	162.55	31	624.68	10	2628.1	19
403	Max	-19	0	1	0	1	0	1	8386.15	52	845.62	52	162.55	31	624.68	10	2628.1	19
403	Max	-18	0	1	0	1	0	1	8386.15	52	845.62	52	162.55	31	624.68	10	2628.1	19
403	Max	-31	0	1	0	1	0	1	8386.15	52	845.62	52	162.55	31	624.68	10	2628.1	19
403	Min.	-32	0	1	0	1	0	1	3237	37	319.7	37	-166.09	4	-634.35	25	-11124.5	40
403	Min.	-19	0	1	0	1	0	1	3237	37	319.7	37	-166.09	4	-634.35	25	-11124.5	40
403	Min.	-18	0	1	0	1	0	1	3237	37	319.7	37	-166.09	4	-634.35	25	-11124.5	40
403	Min.	-31	0	1	0	1	0	1	3237	37	319.7	37	-166.09	4	-634.35	25	-11124.5	40
403	Max	-37	0	1	0	1	0	1	8355.44	52	830.51	49	162.43	31	621.28	7	2984.09	46
403	Max	-24	0	1	0	1	0	1	8355.44	52	830.51	49	162.43	31	621.28	7	2984.09	46
403	Max	-23	0	1	0	1	0	1	8355.44	52	830.51	49	162.43	31	621.28	7	2984.09	46
403	Max	-36	0	1	0	1	0	1	8355.44	52	830.51	49	162.43	31	621.28	7	2984.09	46
403	Min.	-37	0	1	0	1	0	1	3037.67	16	251.45	7	-156.33	4	-510.51	28	-11475.9	13
403	Min.	-24	0	1	0	1	0	1	3037.67	16	251.45	7	-156.33	4	-510.51	28	-11475.9	13
403	Min.	-23	0	1	0	1	0	1	3037.67	16	251.45	7	-156.33	4	-510.51	28	-11475.9	13
403	Min.	-36	0	1	0	1	0	1	3037.67	16	251.45	7	-156.33	4	-510.51	28	-11475.9	13
403	Max	-24	0	1	0	1	0	1	4386	43	453.57	43	212.54	34	554.73	1	-9557.24	34
403	Max	-11	0	1	0	1	0	1	4386	43	453.57	43	212.54	34	554.73	1	-9557.24	34
403	Max	-10	0	1	0	1	0	1	4386	43	453.57	43	212.54	34	554.73	1	-9557.24	34
403	Max	-23	0	1	0	1	0	1	4386	43	453.57	43	212.54	34	554.73	1	-9557.24	34
403	Min.	-24	0	1	0	1	0	1	-1774.15	16	-197.37	16	-195.7	1	-518.34	34	-22317.4	49
403	Min.	-11	0	1	0	1	0	1	-1774.15	16	-197.37	16	-195.7	1	-518.34	34	-22317.4	49
403	Min.	-10	0	1	0	1	0	1	-1774.15	16	-197.37	16	-195.7	1	-518.34	34	-22317.4	49
403	Min.	-23	0	1	0	1	0	1	-1774.15	16	-197.37	16	-195.7	1	-518.34	34	-22317.4	49
403	Max	-62	0	1	0	1	0	1	4324.17	13	443.75	13	211.83	25	523.17	25	22332.2	49
403	Max	-49	0	1	0	1	0	1	4324.17	13	443.75	13	211.83	25	523.17	25	22332.2	49
403	Max	-48	0	1	0	1	0	1	4324.17	13	443.75	13	211.83	25	523.17	25	22332.2	49
403	Max	-61	0	1	0	1	0	1	4324.17	13	443.75	13	211.83	25	523.17	25	22332.2	49
403	Min.	-62	0	1	0	1	0	1	-1706.98	46	-175.65	46	-224.04	10	-556.4	10	10377.1	7
403	Min.	-49	0	1	0	1	0	1	-1706.98	46	-175.65	46	-224.04	10	-556.4	10	10377.1	7
403	Min.	-48	0	1	0	1	0	1	-1706.98	46	-175.65	46	-224.04	10	-556.4	10	10377.1	7
403	Min.	-61	0	1	0	1	0	1	-1706.98	46	-175.65	46	-224.04	10	-556.4	10	10377.1	7
403	Max	-49	0	1	0	1	0	1	8374.61	51	846.27	51	159.77	28	634.53	31	11259.8	43
403	Max	-36	0	1	0	1	0	1	8374.61	51	846.27	51	159.77	28	634.53	31	11259.8	43
403	Max	-35	0	1	0	1	0	1	8374.61	51	846.27	51	159.77	28	634.53	31	11259.8	43
403	Max	-48	0	1	0	1	0	1	8374.61	51	846.27	51	159.77	28	634.53	31	11259.8	43
403	Min.	-49	0	1	0	1	0	1	3136.24	46	304.89	46	-166.63	7	-594.41	4	-2790.87	16
403	Min.	-36	0	1	0	1	0	1	3136.24	46	304.89	46	-166.63	7	-594.41	4	-2790.87	16
403	Min.	-35	0	1	0	1	0	1	3136.24	46	304.89	46	-166.63	7	-594.41	4	-2790.87	16
403	Min.	-48	0	1	0	1	0	1	3136.24	46	304.89	46	-166.63	7	-594.41	4	-2790.87	16
403	Max	-36	0	1	0	1	0	1	8374.61	52	846.27	52	166.63	34	634.53	10	2790.87	46
403	Max	-23	0	1	0	1	0	1	8374.61	52	846.27	52	166.63	34	634.53	10	2790.87	46
403	Max	-22	0	1	0	1	0	1	8374.61	52	846.27	52	166.63	34	634.53	10	2790.87	46
403	Max	-35	0	1	0	1	0	1	8374.61	52	846.27	52	166.63	34	634.53	10	2790.87	46
403	Min.	-36	0	1	0	1	0	1	3136.24	16	304.89	16	-159.77	1	-594.41	25	-11259.8	13
403	Min.	-23	0	1	0	1	0	1	3136.24	16	304.89	16	-159.77	1	-594.41	25	-11259.8	13
403	Min.	-22	0	1	0	1	0	1	3136.24	16	304.89	16	-159.77	1	-594.41	25	-11259.8	13
403	Min.	-35	0	1	0	1	0	1	3136.24	16	304.89	16	-159.77	1	-594.41	25	-11259.8	13
403	Max	-23	0	1	0	1	0	1	4324.17	43	443.75	43	224.04	31	523.17	4	-10377.1	34
403	Max	-10	0	1	0	1	0	1	4324.17	43	443.75	43	224.04	31	523.17	4	-10377.1	34
403	Max	-9	0	1	0	1	0	1	4324.17	43	443.75	43	224.04	31	523.17	4	-10377.1	34
403	Max	-22	0	1	0	1	0	1	4324.17	43	443.75	43	224.04	31	523.17	4	-10377.1	34
403	Min.	-23	0	1	0	1	0	1	-1706.98	16	-175.65	16	-211.83	4	-556.4	31	-22332.2	49
403	Min.	-10	0	1	0	1	0	1	-1706.98	16	-175.65	16	-211.83	4	-556.4	31	-22332.2	49
403	Min.	-9	0	1	0	1	0	1	-1706.98	16	-175.65	16	-211.83	4	-556.4	31	-22332.2	49
403	Min.	-22	0	1	0	1	0	1	-1706.98	16	-175.65	16	-211.83	4	-556.4	31	-22332.2	49
403	Max	-61	0	1	0	1	0	1	4254.81	13	432.6	13	221.04	28	540.46	25	22339.7	49
403	Max	-48	0	1	0	1	0	1	4254.81	13	432.6	13	221.04	28	540.46	25	22339.7	49
403	Max	-47	0	1	0	1	0	1	4254.81	13	432.6	13	221.04	28	540.46	25	22339.7	49
403	Max	-60	0	1	0	1	0	1	4254.81	13	432.6	13	221.04	28	540.46	25	22339.7	49
403	Min.	-61	0	1	0	1	0	1	-1634.38	46	-166.78	46	-227.98	7	-560.93	10	11222.2	7
403	Min.	-48	0	1	0	1	0	1	-1634.38	46	-166.78	46	-227.98	7	-560.93	10	11222.2	7
403	Min.	-47	0	1	0	1	0	1	-1634.38	46	-166.78	46	-227.98	7	-560.93	10	11222.2	7
403	Min.	-60	0	1	0	1	0	1	-1634.38	46	-166.78	46	-227.98	7	-560.93	10	11222.2	7
403	Max	-48	0	1	0	1	0	1	8386.15	51	845.62	51	162.55	28	634.35	34	11124.5	43
403	Max	-35	0	1	0	1	0	1	8386.15	51	845.62	51	162.55	28	634.35	34	11124.5	43
403	Max	-34	0	1	0	1	0	1	8386.15	51	845.62	51	162.55	28	634.35	34	11124.5	43
403	Max	-47	0	1	0	1	0	1	8386.15	51	845.62	51	162.55	28	634.35	34	11124.5	43
403	Min.	-48	0	1	0	1	0	1	3237	46	319.7	46	-166.09	7	-624.68	1	-2628.1	16
403	Min.	-35	0	1	0	1	0	1	3237	46	319.7	46	-166.09	7	-624.68	1	-2628.1	16
403	Min.	-34	0	1	0	1	0	1	3237	46	319.7	46	-166.09	7	-624.68	1	-2628.1	16
403	Min.	-47	0	1	0	1	0	1	3237	46	319.7	46	-166.09	7	-624.68	1	-2628.1	16

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403	Max	-35	0	1	0	1	0	1	8386.15	52	845.62	52	166.09	34	634.35	7	2628.1	46
403	Max	-22	0	1	0	1	0	1	8386.15	52	845.62	52	166.09	34	634.35	7	2628.1	46
403	Max	-21	0	1	0	1	0	1	8386.15	52	845.62	52	166.09	34	634.35	7	2628.1	46
403	Max	-34	0	1	0	1	0	1	8386.15	52	845.62	52	166.09	34	634.35	7	2628.1	46
403	Min.	-35	0	1	0	1	0	1	3237	16	319.7	16	-162.55	1	-624.68	28	-11124.5	13
403	Min.	-22	0	1	0	1	0	1	3237	16	319.7	16	-162.55	1	-624.68	28	-11124.5	13
403	Min.	-21	0	1	0	1	0	1	3237	16	319.7	16	-162.55	1	-624.68	28	-11124.5	13
403	Min.	-34	0	1	0	1	0	1	3237	16	319.7	16	-162.55	1	-624.68	28	-11124.5	13
403	Max	-22	0	1	0	1	0	1	4254.81	43	432.6	43	227.98	34	540.46	4	-11222.2	34
403	Max	-9	0	1	0	1	0	1	4254.81	43	432.6	43	227.98	34	540.46	4	-11222.2	34
403	Max	-8	0	1	0	1	0	1	4254.81	43	432.6	43	227.98	34	540.46	4	-11222.2	34
403	Max	-21	0	1	0	1	0	1	4254.81	43	432.6	43	227.98	34	540.46	4	-11222.2	34
403	Min.	-22	0	1	0	1	0	1	-1634.38	16	-166.78	16	-221.04	1	-560.93	31	-22339.7	49
403	Min.	-9	0	1	0	1	0	1	-1634.38	16	-166.78	16	-221.04	1	-560.93	31	-22339.7	49
403	Min.	-8	0	1	0	1	0	1	-1634.38	16	-166.78	16	-221.04	1	-560.93	31	-22339.7	49
403	Min.	-21	0	1	0	1	0	1	-1634.38	16	-166.78	16	-221.04	1	-560.93	31	-22339.7	49
403	Max	-60	0	1	0	1	0	1	4186.53	13	421.4	13	225.75	28	551.39	25	22336.8	52
403	Max	-47	0	1	0	1	0	1	4186.53	13	421.4	13	225.75	28	551.39	25	22336.8	52
403	Max	-46	0	1	0	1	0	1	4186.53	13	421.4	13	225.75	28	551.39	25	22336.8	52
403	Max	-59	0	1	0	1	0	1	4186.53	13	421.4	13	225.75	28	551.39	25	22336.8	52
403	Min.	-60	0	1	0	1	0	1	-1564.22	46	-157.01	46	-227.56	7	-558.09	10	11687.8	16
403	Min.	-47	0	1	0	1	0	1	-1564.22	46	-157.01	46	-227.56	7	-558.09	10	11687.8	16
403	Min.	-46	0	1	0	1	0	1	-1564.22	46	-157.01	46	-227.56	7	-558.09	10	11687.8	16
403	Min.	-59	0	1	0	1	0	1	-1564.22	46	-157.01	46	-227.56	7	-558.09	10	11687.8	16
403	Max	-47	0	1	0	1	0	1	8391.11	51	843.03	51	164.09	28	633.49	31	10968.4	43
403	Max	-34	0	1	0	1	0	1	8391.11	51	843.03	51	164.09	28	633.49	31	10968.4	43
403	Max	-33	0	1	0	1	0	1	8391.11	51	843.03	51	164.09	28	633.49	31	10968.4	43
403	Max	-46	0	1	0	1	0	1	8391.11	51	843.03	51	164.09	28	633.49	31	10968.4	43
403	Min.	-47	0	1	0	1	0	1	3335.73	46	333.31	46	-165.05	7	-631.27	4	-2470.5	16
403	Min.	-34	0	1	0	1	0	1	3335.73	46	333.31	46	-165.05	7	-631.27	4	-2470.5	16
403	Min.	-33	0	1	0	1	0	1	3335.73	46	333.31	46	-165.05	7	-631.27	4	-2470.5	16
403	Min.	-46	0	1	0	1	0	1	3335.73	46	333.31	46	-165.05	7	-631.27	4	-2470.5	16
403	Max	-34	0	1	0	1	0	1	8391.11	52	843.03	52	165.05	34	633.49	10	2470.5	46
403	Max	-21	0	1	0	1	0	1	8391.11	52	843.03	52	165.05	34	633.49	10	2470.5	46
403	Max	-20	0	1	0	1	0	1	8391.11	52	843.03	52	165.05	34	633.49	10	2470.5	46
403	Max	-33	0	1	0	1	0	1	8391.11	52	843.03	52	165.05	34	633.49	10	2470.5	46
403	Min.	-34	0	1	0	1	0	1	3335.73	16	333.31	16	-164.09	1	-631.27	25	-10968.4	13
403	Min.	-21	0	1	0	1	0	1	3335.73	16	333.31	16	-164.09	1	-631.27	25	-10968.4	13
403	Min.	-20	0	1	0	1	0	1	3335.73	16	333.31	16	-164.09	1	-631.27	25	-10968.4	13
403	Min.	-33	0	1	0	1	0	1	3335.73	16	333.31	16	-164.09	1	-631.27	25	-10968.4	13
403	Max	-21	0	1	0	1	0	1	4186.53	43	421.4	43	227.56	34	551.39	4	-11687.8	46
403	Max	-8	0	1	0	1	0	1	4186.53	43	421.4	43	227.56	34	551.39	4	-11687.8	46
403	Max	-7	0	1	0	1	0	1	4186.53	43	421.4	43	227.56	34	551.39	4	-11687.8	46
403	Max	-20	0	1	0	1	0	1	4186.53	43	421.4	43	227.56	34	551.39	4	-11687.8	46
403	Min.	-21	0	1	0	1	0	1	-1564.22	16	-157.01	16	-225.75	1	-558.09	31	-22336.8	51
403	Min.	-8	0	1	0	1	0	1	-1564.22	16	-157.01	16	-225.75	1	-558.09	31	-22336.8	51
403	Min.	-7	0	1	0	1	0	1	-1564.22	16	-157.01	16	-225.75	1	-558.09	31	-22336.8	51
403	Min.	-20	0	1	0	1	0	1	-1564.22	16	-157.01	16	-225.75	1	-558.09	31	-22336.8	51
403	Max	-59	0	1	0	1	0	1	4186.53	40	421.4	40	227.56	25	558.09	28	22336.8	52
403	Max	-46	0	1	0	1	0	1	4186.53	40	421.4	40	227.56	25	558.09	28	22336.8	52
403	Max	-45	0	1	0	1	0	1	4186.53	40	421.4	40	227.56	25	558.09	28	22336.8	52
403	Max	-58	0	1	0	1	0	1	4186.53	40	421.4	40	227.56	25	558.09	28	22336.8	52
403	Min.	-59	0	1	0	1	0	1	-1564.22	19	-157.01	19	-225.75	10	-551.39	7	11687.8	37
403	Min.	-46	0	1	0	1	0	1	-1564.22	19	-157.01	19	-225.75	10	-551.39	7	11687.8	37
403	Min.	-45	0	1	0	1	0	1	-1564.22	19	-157.01	19	-225.75	10	-551.39	7	11687.8	37
403	Min.	-58	0	1	0	1	0	1	-1564.22	19	-157.01	19	-225.75	10	-551.39	7	11687.8	37
403	Max	-46	0	1	0	1	0	1	8391.11	51	843.03	51	165.05	25	631.27	34	10968.4	22
403	Max	-33	0	1	0	1	0	1	8391.11	51	843.03	51	165.05	25	631.27	34	10968.4	22
403	Max	-32	0	1	0	1	0	1	8391.11	51	843.03	51	165.05	25	631.27	34	10968.4	22
403	Max	-45	0	1	0	1	0	1	8391.11	51	843.03	51	165.05	25	631.27	34	10968.4	22
403	Min.	-46	0	1	0	1	0	1	3335.73	19	333.31	19	-164.09	10	-633.49	1	-2470.5	37
403	Min.	-33	0	1	0	1	0	1	3335.73	19	333.31	19	-164.09	10	-633.49	1	-2470.5	37
403	Min.	-32	0	1	0	1	0	1	3335.73	19	333.31	19	-164.09	10	-633.49	1	-2470.5	37
403	Min.	-45	0	1	0	1	0	1	3335.73	19	333.31	19	-164.09	10	-633.49	1	-2470.5	37
403	Max	-33	0	1	0	1	0	1	8391.11	52	843.03	52	164.09	31	631.27	7	2470.5	19
403	Max	-20	0	1	0	1	0	1	8391.11	52	843.03	52	164.09	31	631.27	7	2470.5	19
403	Max	-19	0	1	0	1	0	1	8391.11	52	843.03	52	164.09	31	631.27	7	2470.5	19
403	Max	-32	0	1	0	1	0	1	8391.11	52	843.03	52	164.09	31	631.27	7	2470.5	19
403	Min.	-33	0	1	0	1	0	1	3335.73	37	333.31	37	-165.05	4	-633.49	28	-10968.4	40
403	Min.	-20	0	1	0	1	0	1	3335.73	37	333.31	37	-165.05	4	-633.49	28	-10968.4	40
403	Min.	-19	0	1	0	1	0	1	3335.73	37	333.31	37	-165.05	4	-633.49	28	-10968.4	40
403	Min.	-32	0	1	0	1	0	1	3335.73	37	333.31	37	-165.05	4	-633.49	28	-10968.4	40
403	Max	-20	0	1	0	1	0	1	4186.53	22	421.4	22	225.75	31	558.09	1	-11687.8	19
403	Max	-7	0	1	0	1	0	1	4186.53	22	421.4	22	225.75	31	558.09	1	-11687.8	19
403	Max	-6	0	1	0	1	0	1	4186.53	22	421.4	22	225.75	31	558.09	1	-11687.8	19
403	Max	-19	0	1	0	1	0	1	4186.53	22	421.4	22	225.75	31	558.09	1	-11687.8	19
403	Min.	-20	0	1	0	1	0	1	-1564.22	37	-157.01	37	-227.56	4	-551.39	34	-22336.8	51
403	Min.	-7	0	1	0	1	0	1	-1564.22	37	-157.01	37	-227.56	4	-551.39	34	-22336.8	51
403	Min.	-6	0	1	0	1	0	1	-1564.22	37	-157.01	37	-227.56	4	-551.39	34	-22336.8	51
403	Min.	-19	0	1	0	1	0	1	-1564.22	37	-157.01	37	-227.56	4	-551.39	34	-22336.8	51
403	Max	-58	0	1	0	1	0	1	4254.81	40	432.6	40	227.98	25	560.93			

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403	Max	-45	0	1	0	1	0	1	4254.81	40	432.6	40	227.98	25	560.93	28	22339.7	50
403	Max	-44	0	1	0	1	0	1	4254.81	40	432.6	40	227.98	25	560.93	28	22339.7	50
403	Max	-57	0	1	0	1	0	1	4254.81	40	432.6	40	227.98	25	560.93	28	22339.7	50
403	Min.	-58	0	1	0	1	0	1	-1634.38	19	-166.78	19	-221.04	10	-540.46	7	11222.2	25
403	Min.	-45	0	1	0	1	0	1	-1634.38	19	-166.78	19	-221.04	10	-540.46	7	11222.2	25
403	Min.	-44	0	1	0	1	0	1	-1634.38	19	-166.78	19	-221.04	10	-540.46	7	11222.2	25
403	Min.	-57	0	1	0	1	0	1	-1634.38	19	-166.78	19	-221.04	10	-540.46	7	11222.2	25
403	Max	-45	0	1	0	1	0	1	8386.15	51	845.62	51	166.09	25	624.68	31	11124.5	22
403	Max	-32	0	1	0	1	0	1	8386.15	51	845.62	51	166.09	25	624.68	31	11124.5	22
403	Max	-31	0	1	0	1	0	1	8386.15	51	845.62	51	166.09	25	624.68	31	11124.5	22
403	Max	-44	0	1	0	1	0	1	8386.15	51	845.62	51	166.09	25	624.68	31	11124.5	22
403	Min.	-45	0	1	0	1	0	1	3237	19	319.7	19	-162.55	10	-634.35	4	-2628.1	37
403	Min.	-32	0	1	0	1	0	1	3237	19	319.7	19	-162.55	10	-634.35	4	-2628.1	37
403	Min.	-31	0	1	0	1	0	1	3237	19	319.7	19	-162.55	10	-634.35	4	-2628.1	37
403	Min.	-44	0	1	0	1	0	1	3237	19	319.7	19	-162.55	10	-634.35	4	-2628.1	37
403	Max	-18	0	1	0	1	0	1	4324.17	22	443.75	22	211.83	34	556.4	1	-10377.1	4
403	Max	-5	0	1	0	1	0	1	4324.17	22	443.75	22	211.83	34	556.4	1	-10377.1	4
403	Max	-4	0	1	0	1	0	1	4324.17	22	443.75	22	211.83	34	556.4	1	-10377.1	4
403	Max	-17	0	1	0	1	0	1	4324.17	22	443.75	22	211.83	34	556.4	1	-10377.1	4
403	Min.	-18	0	1	0	1	0	1	-1706.98	37	-175.65	37	-224.04	1	-523.17	34	-22332.2	50
403	Min.	-5	0	1	0	1	0	1	-1706.98	37	-175.65	37	-224.04	1	-523.17	34	-22332.2	50
403	Min.	-4	0	1	0	1	0	1	-1706.98	37	-175.65	37	-224.04	1	-523.17	34	-22332.2	50
403	Min.	-17	0	1	0	1	0	1	-1706.98	37	-175.65	37	-224.04	1	-523.17	34	-22332.2	50
403	Max	-19	0	1	0	1	0	1	4254.81	22	432.6	22	221.04	31	560.93	1	-11222.2	4
403	Max	-6	0	1	0	1	0	1	4254.81	22	432.6	22	221.04	31	560.93	1	-11222.2	4
403	Max	-5	0	1	0	1	0	1	4254.81	22	432.6	22	221.04	31	560.93	1	-11222.2	4
403	Max	-18	0	1	0	1	0	1	4254.81	22	432.6	22	221.04	31	560.93	1	-11222.2	4
403	Min.	-19	0	1	0	1	0	1	-1634.38	37	-166.78	37	-227.98	4	-540.46	34	-22339.7	50
403	Min.	-6	0	1	0	1	0	1	-1634.38	37	-166.78	37	-227.98	4	-540.46	34	-22339.7	50
403	Min.	-5	0	1	0	1	0	1	-1634.38	37	-166.78	37	-227.98	4	-540.46	34	-22339.7	50
403	Min.	-18	0	1	0	1	0	1	-1634.38	37	-166.78	37	-227.98	4	-540.46	34	-22339.7	50
403	Max	-57	0	1	0	1	0	1	4324.17	40	443.75	40	224.04	28	556.4	28	22332.2	50
403	Max	-44	0	1	0	1	0	1	4324.17	40	443.75	40	224.04	28	556.4	28	22332.2	50
403	Max	-43	0	1	0	1	0	1	4324.17	40	443.75	40	224.04	28	556.4	28	22332.2	50
403	Max	-56	0	1	0	1	0	1	4324.17	40	443.75	40	224.04	28	556.4	28	22332.2	50
403	Min.	-57	0	1	0	1	0	1	-1706.98	19	-175.65	19	-211.83	7	-523.17	7	10377.1	25
403	Min.	-44	0	1	0	1	0	1	-1706.98	19	-175.65	19	-211.83	7	-523.17	7	10377.1	25
403	Min.	-43	0	1	0	1	0	1	-1706.98	19	-175.65	19	-211.83	7	-523.17	7	10377.1	25
403	Min.	-56	0	1	0	1	0	1	-1706.98	19	-175.65	19	-211.83	7	-523.17	7	10377.1	25
403	Max	-44	0	1	0	1	0	1	8374.61	51	846.27	51	166.63	25	594.41	34	11259.8	22
403	Max	-31	0	1	0	1	0	1	8374.61	51	846.27	51	166.63	25	594.41	34	11259.8	22
403	Max	-30	0	1	0	1	0	1	8374.61	51	846.27	51	166.63	25	594.41	34	11259.8	22
403	Max	-43	0	1	0	1	0	1	8374.61	51	846.27	51	166.63	25	594.41	34	11259.8	22
403	Min.	-44	0	1	0	1	0	1	3136.24	19	304.89	19	-159.77	10	-634.53	1	-2790.87	37
403	Min.	-31	0	1	0	1	0	1	3136.24	19	304.89	19	-159.77	10	-634.53	1	-2790.87	37
403	Min.	-30	0	1	0	1	0	1	3136.24	19	304.89	19	-159.77	10	-634.53	1	-2790.87	37
403	Min.	-43	0	1	0	1	0	1	3136.24	19	304.89	19	-159.77	10	-634.53	1	-2790.87	37
403	Max	-31	0	1	0	1	0	1	8374.61	52	846.27	52	159.77	31	594.41	7	2790.87	19
403	Max	-18	0	1	0	1	0	1	8374.61	52	846.27	52	159.77	31	594.41	7	2790.87	19
403	Max	-17	0	1	0	1	0	1	8374.61	52	846.27	52	159.77	31	594.41	7	2790.87	19
403	Max	-30	0	1	0	1	0	1	8374.61	52	846.27	52	159.77	31	594.41	7	2790.87	19
403	Min.	-31	0	1	0	1	0	1	3136.24	37	304.89	37	-166.63	4	-634.53	28	-11259.8	40
403	Min.	-18	0	1	0	1	0	1	3136.24	37	304.89	37	-166.63	4	-634.53	28	-11259.8	40
403	Min.	-17	0	1	0	1	0	1	3136.24	37	304.89	37	-166.63	4	-634.53	28	-11259.8	40
403	Min.	-30	0	1	0	1	0	1	3136.24	37	304.89	37	-166.63	4	-634.53	28	-11259.8	40
403	Max	-26	0	1	0	1	0	1	4543.75	43	199.63	43	68.68	31	1485.55	4	-8062.09	34
403	Max	-13	0	1	0	1	0	1	4543.75	43	199.63	43	68.68	31	1485.55	4	-8062.09	34
403	Max	-12	0	1	0	1	0	1	4543.75	43	199.63	43	68.68	31	1485.55	4	-8062.09	34
403	Max	-25	0	1	0	1	0	1	4543.75	43	199.63	43	68.68	31	1485.55	4	-8062.09	34
403	Min.	-26	0	1	0	1	0	1	-1885.42	16	-197.87	16	-312.99	4	-528.88	31	-23147.8	49
403	Min.	-13	0	1	0	1	0	1	-1885.42	16	-197.87	16	-312.99	4	-528.88	31	-23147.8	49
403	Min.	-12	0	1	0	1	0	1	-1885.42	16	-197.87	16	-312.99	4	-528.88	31	-23147.8	49
403	Min.	-25	0	1	0	1	0	1	-1885.42	16	-197.87	16	-312.99	4	-528.88	31	-23147.8	49
403	Max	-56	0	1	0	1	0	1	4386	40	453.57	40	212.54	25	518.34	25	22317.4	50
403	Max	-43	0	1	0	1	0	1	4386	40	453.57	40	212.54	25	518.34	25	22317.4	50
403	Max	-42	0	1	0	1	0	1	4386	40	453.57	40	212.54	25	518.34	25	22317.4	50
403	Max	-55	0	1	0	1	0	1	4386	40	453.57	40	212.54	25	518.34	25	22317.4	50
403	Min.	-56	0	1	0	1	0	1	-1774.15	19	-197.37	19	-195.7	10	-554.73	10	9557.24	25
403	Min.	-43	0	1	0	1	0	1	-1774.15	19	-197.37	19	-195.7	10	-554.73	10	9557.24	25
403	Min.	-42	0	1	0	1	0	1	-1774.15	19	-197.37	19	-195.7	10	-554.73	10	9557.24	25
403	Min.	-55	0	1	0	1	0	1	-1774.15	19	-197.37	19	-195.7	10	-554.73	10	9557.24	25
403	Max	-43	0	1	0	1	0	1	8355.44	51	830.51	50	162.43	28	510.51	31	11475.9	22
403	Max	-30	0	1	0	1	0	1	8355.44	51	830.51	50	162.43	28	510.51	31	11475.9	22
403	Max	-29	0	1	0	1	0	1	8355.44	51	830.51	50	162.43	28	510.51	31	11475.9	22
403	Max	-42	0	1	0	1	0	1	8355.44	51	830.51	50	162.43	28	510.51	31	11475.9	22
403	Min.	-43	0	1	0	1	0	1	3037.67	19	251.45	4	-156.33	7	-621.28	4	-2984.09	37
403	Min.	-30	0	1	0	1	0	1	3037.67	19	251.45	4	-156.33	7	-621.28	4	-2984.09	37
403	Min.	-29	0	1	0	1	0	1	3037.67	19	251.45	4	-156.33	7	-621.28	4	-2984.09	37
403	Min.	-42	0	1	0	1	0	1	3037.67	19	251.45	4	-156.33	7	-621.28	4	-2984.09	37
403	Max	-52	0	1	0	1	0	1	8486.63	51	368.12	49	228.16	28	487.09	51	12174	43
403	Max	-39	0	1	0	1	0	1	8486.63	51	368.12	49	228.16	28	487.09			

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403	Max	-38	0	1	0	1	0	1	8486.63	51	368.12	49	228.16	28	487.09	51	12174	43
403	Max	-51	0	1	0	1	0	1	8486.63	51	368.12	49	228.16	28	487.09	51	12174	43
403	Min.	-52	0	1	0	1	0	1	2954.85	46	80.35	34	-98.54	7	77.28	43	-3374.26	16
403	Min.	-39	0	1	0	1	0	1	2954.85	46	80.35	34	-98.54	7	77.28	43	-3374.26	16
403	Min.	-38	0	1	0	1	0	1	2954.85	46	80.35	34	-98.54	7	77.28	43	-3374.26	16
403	Min.	-51	0	1	0	1	0	1	2954.85	46	80.35	34	-98.54	7	77.28	43	-3374.26	16
403	Max	-39	0	1	0	1	0	1	8486.63	52	368.12	49	98.54	34	487.09	52	3374.26	46
403	Max	-26	0	1	0	1	0	1	8486.63	52	368.12	49	98.54	34	487.09	52	3374.26	46
403	Max	-25	0	1	0	1	0	1	8486.63	52	368.12	49	98.54	34	487.09	52	3374.26	46
403	Max	-38	0	1	0	1	0	1	8486.63	52	368.12	49	98.54	34	487.09	52	3374.26	46
403	Min.	-39	0	1	0	1	0	1	2954.85	16	80.35	7	-228.16	1	77.28	13	-12174	13
403	Min.	-26	0	1	0	1	0	1	2954.85	16	80.35	7	-228.16	1	77.28	13	-12174	13
403	Min.	-25	0	1	0	1	0	1	2954.85	16	80.35	7	-228.16	1	77.28	13	-12174	13
403	Min.	-38	0	1	0	1	0	1	2954.85	16	80.35	7	-228.16	1	77.28	13	-12174	13
403	Max	-51	0	1	0	1	0	1	8372.16	51	720.49	49	172.05	25	566.56	31	11254.7	43
403	Max	-38	0	1	0	1	0	1	8372.16	51	720.49	49	172.05	25	566.56	31	11254.7	43
403	Max	-37	0	1	0	1	0	1	8372.16	51	720.49	49	172.05	25	566.56	31	11254.7	43
403	Max	-50	0	1	0	1	0	1	8372.16	51	720.49	49	172.05	25	566.56	31	11254.7	43
403	Min.	-51	0	1	0	1	0	1	2973.38	46	168.14	34	-147.39	10	-272.41	4	-3012.44	16
403	Min.	-38	0	1	0	1	0	1	2973.38	46	168.14	34	-147.39	10	-272.41	4	-3012.44	16
403	Min.	-37	0	1	0	1	0	1	2973.38	46	168.14	34	-147.39	10	-272.41	4	-3012.44	16
403	Min.	-50	0	1	0	1	0	1	2973.38	46	168.14	34	-147.39	10	-272.41	4	-3012.44	16
403	Max	-64	0	1	0	1	0	1	4455.46	13	433.79	13	219.2	25	895.39	25	21894.4	49
403	Max	-51	0	1	0	1	0	1	4455.46	13	433.79	13	219.2	25	895.39	25	21894.4	49
403	Max	-50	0	1	0	1	0	1	4455.46	13	433.79	13	219.2	25	895.39	25	21894.4	49
403	Max	-63	0	1	0	1	0	1	4455.46	13	433.79	13	219.2	25	895.39	25	21894.4	49
403	Min.	-64	0	1	0	1	0	1	-1848.22	46	-248.63	46	-171.12	10	-472.15	10	8717.42	7
403	Min.	-51	0	1	0	1	0	1	-1848.22	46	-248.63	46	-171.12	10	-472.15	10	8717.42	7
403	Min.	-50	0	1	0	1	0	1	-1848.22	46	-248.63	46	-171.12	10	-472.15	10	8717.42	7
403	Min.	-63	0	1	0	1	0	1	-1848.22	46	-248.63	46	-171.12	10	-472.15	10	8717.42	7
404	Max	-170	0	13	0	13	0	13	153.43	40	1393.16	37	-49.83	22	-5799.91	22	186.89	16
404	Max	-171	0	13	0	13	0	13	153.43	40	1393.16	37	-49.83	22	-5799.91	22	186.89	16
404	Max	-158	0	13	0	13	0	13	153.43	40	1393.16	37	-49.83	22	-5799.91	22	186.89	16
404	Max	-157	0	13	0	13	0	13	153.43	40	1393.16	37	-49.83	22	-5799.91	22	186.89	16
404	Min.	-170	0	43	0	43	0	46	-173.8	19	-3871.56	22	-192.75	51	-19410.3	51	-1034.67	43
404	Min.	-171	0	43	0	43	0	46	-173.8	19	-3871.56	22	-192.75	51	-19410.3	51	-1034.67	43
404	Min.	-158	0	43	0	43	0	46	-173.8	19	-3871.56	22	-192.75	51	-19410.3	51	-1034.67	43
404	Min.	-157	0	43	0	43	0	46	-173.8	19	-3871.56	22	-192.75	51	-19410.3	51	-1034.67	43
404	Max	-138	0	51	0	51	0	40	117.87	43	1178.91	46	69.58	10	18813.2	52	258.97	25
404	Max	-139	0	51	0	51	0	40	117.87	43	1178.91	46	69.58	10	18813.2	52	258.97	25
404	Max	-126	0	51	0	51	0	40	117.87	43	1178.91	46	69.58	10	18813.2	52	258.97	25
404	Max	-125	0	51	0	51	0	40	117.87	43	1178.91	46	69.58	10	18813.2	52	258.97	25
404	Min.	-138	0	52	0	52	0	19	-365.23	16	-3619.78	13	-63.65	25	5985.29	16	-277.5	10
404	Min.	-139	0	52	0	52	0	19	-365.23	16	-3619.78	13	-63.65	25	5985.29	16	-277.5	10
404	Min.	-126	0	52	0	52	0	19	-365.23	16	-3619.78	13	-63.65	25	5985.29	16	-277.5	10
404	Min.	-125	0	52	0	52	0	19	-365.23	16	-3619.78	13	-63.65	25	5985.29	16	-277.5	10
404	Max	-139	0	25	0	25	0	7	122.39	43	1241.34	46	73.03	10	18779.5	52	249.31	25
404	Max	-140	0	25	0	25	0	7	122.39	43	1241.34	46	73.03	10	18779.5	52	249.31	25
404	Max	-127	0	25	0	25	0	7	122.39	43	1241.34	46	73.03	10	18779.5	52	249.31	25
404	Max	-126	0	25	0	25	0	7	122.39	43	1241.34	46	73.03	10	18779.5	52	249.31	25
404	Min.	-139	0	1	0	1	0	25	-371.81	16	-3679.48	13	-63.06	25	5885	16	-278.63	10
404	Min.	-140	0	1	0	1	0	25	-371.81	16	-3679.48	13	-63.06	25	5885	16	-278.63	10
404	Min.	-127	0	1	0	1	0	25	-371.81	16	-3679.48	13	-63.06	25	5885	16	-278.63	10
404	Min.	-126	0	1	0	1	0	25	-371.81	16	-3679.48	13	-63.06	25	5885	16	-278.63	10
404	Max	-140	0	52	0	52	0	31	138.27	43	1299.94	46	76.17	7	18742.7	52	272.81	28
404	Max	-141	0	52	0	52	0	31	138.27	43	1299.94	46	76.17	7	18742.7	52	272.81	28
404	Max	-128	0	52	0	52	0	31	138.27	43	1299.94	46	76.17	7	18742.7	52	272.81	28
404	Max	-127	0	52	0	52	0	31	138.27	43	1299.94	46	76.17	7	18742.7	52	272.81	28
404	Min.	-140	0	51	0	51	0	1	-377.01	16	-3732.56	13	-61.98	28	5790.93	16	-240.86	7
404	Min.	-141	0	51	0	51	0	1	-377.01	16	-3732.56	13	-61.98	28	5790.93	16	-240.86	7
404	Min.	-128	0	51	0	51	0	1	-377.01	16	-3732.56	13	-61.98	28	5790.93	16	-240.86	7
404	Min.	-127	0	51	0	51	0	1	-377.01	16	-3732.56	13	-61.98	28	5790.93	16	-240.86	7
404	Max	-141	0	52	0	52	0	31	174.47	43	1366.54	46	43.94	10	18353.3	52	418.35	40
404	Max	-142	0	52	0	52	0	31	174.47	43	1366.54	46	43.94	10	18353.3	52	418.35	40
404	Max	-129	0	52	0	52	0	31	174.47	43	1366.54	46	43.94	10	18353.3	52	418.35	40
404	Max	-128	0	52	0	52	0	31	174.47	43	1366.54	46	43.94	10	18353.3	52	418.35	40
404	Min.	-141	0	51	0	51	0	1	-358.43	16	-3796.88	13	-86.64	25	5410.79	16	-73.21	19
404	Min.	-142	0	51	0	51	0	1	-358.43	16	-3796.88	13	-86.64	25	5410.79	16	-73.21	19
404	Min.	-129	0	51	0	51	0	1	-358.43	16	-3796.88	13	-86.64	25	5410.79	16	-73.21	19
404	Min.	-128	0	51	0	51	0	1	-358.43	16	-3796.88	13	-86.64	25	5410.79	16	-73.21	19
404	Max	-142	0	19	0	16	0	16	153.43	43	1393.16	46	-49.83	13	19410.3	52	1034.67	40
404	Max	-143	0	19	0	16	0	16	153.43	43	1393.16	46	-49.83	13	19410.3	52	1034.67	40
404	Max	-130	0	19	0	16	0	16	153.43	43	1393.16	46	-49.83	13	19410.3	52	1034.67	40
404	Max	-129	0	19	0	16	0	16	153.43	43	1393.16	46	-49.83	13	19410.3	52	1034.67	40
404	Min.	-142	0	40	0	43	0	43	-173.8	16	-3871.56	13	-192.75	52	5799.91	13	-186.89	19
404	Min.	-143	0	40	0	43	0	43	-173.8	16	-3871.56	13	-192.75	52	5799.91	13	-186.89	19
404	Min.	-130	0	40	0	43	0	43	-173.8	16	-3871.56	13	-192.75	52	5799.91	13	-186.89	19
404	Min.	-129	0	40	0	43	0	43	-173.8	16	-3871.56	13	-192.75	52	5799.91	13	-186.89	19
404	Max	-181	0	19	0	43	0	13	153.43	13	1393.16	16	192.75	51	-5799.91	43	1034.67	22
404	Max	-182	0	19	0	43	0	13	153.43	13	1393.16	16						

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404	Max	-168	0	19	0	43	0	13	153.43	13	1393.16	16	192.75	51	-5799.91	43	1034.67	22
404	Min.	-181	0	37	0	13	0	22	-173.8	46	-3871.56	43	49.83	43	-19410.3	51	-186.89	37
404	Min.	-182	0	37	0	13	0	22	-173.8	46	-3871.56	43	49.83	43	-19410.3	51	-186.89	37
404	Min.	-169	0	37	0	13	0	22	-173.8	46	-3871.56	43	49.83	43	-19410.3	51	-186.89	37
404	Min.	-168	0	37	0	13	0	22	-173.8	46	-3871.56	43	49.83	43	-19410.3	51	-186.89	37
404	Max	-157	0	25	0	25	0	1	-126.75	40	-3022.53	37	54.09	22	1125.73	22	-82.95	40
404	Max	-158	0	25	0	25	0	1	-126.75	40	-3022.53	37	54.09	22	1125.73	22	-82.95	40
404	Max	-145	0	25	0	25	0	1	-126.75	40	-3022.53	37	54.09	22	1125.73	22	-82.95	40
404	Max	-144	0	25	0	25	0	1	-126.75	40	-3022.53	37	54.09	22	1125.73	22	-82.95	40
404	Min.	-157	0	1	0	1	0	7	-315.13	52	-7374.75	52	-161.36	37	-8009.78	37	-416.01	52
404	Min.	-158	0	1	0	1	0	7	-315.13	52	-7374.75	52	-161.36	37	-8009.78	37	-416.01	52
404	Min.	-145	0	1	0	1	0	7	-315.13	52	-7374.75	52	-161.36	37	-8009.78	37	-416.01	52
404	Min.	-144	0	1	0	1	0	7	-315.13	52	-7374.75	52	-161.36	37	-8009.78	37	-416.01	52
404	Max	-158	0	52	0	52	0	43	-236.6	40	-2991.33	37	72.96	1	856	22	-40.11	7
404	Max	-159	0	52	0	52	0	43	-236.6	40	-2991.33	37	72.96	1	856	22	-40.11	7
404	Max	-146	0	52	0	52	0	43	-236.6	40	-2991.33	37	72.96	1	856	22	-40.11	7
404	Max	-145	0	52	0	52	0	43	-236.6	40	-2991.33	37	72.96	1	856	22	-40.11	7
404	Min.	-158	0	51	0	51	0	16	-622.36	52	-7273.09	52	-94.71	34	-7289.49	37	-229.96	49
404	Min.	-159	0	51	0	51	0	16	-622.36	52	-7273.09	52	-94.71	34	-7289.49	37	-229.96	49
404	Min.	-146	0	51	0	51	0	16	-622.36	52	-7273.09	52	-94.71	34	-7289.49	37	-229.96	49
404	Min.	-145	0	51	0	51	0	16	-622.36	52	-7273.09	52	-94.71	34	-7289.49	37	-229.96	49
404	Max	-159	0	52	0	52	0	43	-289.06	40	-2999.03	37	86.99	1	858.51	19	30.86	10
404	Max	-160	0	52	0	52	0	43	-289.06	40	-2999.03	37	86.99	1	858.51	19	30.86	10
404	Max	-147	0	52	0	52	0	43	-289.06	40	-2999.03	37	86.99	1	858.51	19	30.86	10
404	Max	-146	0	52	0	52	0	43	-289.06	40	-2999.03	37	86.99	1	858.51	19	30.86	10
404	Min.	-159	0	51	0	51	0	16	-720.2	52	-7257.43	52	-82.15	34	-7489.72	40	-121.22	25
404	Min.	-160	0	51	0	51	0	16	-720.2	52	-7257.43	52	-82.15	34	-7489.72	40	-121.22	25
404	Min.	-147	0	51	0	51	0	16	-720.2	52	-7257.43	52	-82.15	34	-7489.72	40	-121.22	25
404	Min.	-146	0	51	0	51	0	16	-720.2	52	-7257.43	52	-82.15	34	-7489.72	40	-121.22	25
404	Max	-160	0	13	0	13	0	19	-303.14	40	-3032.87	37	84.45	4	742.75	19	57.53	10
404	Max	-161	0	13	0	13	0	19	-303.14	40	-3032.87	37	84.45	4	742.75	19	57.53	10
404	Max	-148	0	13	0	13	0	19	-303.14	40	-3032.87	37	84.45	4	742.75	19	57.53	10
404	Max	-147	0	13	0	13	0	19	-303.14	40	-3032.87	37	84.45	4	742.75	19	57.53	10
404	Min.	-160	0	19	0	19	0	16	-735.12	52	-7273.95	52	-78.7	31	-7358.47	40	-91.51	25
404	Min.	-161	0	19	0	19	0	16	-735.12	52	-7273.95	52	-78.7	31	-7358.47	40	-91.51	25
404	Min.	-148	0	19	0	19	0	16	-735.12	52	-7273.95	52	-78.7	31	-7358.47	40	-91.51	25
404	Min.	-147	0	19	0	19	0	16	-735.12	52	-7273.95	52	-78.7	31	-7358.47	40	-91.51	25
404	Max	-161	0	43	0	43	0	1	-306.78	40	-3064.5	37	80.33	1	654.39	22	73.26	7
404	Max	-162	0	43	0	43	0	1	-306.78	40	-3064.5	37	80.33	1	654.39	22	73.26	7
404	Max	-149	0	43	0	43	0	1	-306.78	40	-3064.5	37	80.33	1	654.39	22	73.26	7
404	Max	-148	0	43	0	43	0	1	-306.78	40	-3064.5	37	80.33	1	654.39	22	73.26	7
404	Min.	-161	0	13	0	13	0	7	-734.63	52	-7284.16	52	-77.36	34	-7291.43	37	-81.93	28
404	Min.	-162	0	13	0	13	0	7	-734.63	52	-7284.16	52	-77.36	34	-7291.43	37	-81.93	28
404	Min.	-149	0	13	0	13	0	7	-734.63	52	-7284.16	52	-77.36	34	-7291.43	37	-81.93	28
404	Min.	-148	0	13	0	13	0	7	-734.63	52	-7284.16	52	-77.36	34	-7291.43	37	-81.93	28
404	Max	-162	0	51	0	51	0	19	-310.13	40	-3092.89	37	78.08	1	571.98	19	77.8	7
404	Max	-163	0	51	0	51	0	19	-310.13	40	-3092.89	37	78.08	1	571.98	19	77.8	7
404	Max	-150	0	51	0	51	0	19	-310.13	40	-3092.89	37	78.08	1	571.98	19	77.8	7
404	Max	-149	0	51	0	51	0	19	-310.13	40	-3092.89	37	78.08	1	571.98	19	77.8	7
404	Min.	-162	0	52	0	52	0	16	-732.37	52	-7288.57	52	-77.24	34	-7210.47	40	-79.83	28
404	Min.	-163	0	52	0	52	0	16	-732.37	52	-7288.57	52	-77.24	34	-7210.47	40	-79.83	28
404	Min.	-150	0	52	0	52	0	16	-732.37	52	-7288.57	52	-77.24	34	-7210.47	40	-79.83	28
404	Min.	-149	0	52	0	52	0	16	-732.37	52	-7288.57	52	-77.24	34	-7210.47	40	-79.83	28
404	Max	-163	0	13	0	13	0	46	-310.13	13	-3092.89	16	77.24	4	571.98	46	79.83	10
404	Max	-164	0	13	0	13	0	46	-310.13	13	-3092.89	16	77.24	4	571.98	46	79.83	10
404	Max	-151	0	13	0	13	0	46	-310.13	13	-3092.89	16	77.24	4	571.98	46	79.83	10
404	Max	-150	0	13	0	13	0	46	-310.13	13	-3092.89	16	77.24	4	571.98	46	79.83	10
404	Min.	-163	0	43	0	43	0	13	-732.37	52	-7288.57	52	-78.08	31	-7210.47	13	-77.8	25
404	Min.	-164	0	43	0	43	0	13	-732.37	52	-7288.57	52	-78.08	31	-7210.47	13	-77.8	25
404	Min.	-151	0	43	0	43	0	13	-732.37	52	-7288.57	52	-78.08	31	-7210.47	13	-77.8	25
404	Min.	-150	0	43	0	43	0	13	-732.37	52	-7288.57	52	-78.08	31	-7210.47	13	-77.8	25
404	Max	-164	0	19	0	19	0	25	-306.78	13	-3064.5	16	77.36	4	654.39	43	81.93	10
404	Max	-165	0	19	0	19	0	25	-306.78	13	-3064.5	16	77.36	4	654.39	43	81.93	10
404	Max	-152	0	19	0	19	0	25	-306.78	13	-3064.5	16	77.36	4	654.39	43	81.93	10
404	Max	-151	0	19	0	19	0	25	-306.78	13	-3064.5	16	77.36	4	654.39	43	81.93	10
404	Min.	-164	0	37	0	37	0	7	-734.63	52	-7284.16	52	-80.33	31	-7291.43	16	-73.26	25
404	Min.	-165	0	37	0	37	0	7	-734.63	52	-7284.16	52	-80.33	31	-7291.43	16	-73.26	25
404	Min.	-152	0	37	0	37	0	7	-734.63	52	-7284.16	52	-80.33	31	-7291.43	16	-73.26	25
404	Min.	-151	0	37	0	37	0	7	-734.63	52	-7284.16	52	-80.33	31	-7291.43	16	-73.26	25
404	Max	-165	0	51	0	51	0	22	-303.14	13	-3032.87	16	78.7	1	742.75	46	91.51	7
404	Max	-166	0	51	0	51	0	22	-303.14	13	-3032.87	16	78.7	1	742.75	46	91.51	7
404	Max	-153	0	51	0	51	0	22	-303.14	13	-3032.87	16	78.7	1	742.75	46	91.51	7
404	Max	-152	0	51	0	51	0	22	-303.14	13	-3032.87	16	78.7	1	742.75	46	91.51	7
404	Min.	-165	0	52	0	52	0	37	-735.12	52	-7273.95	52	-84.45	34	-7358.47	13	-57.53	28
404	Min.	-166	0	52	0	52	0	37	-735.12	52	-7273.95	52	-84.45	34	-7358.47	13	-57.53	28
404	Min.	-153	0	52	0	52	0	37	-735.12	52	-7273.95	52	-84.45	34	-7358.47	13	-57.53	28
404	Min.	-152	0	52	0	52	0	37	-735.12	52	-7273.95	52	-84.45	34	-7358.47	13	-57.53	28
404	Max	-166	0	13	0	13	0	43	-289.06	13	-2999.03	16	82.15	4	858.51	46	121.22	7
404	Max	-167	0	13	0	13	0	43	-289.06	13	-2999.03	16	82.15	4	858.51	46	121.22	7
404	Max	-154	0	13	0	13	0	43	-289.06	13	-2999.03	16	82.15	4	858.51</			

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404	Min.	-166	0	43	0	43	0	16	-720.2	52	-7257.43	52	-86.99	31	-7489.72	13	-30.86	28
404	Min.	-167	0	43	0	43	0	16	-720.2	52	-7257.43	52	-86.99	31	-7489.72	13	-30.86	28
404	Min.	-154	0	43	0	43	0	16	-720.2	52	-7257.43	52	-86.99	31	-7489.72	13	-30.86	28
404	Min.	-153	0	43	0	43	0	16	-720.2	52	-7257.43	52	-86.99	31	-7489.72	13	-30.86	28
404	Max	-167	0	52	0	52	0	46	-236.6	13	-2991.33	16	94.71	4	856	43	229.96	50
404	Max	-168	0	52	0	52	0	46	-236.6	13	-2991.33	16	94.71	4	856	43	229.96	50
404	Max	-155	0	52	0	52	0	46	-236.6	13	-2991.33	16	94.71	4	856	43	229.96	50
404	Max	-154	0	52	0	52	0	46	-236.6	13	-2991.33	16	94.71	4	856	43	229.96	50
404	Min.	-167	0	51	0	51	0	13	-622.36	52	-7273.09	52	-72.96	31	-7289.49	16	40.11	25
404	Min.	-168	0	51	0	51	0	13	-622.36	52	-7273.09	52	-72.96	31	-7289.49	16	40.11	25
404	Min.	-155	0	51	0	51	0	13	-622.36	52	-7273.09	52	-72.96	31	-7289.49	16	40.11	25
404	Min.	-154	0	51	0	51	0	13	-622.36	52	-7273.09	52	-72.96	31	-7289.49	16	40.11	25
404	Max	-168	0	43	0	43	0	1	-126.75	13	-3022.53	16	161.36	16	1125.73	43	416.01	52
404	Max	-169	0	43	0	43	0	1	-126.75	13	-3022.53	16	161.36	16	1125.73	43	416.01	52
404	Max	-156	0	43	0	43	0	1	-126.75	13	-3022.53	16	161.36	16	1125.73	43	416.01	52
404	Max	-155	0	43	0	43	0	1	-126.75	13	-3022.53	16	161.36	16	1125.73	43	416.01	52
404	Min.	-168	0	13	0	13	0	31	-315.13	52	-7374.75	52	-54.09	43	-8009.78	16	82.95	13
404	Min.	-169	0	13	0	13	0	31	-315.13	52	-7374.75	52	-54.09	43	-8009.78	16	82.95	13
404	Min.	-156	0	13	0	13	0	31	-315.13	52	-7374.75	52	-54.09	43	-8009.78	16	82.95	13
404	Min.	-155	0	13	0	13	0	31	-315.13	52	-7374.75	52	-54.09	43	-8009.78	16	82.95	13
404	Max	-144	0	37	0	13	0	13	-126.75	22	-3022.53	19	161.36	19	8009.78	19	-82.95	22
404	Max	-145	0	37	0	13	0	13	-126.75	22	-3022.53	19	161.36	19	8009.78	19	-82.95	22
404	Max	-132	0	37	0	13	0	13	-126.75	22	-3022.53	19	161.36	19	8009.78	19	-82.95	22
404	Max	-131	0	37	0	13	0	13	-126.75	22	-3022.53	19	161.36	19	8009.78	19	-82.95	22
404	Min.	-144	0	19	0	43	0	46	-315.13	51	-7374.75	51	-54.09	40	-1125.73	40	-416.01	51
404	Min.	-145	0	19	0	43	0	46	-315.13	51	-7374.75	51	-54.09	40	-1125.73	40	-416.01	51
404	Min.	-132	0	19	0	43	0	46	-315.13	51	-7374.75	51	-54.09	40	-1125.73	40	-416.01	51
404	Min.	-131	0	19	0	43	0	46	-315.13	51	-7374.75	51	-54.09	40	-1125.73	40	-416.01	51
404	Max	-145	0	19	0	19	0	25	-236.6	22	-2991.33	19	94.71	7	7289.49	19	-40.11	34
404	Max	-146	0	19	0	19	0	25	-236.6	22	-2991.33	19	94.71	7	7289.49	19	-40.11	34
404	Max	-133	0	19	0	19	0	25	-236.6	22	-2991.33	19	94.71	7	7289.49	19	-40.11	34
404	Max	-132	0	19	0	19	0	25	-236.6	22	-2991.33	19	94.71	7	7289.49	19	-40.11	34
404	Min.	-145	0	37	0	37	0	7	-622.36	51	-7273.09	51	-72.96	28	-856	40	-229.96	49
404	Min.	-146	0	37	0	37	0	7	-622.36	51	-7273.09	51	-72.96	28	-856	40	-229.96	49
404	Min.	-133	0	37	0	37	0	7	-622.36	51	-7273.09	51	-72.96	28	-856	40	-229.96	49
404	Min.	-132	0	37	0	37	0	7	-622.36	51	-7273.09	51	-72.96	28	-856	40	-229.96	49
404	Max	-146	0	43	0	43	0	1	-289.06	22	-2999.03	19	82.15	7	7489.72	22	30.86	31
404	Max	-147	0	43	0	43	0	1	-289.06	22	-2999.03	19	82.15	7	7489.72	22	30.86	31
404	Max	-134	0	43	0	43	0	1	-289.06	22	-2999.03	19	82.15	7	7489.72	22	30.86	31
404	Max	-133	0	43	0	43	0	1	-289.06	22	-2999.03	19	82.15	7	7489.72	22	30.86	31
404	Min.	-146	0	13	0	13	0	31	-720.2	51	-7257.43	51	-86.99	28	-858.51	37	-121.22	4
404	Min.	-147	0	13	0	13	0	31	-720.2	51	-7257.43	51	-86.99	28	-858.51	37	-121.22	4
404	Min.	-134	0	13	0	13	0	31	-720.2	51	-7257.43	51	-86.99	28	-858.51	37	-121.22	4
404	Min.	-133	0	13	0	13	0	31	-720.2	51	-7257.43	51	-86.99	28	-858.51	37	-121.22	4
404	Max	-147	0	51	0	51	0	1	-303.14	22	-3032.87	19	78.7	10	7358.47	22	57.53	31
404	Max	-148	0	51	0	51	0	1	-303.14	22	-3032.87	19	78.7	10	7358.47	22	57.53	31
404	Max	-135	0	51	0	51	0	1	-303.14	22	-3032.87	19	78.7	10	7358.47	22	57.53	31
404	Max	-134	0	51	0	51	0	1	-303.14	22	-3032.87	19	78.7	10	7358.47	22	57.53	31
404	Min.	-147	0	52	0	52	0	31	-735.12	51	-7273.95	51	-84.45	25	-742.75	37	-91.51	4
404	Min.	-148	0	52	0	52	0	31	-735.12	51	-7273.95	51	-84.45	25	-742.75	37	-91.51	4
404	Min.	-135	0	52	0	52	0	31	-735.12	51	-7273.95	51	-84.45	25	-742.75	37	-91.51	4
404	Min.	-134	0	52	0	52	0	31	-735.12	51	-7273.95	51	-84.45	25	-742.75	37	-91.51	4
404	Max	-148	0	43	0	43	0	13	-306.78	22	-3064.5	19	77.36	7	7291.43	19	73.26	34
404	Max	-149	0	43	0	43	0	13	-306.78	22	-3064.5	19	77.36	7	7291.43	19	73.26	34
404	Max	-136	0	43	0	43	0	13	-306.78	22	-3064.5	19	77.36	7	7291.43	19	73.26	34
404	Max	-135	0	43	0	43	0	13	-306.78	22	-3064.5	19	77.36	7	7291.43	19	73.26	34
404	Min.	-148	0	13	0	13	0	46	-734.63	51	-7284.16	51	-80.33	28	-654.39	40	-81.93	1
404	Min.	-149	0	13	0	13	0	46	-734.63	51	-7284.16	51	-80.33	28	-654.39	40	-81.93	1
404	Min.	-136	0	13	0	13	0	46	-734.63	51	-7284.16	51	-80.33	28	-654.39	40	-81.93	1
404	Min.	-135	0	13	0	13	0	46	-734.63	51	-7284.16	51	-80.33	28	-654.39	40	-81.93	1
404	Max	-149	0	43	0	43	0	1	-310.13	22	-3092.89	19	77.24	7	7210.47	22	77.8	34
404	Max	-150	0	43	0	43	0	1	-310.13	22	-3092.89	19	77.24	7	7210.47	22	77.8	34
404	Max	-137	0	43	0	43	0	1	-310.13	22	-3092.89	19	77.24	7	7210.47	22	77.8	34
404	Max	-136	0	43	0	43	0	1	-310.13	22	-3092.89	19	77.24	7	7210.47	22	77.8	34
404	Min.	-149	0	13	0	13	0	31	-732.37	51	-7288.57	51	-78.08	28	-571.98	37	-79.83	1
404	Min.	-150	0	13	0	13	0	31	-732.37	51	-7288.57	51	-78.08	28	-571.98	37	-79.83	1
404	Min.	-137	0	13	0	13	0	31	-732.37	51	-7288.57	51	-78.08	28	-571.98	37	-79.83	1
404	Min.	-136	0	13	0	13	0	31	-732.37	51	-7288.57	51	-78.08	28	-571.98	37	-79.83	1
404	Max	-150	0	25	0	25	0	50	-310.13	43	-3092.89	46	78.08	10	7210.47	43	79.83	31
404	Max	-151	0	25	0	25	0	50	-310.13	43	-3092.89	46	78.08	10	7210.47	43	79.83	31
404	Max	-138	0	25	0	25	0	50	-310.13	43	-3092.89	46	78.08	10	7210.47	43	79.83	31
404	Max	-137	0	25	0	25	0	50	-310.13	43	-3092.89	46	78.08	10	7210.47	43	79.83	31
404	Min.	-150	0	1	0	1	0	49	-732.37	51	-7288.57	51	-77.24	25	-571.98	16	-77.8	4
404	Min.	-151	0	1	0	1	0	49	-732.37	51	-7288.57	51	-77.24	25	-571.98	16	-77.8	4
404	Min.	-138	0	1	0	1	0	49	-732.37	51	-7288.57	51	-77.24	25	-571.98	16	-77.8	4
404	Min.	-137	0	1	0	1	0	49	-732.37	51	-7288.57	51	-77.24	25	-571.98	16	-77.8	4
404	Max	-151	0	43	0	43	0	13	-306.78	43	-3064.5	46	80.33	10	7291.43	46	81.93	31
404	Max	-152	0	43	0	43	0	13	-306.78	43	-3064.5	46	80.33	10	7291.43	46	81.93	31
404	Max	-139	0	43	0	43	0	13	-306.78	43	-3064.5	46	80.33	10	7291.43	46	81.93	31
404	Max	-138	0	43	0	43	0	13	-306.78	43	-3064.5	46	80.33	10				

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404	Min.	-152	0	13	0	13	0	46	-734.63	51	-7284.16	51	-77.36	25	-654.39	13	-73.26	4
404	Min.	-139	0	13	0	13	0	46	-734.63	51	-7284.16	51	-77.36	25	-654.39	13	-73.26	4
404	Min.	-138	0	13	0	13	0	46	-734.63	51	-7284.16	51	-77.36	25	-654.39	13	-73.26	4
404	Max	-152	0	43	0	43	0	7	-303.14	43	-3032.87	46	84.45	7	7358.47	43	91.51	34
404	Max	-153	0	43	0	43	0	7	-303.14	43	-3032.87	46	84.45	7	7358.47	43	91.51	34
404	Max	-140	0	43	0	43	0	7	-303.14	43	-3032.87	46	84.45	7	7358.47	43	91.51	34
404	Max	-139	0	43	0	43	0	7	-303.14	43	-3032.87	46	84.45	7	7358.47	43	91.51	34
404	Min.	-152	0	13	0	13	0	25	-735.12	51	-7273.95	51	-78.7	28	-742.75	16	-57.53	1
404	Min.	-153	0	13	0	13	0	25	-735.12	51	-7273.95	51	-78.7	28	-742.75	16	-57.53	1
404	Min.	-140	0	13	0	13	0	25	-735.12	51	-7273.95	51	-78.7	28	-742.75	16	-57.53	1
404	Min.	-139	0	13	0	13	0	25	-735.12	51	-7273.95	51	-78.7	28	-742.75	16	-57.53	1
404	Max	-153	0	52	0	52	0	51	-289.06	43	-2999.03	46	86.99	10	7489.72	43	121.22	34
404	Max	-154	0	52	0	52	0	51	-289.06	43	-2999.03	46	86.99	10	7489.72	43	121.22	34
404	Max	-141	0	52	0	52	0	51	-289.06	43	-2999.03	46	86.99	10	7489.72	43	121.22	34
404	Max	-140	0	52	0	52	0	51	-289.06	43	-2999.03	46	86.99	10	7489.72	43	121.22	34
404	Min.	-153	0	51	0	51	0	52	-720.2	51	-7257.43	51	-82.15	25	-858.51	16	-30.86	1
404	Min.	-154	0	51	0	51	0	52	-720.2	51	-7257.43	51	-82.15	25	-858.51	16	-30.86	1
404	Min.	-141	0	51	0	51	0	52	-720.2	51	-7257.43	51	-82.15	25	-858.51	16	-30.86	1
404	Min.	-140	0	51	0	51	0	52	-720.2	51	-7257.43	51	-82.15	25	-858.51	16	-30.86	1
404	Max	-154	0	1	0	1	0	7	-236.64	43	-2991.33	46	72.96	10	7289.49	46	229.96	50
404	Max	-155	0	1	0	1	0	7	-236.64	43	-2991.33	46	72.96	10	7289.49	46	229.96	50
404	Max	-142	0	1	0	1	0	7	-236.64	43	-2991.33	46	72.96	10	7289.49	46	229.96	50
404	Max	-141	0	1	0	1	0	7	-236.64	43	-2991.33	46	72.96	10	7289.49	46	229.96	50
404	Min.	-154	0	25	0	25	0	1	-622.36	51	-7273.09	51	-94.71	25	-856	13	40.11	4
404	Min.	-155	0	25	0	25	0	1	-622.36	51	-7273.09	51	-94.71	25	-856	13	40.11	4
404	Min.	-142	0	25	0	25	0	1	-622.36	51	-7273.09	51	-94.71	25	-856	13	40.11	4
404	Min.	-141	0	25	0	25	0	1	-622.36	51	-7273.09	51	-94.71	25	-856	13	40.11	4
404	Max	-155	0	51	0	51	0	13	-126.75	43	-3022.53	46	54.09	13	8009.78	46	416.01	51
404	Max	-156	0	51	0	51	0	13	-126.75	43	-3022.53	46	54.09	13	8009.78	46	416.01	51
404	Max	-143	0	51	0	51	0	13	-126.75	43	-3022.53	46	54.09	13	8009.78	46	416.01	51
404	Max	-142	0	51	0	51	0	13	-126.75	43	-3022.53	46	54.09	13	8009.78	46	416.01	51
404	Min.	-155	0	52	0	52	0	46	-315.13	51	-7374.75	51	-161.36	46	-1125.73	13	82.95	43
404	Min.	-156	0	52	0	52	0	46	-315.13	51	-7374.75	51	-161.36	46	-1125.73	13	82.95	43
404	Min.	-143	0	52	0	52	0	46	-315.13	51	-7374.75	51	-161.36	46	-1125.73	13	82.95	43
404	Min.	-142	0	52	0	52	0	46	-315.13	51	-7374.75	51	-161.36	46	-1125.73	13	82.95	43
404	Max	-131	0	13	0	13	0	16	153.43	22	1393.16	19	192.75	52	19410.3	52	186.89	46
404	Max	-132	0	13	0	13	0	16	153.43	22	1393.16	19	192.75	52	19410.3	52	186.89	46
404	Max	-119	0	13	0	13	0	16	153.43	22	1393.16	19	192.75	52	19410.3	52	186.89	46
404	Max	-118	0	13	0	13	0	16	153.43	22	1393.16	19	192.75	52	19410.3	52	186.89	46
404	Min.	-131	0	43	0	43	0	43	-173.8	37	-3871.56	40	49.83	40	5799.91	40	-1034.67	13
404	Min.	-132	0	43	0	43	0	43	-173.8	37	-3871.56	40	49.83	40	5799.91	40	-1034.67	13
404	Min.	-119	0	43	0	43	0	43	-173.8	37	-3871.56	40	49.83	40	5799.91	40	-1034.67	13
404	Min.	-118	0	43	0	43	0	43	-173.8	37	-3871.56	40	49.83	40	5799.91	40	-1034.67	13
404	Max	-132	0	43	0	43	0	31	174.47	22	1366.54	19	86.64	7	18353.3	52	73.21	46
404	Max	-133	0	43	0	43	0	31	174.47	22	1366.54	19	86.64	7	18353.3	52	73.21	46
404	Max	-120	0	43	0	43	0	31	174.47	22	1366.54	19	86.64	7	18353.3	52	73.21	46
404	Max	-119	0	43	0	43	0	31	174.47	22	1366.54	19	86.64	7	18353.3	52	73.21	46
404	Min.	-132	0	13	0	13	0	1	-358.43	37	-3796.88	40	-43.94	28	5410.79	37	-418.35	13
404	Min.	-133	0	13	0	13	0	1	-358.43	37	-3796.88	40	-43.94	28	5410.79	37	-418.35	13
404	Min.	-120	0	13	0	13	0	1	-358.43	37	-3796.88	40	-43.94	28	5410.79	37	-418.35	13
404	Min.	-119	0	13	0	13	0	1	-358.43	37	-3796.88	40	-43.94	28	5410.79	37	-418.35	13
404	Max	-133	0	1	0	1	0	25	138.27	22	1299.9	19	61.98	10	18742.7	52	240.86	25
404	Max	-134	0	1	0	1	0	25	138.27	22	1299.9	19	61.98	10	18742.7	52	240.86	25
404	Max	-121	0	1	0	1	0	25	138.27	22	1299.9	19	61.98	10	18742.7	52	240.86	25
404	Max	-120	0	1	0	1	0	25	138.27	22	1299.9	19	61.98	10	18742.7	52	240.86	25
404	Min.	-133	0	25	0	25	0	7	-377.01	37	-3732.56	40	-76.17	25	5790.93	37	-272.81	10
404	Min.	-134	0	25	0	25	0	7	-377.01	37	-3732.56	40	-76.17	25	5790.93	37	-272.81	10
404	Min.	-121	0	25	0	25	0	7	-377.01	37	-3732.56	40	-76.17	25	5790.93	37	-272.81	10
404	Min.	-120	0	25	0	25	0	7	-377.01	37	-3732.56	40	-76.17	25	5790.93	37	-272.81	10
404	Max	-134	0	51	0	51	0	52	122.39	22	1241.34	19	63.06	7	18779.5	52	278.63	28
404	Max	-135	0	51	0	51	0	52	122.39	22	1241.34	19	63.06	7	18779.5	52	278.63	28
404	Max	-122	0	51	0	51	0	52	122.39	22	1241.34	19	63.06	7	18779.5	52	278.63	28
404	Max	-121	0	51	0	51	0	52	122.39	22	1241.34	19	63.06	7	18779.5	52	278.63	28
404	Min.	-134	0	52	0	52	0	51	-371.81	37	-3679.48	40	-73.03	28	5885	37	-249.31	7
404	Min.	-135	0	52	0	52	0	51	-371.81	37	-3679.48	40	-73.03	28	5885	37	-249.31	7
404	Min.	-122	0	52	0	52	0	51	-371.81	37	-3679.48	40	-73.03	28	5885	37	-249.31	7
404	Min.	-121	0	52	0	52	0	51	-371.81	37	-3679.48	40	-73.03	28	5885	37	-249.31	7
404	Max	-135	0	25	0	25	0	13	117.87	22	1178.91	19	63.65	7	18813.2	52	277.5	28
404	Max	-136	0	25	0	25	0	13	117.87	22	1178.91	19	63.65	7	18813.2	52	277.5	28
404	Max	-123	0	25	0	25	0	13	117.87	22	1178.91	19	63.65	7	18813.2	52	277.5	28
404	Max	-122	0	25	0	25	0	13	117.87	22	1178.91	19	63.65	7	18813.2	52	277.5	28
404	Min.	-135	0	1	0	1	0	46	-365.23	37	-3619.78	40	-69.58	28	5985.29	37	-258.97	7
404	Min.	-136	0	1	0	1	0	46	-365.23	37	-3619.78	40	-69.58	28	5985.29	37	-258.97	7
404	Min.	-123	0	1	0	1	0	46	-365.23	37	-3619.78	40	-69.58	28	5985.29	37	-258.97	7
404	Min.	-122	0	1	0	1	0	46	-365.23	37	-3619.78	40	-69.58	28	5985.29	37	-258.97	7
404	Max	-136	0	52	0	52	0	7	111.48	22	1118.8	19	65.15	10	18818.6	52	271.42	28
404	Max	-137	0	52	0	52	0	7	111.48	22	1118.8	19	65.15	10	18818.6	52	271.42	28
404	Max	-124	0	52	0	52	0	7	111.48	22	1118.8	19	65.15	10	18818.6	52	271.42	28
404	Max	-123	0	52	0	52	0	7	111.48	22	1118.8	19	65.15	10	18818.6	52	271.42	28
404	Min.	-136	0	51	0	51	0	25	-357.56									

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404	Min.	-124	0	51	0	51	0	25	-357.56	37	-3561.52	40	-66.73	25	6068.45	37	-265.6	7
404	Min.	-123	0	51	0	51	0	25	-357.56	37	-3561.52	40	-66.73	25	6068.45	37	-265.6	7
404	Max	-137	0	51	0	51	0	31	111.48	43	1118.8	46	66.73	7	18818.6	52	265.6	25
404	Max	-138	0	51	0	51	0	31	111.48	43	1118.8	46	66.73	7	18818.6	52	265.6	25
404	Max	-125	0	51	0	51	0	31	111.48	43	1118.8	46	66.73	7	18818.6	52	265.6	25
404	Max	-124	0	51	0	51	0	31	111.48	43	1118.8	46	66.73	7	18818.6	52	265.6	25
404	Min.	-137	0	52	0	52	0	1	-357.56	16	-3561.52	13	-65.15	28	6068.45	16	-271.42	10
404	Min.	-138	0	52	0	52	0	1	-357.56	16	-3561.52	13	-65.15	28	6068.45	16	-271.42	10
404	Min.	-125	0	52	0	52	0	1	-357.56	16	-3561.52	13	-65.15	28	6068.45	16	-271.42	10
404	Min.	-124	0	52	0	52	0	1	-357.56	16	-3561.52	13	-65.15	28	6068.45	16	-271.42	10
404	Max	-171	0	52	0	52	0	31	174.47	40	1366.54	37	43.94	1	-5410.79	19	73.21	16
404	Max	-172	0	52	0	52	0	31	174.47	40	1366.54	37	43.94	1	-5410.79	19	73.21	16
404	Max	-159	0	52	0	52	0	31	174.47	40	1366.54	37	43.94	1	-5410.79	19	73.21	16
404	Max	-158	0	52	0	52	0	31	174.47	40	1366.54	37	43.94	1	-5410.79	19	73.21	16
404	Min.	-171	0	51	0	51	0	1	-358.43	19	-3796.88	22	-86.64	34	-18353.3	51	-418.35	43
404	Min.	-172	0	51	0	51	0	1	-358.43	19	-3796.88	22	-86.64	34	-18353.3	51	-418.35	43
404	Min.	-159	0	51	0	51	0	1	-358.43	19	-3796.88	22	-86.64	34	-18353.3	51	-418.35	43
404	Min.	-158	0	51	0	51	0	1	-358.43	19	-3796.88	22	-86.64	34	-18353.3	51	-418.35	43
404	Max	-172	0	52	0	52	0	51	138.27	40	1299.9	37	76.17	4	-5790.93	19	240.86	4
404	Max	-173	0	52	0	52	0	51	138.27	40	1299.9	37	76.17	4	-5790.93	19	240.86	4
404	Max	-160	0	52	0	52	0	51	138.27	40	1299.9	37	76.17	4	-5790.93	19	240.86	4
404	Max	-159	0	52	0	52	0	51	138.27	40	1299.9	37	76.17	4	-5790.93	19	240.86	4
404	Min.	-172	0	51	0	51	0	52	-377.01	19	-3732.56	22	-61.98	31	-18742.7	51	-272.81	31
404	Min.	-173	0	51	0	51	0	52	-377.01	19	-3732.56	22	-61.98	31	-18742.7	51	-272.81	31
404	Min.	-160	0	51	0	51	0	52	-377.01	19	-3732.56	22	-61.98	31	-18742.7	51	-272.81	31
404	Min.	-159	0	51	0	51	0	52	-377.01	19	-3732.56	22	-61.98	31	-18742.7	51	-272.81	31
404	Max	-173	0	13	0	13	0	7	122.39	40	1241.34	37	73.03	1	-5885	19	278.63	1
404	Max	-174	0	13	0	13	0	7	122.39	40	1241.34	37	73.03	1	-5885	19	278.63	1
404	Max	-161	0	13	0	13	0	7	122.39	40	1241.34	37	73.03	1	-5885	19	278.63	1
404	Max	-160	0	13	0	13	0	7	122.39	40	1241.34	37	73.03	1	-5885	19	278.63	1
404	Min.	-173	0	43	0	43	0	25	-371.81	19	-3679.48	22	-63.06	34	-18779.5	51	-249.31	34
404	Min.	-174	0	43	0	43	0	25	-371.81	19	-3679.48	22	-63.06	34	-18779.5	51	-249.31	34
404	Min.	-161	0	43	0	43	0	25	-371.81	19	-3679.48	22	-63.06	34	-18779.5	51	-249.31	34
404	Min.	-160	0	43	0	43	0	25	-371.81	19	-3679.48	22	-63.06	34	-18779.5	51	-249.31	34
404	Max	-174	0	13	0	13	0	37	117.87	40	1178.91	37	69.58	1	-5985.29	19	277.5	1
404	Max	-175	0	13	0	13	0	37	117.87	40	1178.91	37	69.58	1	-5985.29	19	277.5	1
404	Max	-162	0	13	0	13	0	37	117.87	40	1178.91	37	69.58	1	-5985.29	19	277.5	1
404	Max	-161	0	13	0	13	0	37	117.87	40	1178.91	37	69.58	1	-5985.29	19	277.5	1
404	Min.	-174	0	43	0	43	0	22	-365.23	19	-3619.78	22	-63.65	34	-18813.2	51	-258.97	34
404	Min.	-175	0	43	0	43	0	22	-365.23	19	-3619.78	22	-63.65	34	-18813.2	51	-258.97	34
404	Min.	-162	0	43	0	43	0	22	-365.23	19	-3619.78	22	-63.65	34	-18813.2	51	-258.97	34
404	Min.	-161	0	43	0	43	0	22	-365.23	19	-3619.78	22	-63.65	34	-18813.2	51	-258.97	34
404	Max	-175	0	51	0	51	0	31	111.48	40	1118.8	37	66.73	4	-6068.45	19	271.42	1
404	Max	-176	0	51	0	51	0	31	111.48	40	1118.8	37	66.73	4	-6068.45	19	271.42	1
404	Max	-163	0	51	0	51	0	31	111.48	40	1118.8	37	66.73	4	-6068.45	19	271.42	1
404	Max	-162	0	51	0	51	0	31	111.48	40	1118.8	37	66.73	4	-6068.45	19	271.42	1
404	Min.	-175	0	52	0	52	0	1	-357.56	19	-3561.52	22	-65.15	31	-18818.6	51	-265.6	34
404	Min.	-176	0	52	0	52	0	1	-357.56	19	-3561.52	22	-65.15	31	-18818.6	51	-265.6	34
404	Min.	-163	0	52	0	52	0	1	-357.56	19	-3561.52	22	-65.15	31	-18818.6	51	-265.6	34
404	Min.	-162	0	52	0	52	0	1	-357.56	19	-3561.52	22	-65.15	31	-18818.6	51	-265.6	34
404	Max	-176	0	13	0	13	0	31	111.48	13	1118.8	16	65.15	1	-6068.45	46	265.6	4
404	Max	-177	0	13	0	13	0	31	111.48	13	1118.8	16	65.15	1	-6068.45	46	265.6	4
404	Max	-164	0	13	0	13	0	31	111.48	13	1118.8	16	65.15	1	-6068.45	46	265.6	4
404	Max	-163	0	13	0	13	0	31	111.48	13	1118.8	16	65.15	1	-6068.45	46	265.6	4
404	Min.	-176	0	43	0	43	0	1	-357.56	46	-3561.52	43	-66.73	34	-18818.6	51	-271.42	31
404	Min.	-177	0	43	0	43	0	1	-357.56	46	-3561.52	43	-66.73	34	-18818.6	51	-271.42	31
404	Min.	-164	0	43	0	43	0	1	-357.56	46	-3561.52	43	-66.73	34	-18818.6	51	-271.42	31
404	Min.	-163	0	43	0	43	0	1	-357.56	46	-3561.52	43	-66.73	34	-18818.6	51	-271.42	31
404	Max	-177	0	13	0	13	0	40	117.87	13	1178.91	16	63.65	4	-5985.29	46	258.97	4
404	Max	-178	0	13	0	13	0	40	117.87	13	1178.91	16	63.65	4	-5985.29	46	258.97	4
404	Max	-165	0	13	0	13	0	40	117.87	13	1178.91	16	63.65	4	-5985.29	46	258.97	4
404	Max	-164	0	13	0	13	0	40	117.87	13	1178.91	16	63.65	4	-5985.29	46	258.97	4
404	Min.	-177	0	43	0	43	0	19	-365.23	46	-3619.78	43	-69.58	31	-18813.2	51	-277.5	31
404	Min.	-178	0	43	0	43	0	19	-365.23	46	-3619.78	43	-69.58	31	-18813.2	51	-277.5	31
404	Min.	-165	0	43	0	43	0	19	-365.23	46	-3619.78	43	-69.58	31	-18813.2	51	-277.5	31
404	Min.	-164	0	43	0	43	0	19	-365.23	46	-3619.78	43	-69.58	31	-18813.2	51	-277.5	31
404	Max	-178	0	51	0	51	0	7	122.39	13	1241.34	16	63.06	4	-5885	46	249.31	4
404	Max	-179	0	51	0	51	0	7	122.39	13	1241.34	16	63.06	4	-5885	46	249.31	4
404	Max	-166	0	51	0	51	0	7	122.39	13	1241.34	16	63.06	4	-5885	46	249.31	4
404	Max	-165	0	51	0	51	0	7	122.39	13	1241.34	16	63.06	4	-5885	46	249.31	4
404	Min.	-178	0	52	0	52	0	25	-371.81	46	-3679.48	43	-73.03	31	-18779.5	51	-278.63	31
404	Min.	-179	0	52	0	52	0	25	-371.81	46	-3679.48	43	-73.03	31	-18779.5	51	-278.63	31
404	Min.	-166	0	52	0	52	0	25	-371.81	46	-3679.48	43	-73.03	31	-18779.5	51	-278.63	31
404	Min.	-165	0	52	0	52	0	25	-371.81	46	-3679.48	43	-73.03	31	-18779.5	51	-278.63	31
404	Max	-179	0	37	0	37	0	51	138.27	13	1299.9	16	61.98	1	-5790.93	46	272.81	1
404	Max	-180	0	37	0	37	0	51	138.27	13	1299.9	16	61.98	1	-5790.93	46	272.81	1
404	Max	-167	0	37	0	37	0	51	138.27	13	1299.9	16	61.98	1	-5790.93	46	272.81	1
404	Max	-166	0	37	0	37	0	51	138.27	13	1299.9	16	61.98	1	-5790.93	46	272.81	1
404	Min.	-179	0	19	0	19	0	52	-377.01	46	-3732.56	43	-76.17	34	-18742.7	51	-240.86	34
404	Min.	-180	0	19	0	19	0	52	-377.01	4								

Relazione geotecnica tombino

404	Min.	-166	0	19	0	19	0	52	-377.01	46	-3732.56	43	-76.17	34	-18742.7	51	-240.86	34
404	Max	-180	0	13	0	37	0	49	174.47	13	1366.54	16	86.64	4	-5410.79	46	418.35	22
404	Max	-181	0	13	0	37	0	49	174.47	13	1366.54	16	86.64	4	-5410.79	46	418.35	22
404	Max	-168	0	13	0	37	0	49	174.47	13	1366.54	16	86.64	4	-5410.79	46	418.35	22
404	Max	-167	0	13	0	37	0	49	174.47	13	1366.54	16	86.64	4	-5410.79	46	418.35	22
404	Min.	-180	0	43	0	19	0	50	-358.43	46	-3796.88	43	-43.94	31	-18353.3	51	-73.21	37
404	Min.	-181	0	43	0	19	0	50	-358.43	46	-3796.88	43	-43.94	31	-18353.3	51	-73.21	37
404	Min.	-168	0	43	0	19	0	50	-358.43	46	-3796.88	43	-43.94	31	-18353.3	51	-73.21	37
404	Min.	-167	0	43	0	19	0	50	-358.43	46	-3796.88	43	-43.94	31	-18353.3	51	-73.21	37

Criteri di progetto utilizzati

Pareti

Generali	
Verifiche a taglio per elementi esistenti come per elementi nuovi	Si
Parametri di disegno	
Scala disegno pareti	50
Campitura disegno parete	Rada
Disegno armatura diffusa	No
Disegno prospetto e pianta	Sempre
Stampe	
Tipo di relazione	Sintetica

Specifici	1
Materiali	
-Considera come elemento esistente	No
-Calcestruzzo	
-Livello di conoscenza	LC2
-Fattore di confidenza	1.2
-Tipo di calcestruzzo	C28/35
-Rck calcestruzzo	350
-Modulo elastico <daN/cm²>	325881
-Resistenza caratteristica cilindrica (Fck)	290.5
-Resistenza caratteristica a trazione (Fctk)	19.84
-Resistenza media (Fcm) <daN/cm²>	370.5
-Resistenza media a trazione (Fctm) <daN/cm²>	28.35
-σ amm. calcestruzzo <daN/cm²>	110
-τc0 <daN/cm²>	6.7
-τc1 <daN/cm²>	19.7
-Riduci Fcd per tutte le verifiche secondo il D.M. 08	Si
-γc per stati limite ultimi	
-Automatico	x
-Pari a	
-Acciaio	
-Livello di conoscenza	LC2
-Fattore di confidenza	1.2
-Tipo di acciaio	B450C
-Modulo elastico <daN/cm²>	2060000
-Tensione caratteristica di snervamento (Fyk) <daN/cm²>	4500
-Tensione media di snervamento (Fym) <daN/cm²>	4500
-Sigma amm. acciaio <daN/cm²>	2600
-Sigma amm. reti e tralicci <daN/cm²>	2600
-Allungamento per verifiche di duttilità (Agt) <%>	4
-γs per stati limite ultimi	
-Automatico	x
-Pari a	
-Coeff. di omogeneizzazione	15
Parametri di calcolo	
Copriferro <cm>	2.5
Fattore moltiplicativo per calcolo τ l	1
Fattore moltiplicativo per calcolo τ t	1
Fattore di riduzione per ancoraggio ferri	1
Lunghezza ancoraggi armature	
-Calcolata in funzione della σ f	
-Imposta come multiplo del diametro	20
Lunghezza minima pari a <m>	0.5
-Inserire solo armatura al centro della parete	No
Modalità di progettazione e verifica armatura verticale	
-In funzione delle zone di incidenza elementi	
-In funzione delle sollecitazioni globali	x
-Inserisci armatura di rinforzo nelle zone di incidenza elementi	Si
-Dimensione minima zone di incidenza elementi	Si
-Pari a multiplo dello spessore	1
-Passo di verifica	1.5

Relazione geotecnica tombino

-Trascura zone con pilastro inglobato	Si
-Effettuare verifiche nel piano della parete	No
-Elimina armatura diffusa nelle zone di rinforzo	Si
Elimina armatura diffusa nell'architrave	Si
-Effettuare verifiche su sezioni verticali	No
-Passo di verifica	1
Controllare resistenza a taglio trasversale come sezione priva di armatura a taglio	No
Min. Af armatura diffusa <cmq/m>	3
Considera come parete debolmente armata ai sensi D.M. 08	No
-Modalità di valutazione parametri nel caso di sisma diverso per X e Y	
-Usa valore massimo	x
-Componi in direzione parete	
-Incremento del 50% delle forze assiali	
Sempre	x
-Solo per analisi sismiche statiche	
-Mai	
Coeff. β per controllo snellezza <m>	1
Rispetta i disposti del punto 7.4.4.5.2.1 solo per stati limite sismici	Si
Armatura diffusa	
Considera armatura con rete elettrosaldata	No
Armatura verticale o rete	
Elenco diametri utilizzabili 1 <mm>	10
Elenco diametri utilizzabili 2 <mm>	12
Elenco diametri utilizzabili 3 <mm>	
Elenco diametri utilizzabili 4 <mm>	
Elenco diametri utilizzabili 5 <mm>	
Elenco diametri utilizzabili 6 <mm>	
Elenco diametri utilizzabili 7 <mm>	
Passi utilizzabili	
-Minimo <cm>	15
-Massimo <cm>	30
-Incremento <cm>	5
-Modalità di completamento armatura	
-Adattata	x
-Terminata	
-Nessuna	
Armatura orizzontale	
Elenco diametri utilizzabili 1 <mm>	8
Elenco diametri utilizzabili 2 <mm>	10
Elenco diametri utilizzabili 3 <mm>	
Elenco diametri utilizzabili 4 <mm>	
Elenco diametri utilizzabili 5 <mm>	
Elenco diametri utilizzabili 6 <mm>	
Elenco diametri utilizzabili 7 <mm>	
Passi utilizzabili	
-Minimo <cm>	10
-Massimo <cm>	30
-Incremento <cm>	5
Tipo di armatura orizzontale	
-Dritta	x
-Con risvolti di estremità	
-Modalità di chiusura orizzontale	
-Nessuna chiusura	
-Chiusura con ferri ad U	x
-Chiusura con staffe	
-Lunghezza armatura di chiusura	
-Multiplo dello spessore pari a	
-Lunghezza fissa pari a <cm>	0.5
-Tipo di ottimizzazione armatura	
-Minimizza il peso complessivo dei ferri	x
-Minimizza il numero dei ferri	
Armatura di rinforzo	
Elenco diametri utilizzabili 1 <mm>	16
Elenco diametri utilizzabili 2 <mm>	
Elenco diametri utilizzabili 3 <mm>	
Elenco diametri utilizzabili 4 <mm>	
Elenco diametri utilizzabili 5 <mm>	
Elenco diametri utilizzabili 6 <mm>	
Elenco diametri utilizzabili 7 <mm>	
Numero minimo ferri	2
Interferro minimo <cm>	10
-Aggiungi staffe chiuse	Si
-Stesso diametro armatura diffusa orizzontale	x
-Diametro imposto	
-Stesso passo armatura diffusa orizzontale	x
-Passo imposto	
Armatura secondaria	
Diametro ferri di collegamento <mm>	6

Relazione geotecnica tombino

Numero ferri di collegamento (a mq)	6
Lunghezza ancoraggio ferri di collegamento <cm>	10
Dati per progettazione agli stati limite	
Gruppo di esigenza	
-Ambiente poco aggressivo	x
-Ambiente moderatamente aggressivo	
-Ambiente molto aggressivo	
Usa dominio N-M per flessioni rette	No
-Ricerca della sicurezza con sforzo normale costante	
-Ricerca della sicurezza con eccentricità costante	
Controllo rapporto X/D	No
Barre da considerare tese per verifiche a taglio	
-Solo le barre con deformazione percentuale rispetto alla barra più tesa non inferiore al <%>	30
-Tutte le barre in trazione	

Solette/Platee

Generali	
Parametri di progetto	
Controllo resistenza a taglio allo S.L.U. DM 96	No
Progetto e verifica con metodo d'integrazione	No
-Massima dimensione della linea d'integrazione	1
Calcolo armature con metodo di Wood	No
Accoppia pilastri per calcolo punzonamento	Si
-Massima distanza come un moltiplicatore dello spessore	1.5
Verifiche a taglio per elementi esistenti come per elementi nuovi	Si
Parametri di disegno	
Disposizione disegno	2A
Particolari nel disegno principale	
-Eliminare le quotature	No
-Eliminare le campiture	No
-Eliminare la numerazione dei pilastri	No
-Eliminare la numerazione delle travi e dei muri	No
Particolari nei disegni secondari	
-Eliminare le quotature	Si
-Eliminare le campiture	Si
-Eliminare la numerazione dei pilastri	Si
-Eliminare la numerazione delle travi e dei muri	Si
Disegno armatura diffusa	No
Posizione particolari punzonamento	In automatico
Copriferro per calcolo lunghezza ferri <cm>	3.5
Risvoltare al bordo i ferri	
-Inferiori	Si
-Superiori	Si
Lunghezza risvolti ferri al bordo	Pari all'altezza meno due volte il copriferro
Disegno particolare ferri al bordo	Si
Scala disegno particolare ferri al bordo	20
Calcolo lunghezza ferri semplificato	No
Stampe	
Tipo di relazione	Sintetica

Specifici	1	2
Materiali		
-Considera come elemento esistente	No	No
-Calcestruzzo		
-Livello di conoscenza	LC2	LC2
-Fattore di confidenza	1.2	1.2
-Tipo di calcestruzzo	C28/35	C28/35
-Rck calcestruzzo	350	350
-Modulo elastico <daN/cm ² >	325881	325881
-Resistenza caratteristica cilindrica (Fck)	290.5	290.5
-Resistenza caratteristica a trazione (Fctk)	19.84	19.84
-Resistenza media (Fcm) <daN/cm ² >	370.5	370.5
-Resistenza media a trazione (Fctm) <daN/cm ² >	28.35	28.35
-σ amm. calcestruzzo <daN/cm ² >	110	110
-τc0 <daN/cm ² >	6.7	6.7
-τc1 <daN/cm ² >	19.7	19.7
-Riduci Fcd per tutte le verifiche secondo il D.M. 08	Si	Si
-γc per stati limite ultimi		
-Automatico	x	x
-Pari a		
-Acciaio		
-Livello di conoscenza	LC2	LC2

Relazione geotecnica tombino

-Fattore di confidenza	1.2	1.2
-Tipo di acciaio	B450C	B450C
-Modulo elastico <daN/cm ² >	2060000	2060000
-Tensione caratteristica di snervamento (Fyk) <daN/cm ² >	4500	4500
-Tensione media di snervamento (Fym) <daN/cm ² >	4500	4500
-Sigma amm. acciaio <daN/cm ² >	2600	2600
-Sigma amm. reti e tralicci <daN/cm ² >	2600	2600
-Allungamento per verifiche di duttilità (Agt) <%>	4	4
-γs per stati limite ultimi		
-Automatico	x	x
-Pari a		
-Coeff. di omogeneizzazione	15	15
Armatura a flessione		
Angolo d'armatura <grad>	0	0
Copriferro teorico superiore <cm>	3	3
Copriferro teorico inferiore <cm>	3	3
Tipo di progetto in doppia armatura		
-Tensione pari ai valori amm.		
-Tensione pari ai valori amm. con AfComp/AfTesa minore o pari a	1	1
-Tensione pari ai valori amm. con AfComp/AfTesa pari a		
Min. percentuale di regolamento		
-Platee di fondazione su suolo elastico	No	No
-Solette di elevazione	Si	Si
Controlla min. armatura di ripartizione	No	No
Elenco diametri utilizzabili 1 <mm>	10	10
Elenco diametri utilizzabili 2 <mm>	12	12
Elenco diametri utilizzabili 3 <mm>	14	14
Elenco diametri utilizzabili 4 <mm>	16	16
Elenco diametri utilizzabili 5 <mm>		
Elenco diametri utilizzabili 6 <mm>		
Elenco diametri utilizzabili 7 <mm>		
Passi utilizzabili		
-Minimo <cm>	15	15
-Massimo <cm>	30	30
-Incremento <cm>	5	5
Uniformizzazione interassi armatura	No	No
-Sempre		
-Nella stessa direzione		
-Nella stessa posizione		
Uniformizzazione diametri armatura	No	No
-Sempre		
-Nella stessa direzione		
-Nella stessa posizione		
Tipo di ottimizzazione armatura a flessione		
-Minimizza il numero dei ferri		
-Minimizza il peso complessivo dei ferri	x	x
Verifiche a taglio		
-Escludi punti di verifica sotto piramidi di punzonamento	No	No
-Escludi punti di verifica sotto muri/bidimensionali	No	No
Ancoraggi		
Fattore di riduzione per ancoraggio ferri	1	1
Lunghezza ancoraggi armature		
-Calcolata in funzione della Sigma _f	x	x
-Imposta come multiplo del diametro		
Lunghezza ancoraggi ferri punzonamento		
-Calcolata in funzione della Sigma _f	x	x
-Imposta come multiplo del diametro		
Armatura a punzonamento		
Fattore di riduzione altezza soletta/platea	0.9	0.9
Modifica altezza soletta/platea	Si	Si
Allargamento piastra pilastri in acciaio <cm>	5	5
Distanza dal bordo libero		
-Distanza come un moltiplicatore dello spessore	1	1
-Distanza imposta a <cm>		
Moltiplicatore altezza utile per valutare perimetro efficace (D.M. 08)	2	2
Tolleranza di posizionamento barre		
-Distanza come un moltiplicatore dello spessore	0.1	0.1
-Distanza imposta a <cm>		
Elenco diametri utilizzabili 1 <mm>	12	12
Elenco diametri utilizzabili 2 <mm>	14	14
Elenco diametri utilizzabili 3 <mm>	16	16
Elenco diametri utilizzabili 4 <mm>	18	18
Elenco diametri utilizzabili 5 <mm>	20	20
Elenco diametri utilizzabili 6 <mm>		
Elenco diametri utilizzabili 7 <mm>		
Passi utilizzabili		
-Minimo <cm>	10	10

Relazione geotecnica tombino

-Massimo <cm>	20	20
-Incremento <cm>	2	2
Tipo di ottimizzazione armatura a punzonamento		
-Minimizza il numero dei ferri	x	x
-Minimizza il peso complessivo dei ferri		
Dati per progettazione agli stati limite		
Gruppo di esigenza		
-Ambiente poco aggressivo	x	x
-Ambiente moderatamente aggressivo		
-Ambiente molto aggressivo		
Usa dominio N-M per flessioni rette	No	No
-Ricerca della sicurezza con sforzo normale costante		
-Ricerca della sicurezza con eccentricità costante		
Controllo rapporto X/D	No	No
Barre da considerare tese per verifiche a taglio		
-Solo le barre con deformazione percentuale rispetto		
Incremento <%>	30	30
-Tutte le barre in trazione		

Verifiche e armature solette/platee

Simbologia

Nodo	= Numero del nodo
X	= Coordinata X del nodo
Y	= Coordinata Y del nodo
DV	= Direzione di verifica
	XX = Verifica per momento Mxx
	YY = Verifica per momento Myy
CC	= Numero della combinazione delle condizioni di carico elementari
TCC	= Tipo di combinazione di carico
	SLU = Stato limite ultimo
	SLU S = Stato limite ultimo (azione sismica)
	SLE R = Stato limite d'esercizio, combinazione rara
	SLE F = Stato limite d'esercizio, combinazione frequente
	SLE Q = Stato limite d'esercizio, combinazione quasi permanente
	SLD = Stato limite di danno
	SLV = Stato limite di salvaguardia della vita
	SLC = Stato limite di prevenzione del collasso
	SLO = Stato limite di operatività
	SLU I = Stato limite di resistenza al fuoco
c	= Ricoprimento dell'armatura
s	= Distanza minima tra le barre
K3	= Coefficiente di forma del diagramma delle tensioni prima della fessurazione
s _{rm}	= Distanza media tra le fessure
Φ	= Diametro della barra
A _s	= Area complessiva dei ferri nell'area di calcestruzzo efficace
A _{c eff}	= Area di calcestruzzo efficace
σ _s	= Tensione nell'acciaio nella sezione fessurata
σ _{sr}	= Tensione nell'acciaio corrispondente al raggiungimento della resistenza a trazione nel calcestruzzo
ε _{sm}	= Deformazione unitaria media dell'armatura (*1000)
Wk	= Apertura delle fessure
AfE S	= Area di ferro effettiva totale presente nel punto di verifica, superiore
AfE I	= Area di ferro effettiva totale presente nel punto di verifica, inferiore
Mom	= Momento flettente
Mu	= Momento ultimo
Sic.	= Sicurezza a rottura
Vsdu	= Taglio agente nella direzione del momento ultimo
Vrdu	= Taglio ultimo assorbibile dal solo calcestruzzo
σ _c	= Tensione nel calcestruzzo
σ _f	= Tensione nel ferro
Spess.	= Spessore
Cf sup	= Copriferro superiore
Cf inf	= Copriferro inferiore
Cls	= Tipo di calcestruzzo
Fck	= Resistenza caratteristica cilindrica a compressione del calcestruzzo
Fctk	= Resistenza caratteristica a trazione del calcestruzzo
Fcd	= Resistenza di calcolo a compressione del calcestruzzo
Fctd	= Resistenza di calcolo a trazione del calcestruzzo
Tp	= Tipo di acciaio
Fyk	= Tensione caratteristica di snervamento dell'acciaio
Fyd	= Resistenza di calcolo dell'acciaio

Armatura platea a quota 0.00

Caratteristiche delle sezioni e dei materiali utilizzati

Spess.	Cf sup	Cf inf	Cls	Fck	Fctk	Fcd	Fctd	Tp	Fyk	Fyd
<cm>	<cm>	<cm>		<daN/cmq>	<daN/cmq>	<daN/cmq>	<daN/cmq>		<daN/cmq>	<daN/cmq>
50	3	3	C28/35	290.5	19.84	164.62	13.23	B450C	4500	3913.04

Stato limite ultimo - Ferri longitudinali - Verifiche armatura

Nodo	X	Y	DV	CC	TCC	AfE S	AfE I	Mom	Mu	Sic.
	<m>	<m>				<cmq>	<cmq>	<daNm>	<daNm>	
-35	8	1.6	XX	49	SLU	2.62	2.62	-844.36	-4988.93	5.909
-64	11	3.2	XX	13	SLV	2.62	2.62	-348.38	-4988.93	14.320
-39	12	1.6	YY	49	SLU	5.13	2.62	-8484.81	-9429.71	1.111

Relazione geotecnica tombino

-65	12	3.2	YY	13	SLV	5.13	2.62	-4998.12	-9429.71	1.887
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Stato limite ultimo - Verifica a taglio del calcestruzzo

Nodo	X <m>	Y <m>	DV	CC	TCC	AfE S <cmq>	AfE I <cmq>	Vsdu <daN>	Vrdu <daN>
-65	12	3.2	XX	25	SLV	2.62	2.62	817.05	18831.4
-65	12	3.2	YY	49	SLU	5.13	2.62	11573.9	18831.4

Stato limite d'esercizio - Ferri longitudinali - Verifiche armatura

Nodo	X <m>	Y <m>	DV	CC	TCC	AfE S <cmq>	AfE I <cmq>	Mom <daNm>	σ_c <daN/cmq>	σ_f <daN/cmq>
-35	8	1.6	XX	53	SLE R	2.62	2.62	-593.39	4.47	502.72
-65	12	3.2	XX	55	SLE R	2.62	2.62	-11.43	0.09	9.68
-35	8	1.6	XX	61	SLE Q	2.62	2.62	-478.98	3.61	405.8
-65	12	3.2	XX	63	SLE Q	2.62	2.62	-8.06	0.06	6.83
-39	12	1.6	YY	53	SLE R	5.13	2.62	-5967	33.42	2616.01
-39	12	1.6	YY	61	SLE Q	5.13	2.62	-4819.2	26.99	2112.8

Verifiche stato limite di formazione delle fessure

Nodo	X <m>	Y <m>	DV	CC	TCC	c <mm>	s <mm>	K3	s_{rm} <mm>	Φ	A_s <cmq>	$A_{c\ eff}$ <cmq>	σ_s <daN/cmq>	σ_{sr} <daN/cmq>	ϵ_{sm}	Wk <mm>
-35	8	1.6	XX	61	SLE Q	25	140	0.2	196.08	10	0.79	115.85	405.8	10408.5	0.08	0.03
-65	12	3.2	XX	63	SLE Q	25	140	0.2	196.08	10	0.79	115.85	6.83	10408.5	0	0
-35	8	1.6	XX	57	SLE F	25	140	0.2	196.08	10	0.79	115.85	430.03	10408.5	0.08	0.03
-65	12	3.2	XX	59	SLE F	25	140	0.2	196.08	10	0.79	115.85	7.54	10408.5	0	0
-39	12	1.6	YY	61	SLE Q	23	196	0.19	224.02	14	1.54	205.44	2112.8	5517.71	0.41	0.16
-39	12	1.6	YY	57	SLE F	23	196	0.19	224.02	14	1.54	205.44	2238.6	5517.71	0.43	0.17

Armatura soletta a quota 2.50

Caratteristiche delle sezioni e dei materiali utilizzati

Spess. <cm>	Cf sup <cm>	Cf inf <cm>	Cls	Fck <daN/cmq>	Fctk <daN/cmq>	Fcd <daN/cmq>	Fctd <daN/cmq>	Tp	Fyk <daN/cmq>	Fyd <daN/cmq>
50	3	3	C28/35	290.5	19.84	164.62	13.23	B450C	4500	3913.04

Stato limite ultimo - Ferri longitudinali - Verifiche armatura

Nodo	X <m>	Y <m>	DV	CC	TCC	AfE S <cmq>	AfE I <cmq>	Mom <daNm>	Mu <daNm>	Sic.
-148	4	1.6	XX	49	SLU	2.62	2.62	732.65	4988.93	6.809
-171	1	3.2	XX	19	SLV	2.62	2.62	266.11	4988.93	18.747
-144	0	1.6	YY	50	SLU	2.62	4.52	7347.69	8369	1.139
-170	0	3.2	YY	22	SLV	2.62	4.52	3871.56	8369	2.162

Stato limite ultimo - Verifica a taglio del calcestruzzo

Nodo	X <m>	Y <m>	DV	CC	TCC	AfE S <cmq>	AfE I <cmq>	Vsdu <daN>	Vrdu <daN>
-118	0	0	XX	13	SLV	2.62	2.62	517.34	18831.4
-170	0	3.2	YY	51	SLU	2.62	4.52	9705.16	18831.4

Stato limite d'esercizio - Ferri longitudinali - Verifiche armatura

Nodo	X <m>	Y <m>	DV	CC	TCC	AfE S <cmq>	AfE I <cmq>	Mom <daNm>	σ_c <daN/cmq>	σ_f <daN/cmq>
-148	4	1.6	XX	53	SLE R	2.62	2.62	506.27	3.81	428.92
-148	4	1.6	XX	61	SLE Q	2.62	2.62	391.78	2.95	331.92
-144	0	1.6	YY	54	SLE R	2.62	4.52	5076	30.01	2516.62
-144	0	1.6	YY	62	SLE Q	2.62	4.52	3927.28	23.22	1947.1

Verifiche stato limite di formazione delle fessure

Nodo	X <m>	Y <m>	DV	CC	TCC	c <mm>	s <mm>	K3	s_{rm} <mm>	Φ	A_s <cmq>	$A_{c\ eff}$ <cmq>	σ_s <daN/cmq>	σ_{sr} <daN/cmq>	ϵ_{sm}	Wk <mm>
-148	4	1.6	XX	61	SLE Q	25	140	0.2	196.08	10	0.79	115.85	331.92	10408.5	0.06	0.02
-152	8	1.6	XX	58	SLE F	25	140	0.2	196.08	10	0.79	115.85	356.17	10408.5	0.07	0.02
-144	0	1.6	YY	62	SLE Q	24	168	0.19	210.66	12	1.13	157.67	1947.1	7360.9	0.38	0.14
-144	0	1.6	YY	58	SLE F	24	168	0.19	210.66	12	1.13	157.67	2089.48	7360.9	0.41	0.15

Verifiche e armature pareti

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
 Zona = Zona di verifica
 Zv = Coordinata Z di verifica
 Xi = Coordinata X iniziale
 Xf = Coordinata X finale
 Xv = Coordinata X di verifica
 TCC = Tipo di combinazione di carico
 SLU = Stato limite ultimo
 SLU S = Stato limite ultimo (azione sismica)
 SLE R = Stato limite d'esercizio, combinazione rara

Relazione geotecnica tombino

SLE F	= Stato limite d'esercizio, combinazione frequente
SLE Q	= Stato limite d'esercizio, combinazione quasi permanente
SLD	= Stato limite di danno
SLV	= Stato limite di salvaguardia della vita
SLC	= Stato limite di prevenzione del collasso
SLO	= Stato limite di operatività
SLU I	= Stato limite di resistenza al fuoco
N	= Sforzo normale
My	= Momento flettente intorno all'asse Y
Nu	= Sforzo normale ultimo
Myu	= Momento ultimo intorno all'asse Y
Sic.	= Sicurezza a rottura
σ_c	= Tensione nel calcestruzzo
σ_f	= Tensione nel ferro
c	= Ricoprimento dell'armatura
s	= Distanza minima tra le barre
K3	= Coefficiente di forma del diagramma delle tensioni prima della fessurazione
s_{rm}	= Distanza media tra le fessure
Φ	= Diametro della barra
A_s	= Area complessiva dei ferri nell'area di calcestruzzo efficace
$A_{c\ eff}$	= Area di calcestruzzo efficace
σ_s	= Tensione nell'acciaio nella sezione fessurata
σ_{sr}	= Tensione nell'acciaio corrispondente al raggiungimento della resistenza a trazione nel calcestruzzo
ϵ_{sm}	= Deformazione unitaria media dell'armatura (*1000)
Wk	= Apertura delle fessure
Ty	= Taglio in dir. Y
Vsdu	= Taglio agente nella direzione del momento ultimo
VRsd	= Taglio ultimo lato armatura
VRcd	= Taglio ultimo lato calcestruzzo
Vrdu	= Taglio ultimo assorbibile dal solo calcestruzzo
Sic.T	= Sicurezza a rottura per taglio
Sez.	= Sezione di verifica
Spess.	= Spessore
Cf	= Copriferro
Cls	= Tipo di calcestruzzo
Fck	= Resistenza caratteristica cilindrica a compressione del calcestruzzo
Fctk	= Resistenza caratteristica a trazione del calcestruzzo
Fcd	= Resistenza di calcolo a compressione del calcestruzzo
Fctd	= Resistenza di calcolo a trazione del calcestruzzo
Tp	= Tipo di acciaio
Fyk	= Tensione caratteristica di snervamento dell'acciaio
Fyd	= Resistenza di calcolo dell'acciaio

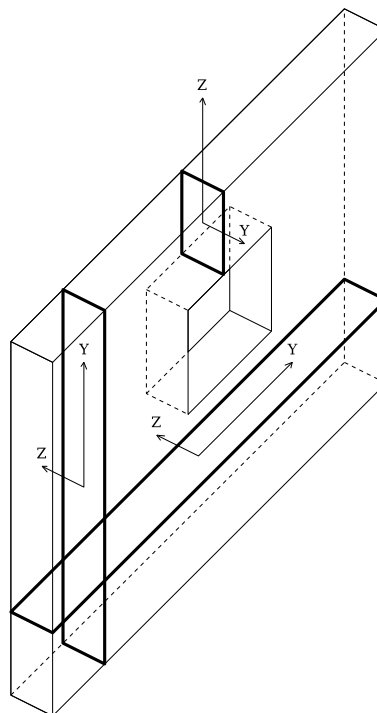


Figura numero 4: Riferimenti sezione

Parete n. 105

Caratteristiche delle sezioni e dei materiali utilizzati

Sez.	Spess. <cm>	Cf <cm>	Cls	Fck <daN/cm²>	Fctk <daN/cm²>	Fcd <daN/cm²>	Fctd <daN/cm²>	Tp	Fyk <daN/cm²>	Fyd <daN/cm²>
Oriz.	30	4.1	C28/35	290.5	19.84	164.62	13.23	B450C	4500	3913.04

Verifiche su sezioni orizzontali

Relazione geotecnica tombino

Stato limite ultimo - Armatura a flessione

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	Nu <daN>	Myu <daNm>	Sic.
19	SLV	Diff.	0	0	12	-75328.6	-35673.8	-75328.6	-60575.9	1.698
52	SLU	Diff.	1.25	0	12	-162947	-14691.8	-162947	-70877.5	4.824
13	SLV	Diff.	2.5	0	12	-106531	-33047.4	-106531	-64237.9	1.944

Stato limite d'esercizio - Armatura a flessione

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	σ_c <daN/cm ² >	σ_f <daN/cm ² >
56	SLE R	Diff.	0	0	12	-120512	-15082.7	15.65	227.47
64	SLE Q	Diff.	0	0	12	-97472.4	-12589	13.25	207.1
55	SLE R	Diff.	1.25	0	12	-114928	-10326.7	9.57	113.33
56	SLE R	Diff.	1.25	0	12	-113012	-10298.9	9.57	112.82
63	SLE Q	Diff.	1.25	0	12	-91887.7	-7831.31	7.21	86.68
55	SLE R	Diff.	2.5	0	12	-107428	-11817.3	11.6	127.63
63	SLE Q	Diff.	2.5	0	12	-84387.6	-9320.31	9.17	100.64

Verifiche stato limite di formazione delle fessure

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	c <mm>	s <mm>	K3	s_{rm} <mm>	Φ	A_s <cm ² >	$A_{c\ eff}$ <cm ² >	σ_s <daN/cm ² >	σ_{sr} <daN/cm ² >	ϵ_{sm}	Wk <mm>
64	SLE Q	Diff.	0	0	12	-97472.4	-12589	35	168	0.13	196.02	12	1.13	174.21	207.1	1768.63	0.04	0.01
60	SLE F	Diff.	0	0	12	-103232	-13212.5	35	168	0.13	196.02	12	1.13	174.21	212.07	1735.94	0.04	0.01
64	SLE Q	Diff.	1.25	0	12	-89972.3	-7803.53	35	168	0.13	196.02	12	1.13	174.21	30.28	613.46	0.01	0
60	SLE F	Diff.	1.25	0	12	-95732.3	-8427.37	35	168	0.13	196.02	12	1.13	174.21	35.1	644.98	0.01	0
63	SLE Q	Diff.	2.5	0	12	-84387.6	-9320.31	35	168	0.13	196.02	12	1.13	174.21	95.27	1235.99	0.02	0.01
59	SLE F	Diff.	2.5	0	12	-90147.6	-9944.56	35	168	0.13	196.02	12	1.13	174.21	101.24	1232.25	0.02	0.01

Parete n. 106

Caratteristiche delle sezioni e dei materiali utilizzati

Sez.	Spess. <cm>	Cf <cm>	Cls	Fck <daN/cm ² >	Fctk <daN/cm ² >	Fcd <daN/cm ² >	Fctd <daN/cm ² >	Tp	Fyk <daN/cm ² >	Fyd <daN/cm ² >
Oriz.	30	4.1	C28/35	290.5	19.84	164.62	13.23	B450C	4500	3913.04

Verifiche su sezioni orizzontali

Stato limite ultimo - Armatura a flessione

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	Nu <daN>	Myu <daNm>	Sic.
13	SLV	Diff.	0	0	12	-75328.6	-35673.8	-75328.6	-60575.9	1.698
51	SLU	Diff.	1.25	0	12	-162947	-14691.8	-162947	-70877.4	4.824
19	SLV	Diff.	2.5	0	12	-106531	-33047.4	-106531	-64237.9	1.944

Stato limite d'esercizio - Armatura a flessione

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	σ_c <daN/cm ² >	σ_f <daN/cm ² >
55	SLE R	Diff.	0	0	12	-120512	-15082.7	15.65	227.47
63	SLE Q	Diff.	0	0	12	-97472.4	-12589	13.25	207.1
56	SLE R	Diff.	1.25	0	12	-114928	-10326.7	9.57	113.33
55	SLE R	Diff.	1.25	0	12	-113012	-10298.9	9.57	112.82
64	SLE Q	Diff.	1.25	0	12	-91887.7	-7831.31	7.21	86.68
56	SLE R	Diff.	2.5	0	12	-107428	-11817.3	11.6	127.63
64	SLE Q	Diff.	2.5	0	12	-84387.6	-9320.31	9.17	100.64

Verifiche stato limite di formazione delle fessure

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	c <mm>	s <mm>	K3	s_{rm} <mm>	Φ	A_s <cm ² >	$A_{c\ eff}$ <cm ² >	σ_s <daN/cm ² >	σ_{sr} <daN/cm ² >	ϵ_{sm}	Wk <mm>
63	SLE Q	Diff.	0	0	12	-97472.4	-12589	35	168	0.13	196.02	12	1.13	174.21	207.1	1768.63	0.04	0.01
59	SLE F	Diff.	0	0	12	-103232	-13212.5	35	168	0.13	196.02	12	1.13	174.21	212.07	1735.94	0.04	0.01
63	SLE Q	Diff.	1.25	0	12	-89972.3	-7803.53	35	168	0.13	196.02	12	1.13	174.21	30.28	613.46	0.01	0
59	SLE F	Diff.	1.25	0	12	-95732.3	-8427.37	35	168	0.13	196.02	12	1.13	174.21	35.1	644.98	0.01	0
64	SLE Q	Diff.	2.5	0	12	-84387.6	-9320.31	35	168	0.13	196.02	12	1.13	174.21	95.27	1235.99	0.02	0.01
60	SLE F	Diff.	2.5	0	12	-90147.6	-9944.56	35	168	0.13	196.02	12	1.13	174.21	101.24	1232.25	0.02	0.01

Geotecnica

Elenco colonne stratigrafiche

Simbologia

St.	=Strato
z	=Profondità della superficie superiore dello strato
Unità geotecnica	=Unità geotecnica
Class.	=Classificazione
	Coes. = Coesivo
	Inc. = Incoerente
	Roc. = Roccia
	N. c. = Non classificato

Colonna stratigrafica numero 1

St.	z <m>	Unità geotecnica	Class.
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Relazione geotecnica tombino

1	01 Argilla bassa o media plasticità alta consistenza	Coes.
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Falda non presente

Elenco unità geotecniche

1 Argilla bassa o media plasticità alta consistenza:

Classificazione: Coesivo

Pesi:

- Peso specifico del terreno naturale: $\gamma = 1900.00$ daN/mc
- Peso specifico del terreno saturo: $\gamma_{sat} = 1950.00$ daN/mc

Proprietà indice:

- Indice di plasticità: $I_p = 10.00$ <%>

Parametri plastici:

- Angolo di attrito efficace: $\phi' = 20.00$ grad
- Coesione efficace: $c' = 2000.00$ daN/mq
- Coesione non drenata: $c_u = 20000.00$ daN/mq

Caratteristiche litostatiche:

- Grado di sovraconsolidazione: $OCR = 1.00$
- Coeff. di spinta a riposo: $\kappa_0 = 0.66$

Parametri elastici:

- Modulo elastico normale: $E = 750000.00$ daN/mq
- Modulo elastico tangenziale: $G = 267857.00$ daN/mq
- Esponente del parametro tensionale: $k_j = 0.00$
- Coeff. di Poisson: $\nu = 0.40$
- Modulo edometrico: $E_{ed} = 1610000.00$ daN/mq
- Modulo elastico non drenato: $E_u = 803571.00$ daN/mq

Report grafico complessivo

Colonna stratigrafica numero 1

Simbologia

St.	=Strato
z	=Profondità della superficie superiore dello strato
Unità geotecnica	=Unità geotecnica
Class.	=Classificazione
	Coes. = Coesivo
	Inc. = Incoerente
	Roc. = Roccia
	N. c. = Non classificato
γ	=Peso specifico del terreno naturale
γ_{sat}	=Peso specifico del terreno saturo
D_r	=Densità relativa
I_p	=Indice di plasticità
ϕ'	=Angolo di attrito efficace
c'	=Coesione efficace
c_u	=Coesione non drenata
OCR	=Grado di sovraconsolidazione
κ_0	=Coeff. di spinta a riposo
Crit.	=Criterio di progetto

St.	z <m>	Unità geotecnica	Class.	γ <daN/mc>	γ_{sat} <daN/mc>	D_r	I_p	ϕ' <grad>	c' <daN/mq>	c_u <daN/mq>	OCR	κ_0	Crit.
1	01	Argilla bassa o media plasticità alta consistenza	Coes.	1900	1950	0	10	20	2000	20000	1	0.66	1

Simbologia

St.	=Strato
z	=Profondità della superficie superiore dello strato
Unità geotecnica	=Unità geotecnica
Class.	=Classificazione
	Coes. = Coesivo
	Inc. = Incoerente
	Roc. = Roccia
	N. c. = Non classificato
γ	=Peso specifico del terreno naturale
γ_{sat}	=Peso specifico del terreno saturo
D_r	=Densità relativa
I_p	=Indice di plasticità
ϕ'	=Angolo di attrito efficace
c'	=Coesione efficace
c_u	=Coesione non drenata
OCR	=Grado di sovraconsolidazione
κ_0	=Coeff. di spinta a riposo
Crit.	=Criterio di progetto

St.	z	E	G	k_j	ν	E_{ed}	E_u	Crit.
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Relazione geotecnica tombino

	<m>	<daN/mq>	<daN/mq>			<daN/mq>	<daN/mq>	
1	0	750000	267857	0	0.4	1610000	803571	1

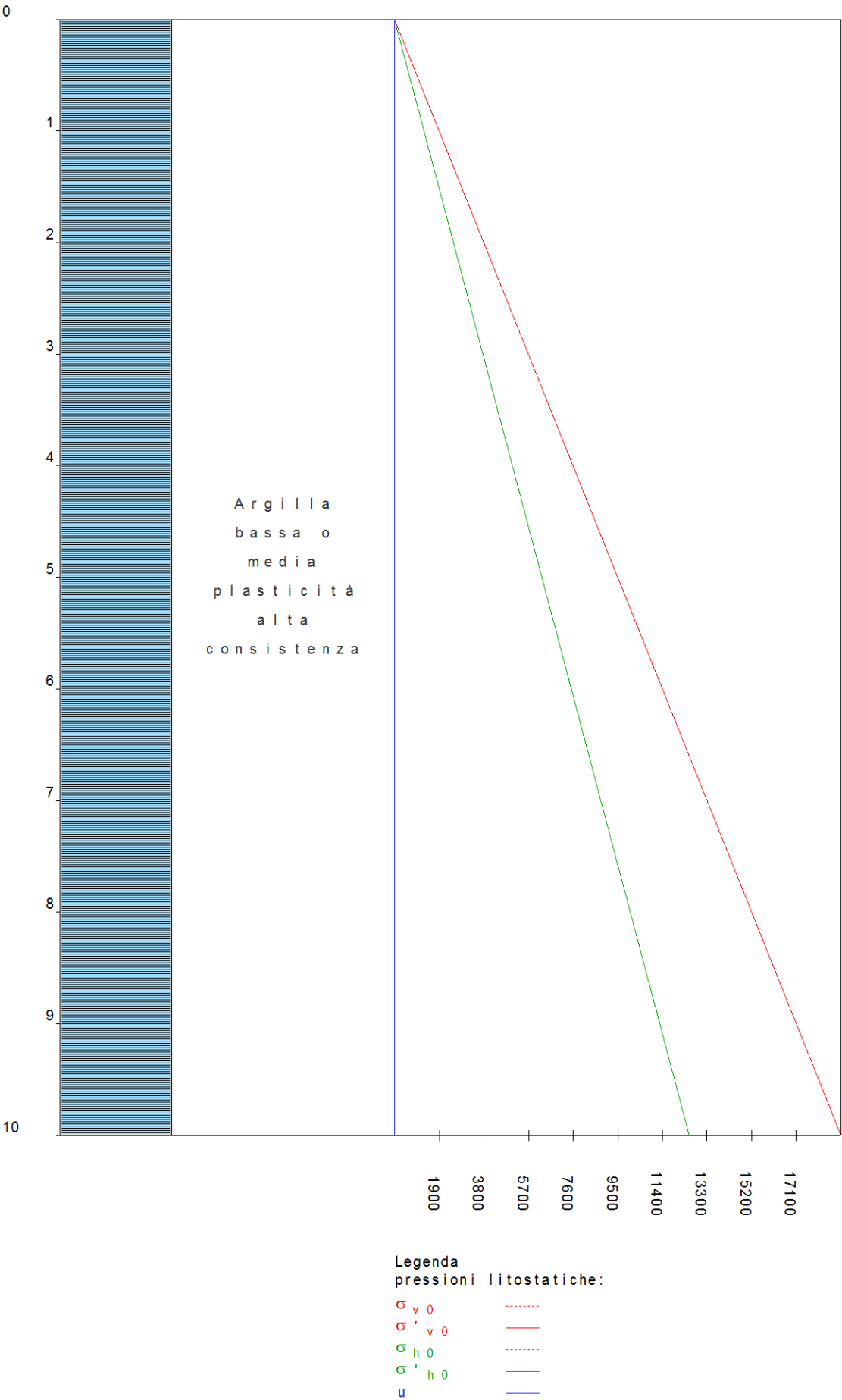


Figura numero 5: Colonna stratigrafica numero 1

Le verifiche degli elementi di fondazione sono state effettuate utilizzando l'approccio 2.

Coefficienti parziali per le azioni, per verifiche in condizioni statiche:

Permanenti strutturali, sicurezza a favore $\gamma_A = 1.00$;
 Permanenti strutturali, sicurezza a sfavore $\gamma_A = 1.30$;
 Permanenti non strutturali, sicurezza a favore $\gamma_A = 0.00$;
 Permanenti non strutturali, sicurezza a sfavore $\gamma_A = 1.50$;
 Variabili, sicurezza a favore $\gamma_A = 0.00$;
 Variabili, sicurezza a sfavore $\gamma_A = 1.50$.

I coefficienti parziali per le azioni sono posti pari all'unità per le verifiche in condizioni sismiche.

Tali coefficienti sono comunque desumibili dalla tabella delle combinazioni delle CCE (Parametri di calcolo).

Coefficienti parziali per i parametri geotecnici:

Tangente dell'angolo di attrito $\gamma_M = 1.00$;
 Coesione efficace $\gamma_M = 1.00$;
 Coesione non drenata $\gamma_M = 1.00$;

Coefficienti parziali per la resistenza delle fondazioni superficiali:

Capacità portante $\gamma_R = 2.30$;
 Scorrimento $\gamma_R = 1.10$;

Fondazioni superficiali

Simbologia

B = Base della fondazione
 L = Lunghezza della fondazione ($L > B$)
 D = Profondità del piano di posa della fondazione
 β = Inclinazione del piano di campagna
 η = Inclinazione del piano di posa della fondazione
 γ_r = Peso specifico rappresentativo del terreno di fondazione
 $\sigma_{v0,f}$ = Pressione verticale alla profondità del piano di posa della fondazione
 ϕ'_r = Angolo di attrito rappresentativo del terreno di fondazione
 c'_r = Coesione efficace rappresentativa del terreno di fondazione
 N_q = Coefficiente di capacità portante relativo al sovraccarico laterale
 N_c = Coefficiente di capacità portante relativo alla coesione del terreno di fondazione
 N_g = Coefficiente di capacità portante relativo al peso del terreno di fondazione
 b_q = Fattore di inclinazione del piano di fondazione relativo a sovraccarico laterale
 b_c = Fattore di inclinazione del piano di fondazione relativo a coesione
 b_g = Fattore di inclinazione del piano di fondazione relativo a peso del terreno
 c_{ur} = Coesione non drenata rappresentativa del terreno di fondazione
 CC = Numero della combinazione delle condizioni di carico elementari
 N = Sforzo normale
 Tx = Taglio in dir. X
 Ty = Taglio in dir. Y
 Mx = Momento intorno all'asse X
 My = Momento intorno all'asse Y
 B' = Base della fondazione reagente
 L' = Lunghezza della fondazione reagente
 s_q = Fattore di forma relativo al sovraccarico laterale
 s_c = Fattore di forma relativo alla coesione
 s_g = Fattore di forma relativo al peso del terreno
 i_q = Fattore di inclinazione relativo al sovraccarico laterale
 i_c = Fattore di inclinazione relativo alla coesione
 i_g = Fattore di inclinazione relativo al peso del terreno
 q_{lim} = Pressione limite
 R_d = Resistenza di progetto (Carico limite)
 Sic. = Sicurezza a rottura

Verifiche capacità portante

Verifiche di capacità portante per rottura generale in condizioni statiche

Metodo utilizzato: Indicazioni EC7

Platea n. 403

$B=3.20$ <m> $L=12.00$ <m> $D=0.50$ <m> $\beta=0.00$ <grad> $\eta=0.00$ <grad> $\gamma_r=1900.00$ <daN/mc>
 $\sigma_{v0,f}=950.00$ <daN/mq>

Verifiche in condizioni drenate

$\phi'_r=20.00$ <grad> $c'_r=2000.00$ <daN/mq>
 $N_q=6.40$ $N_c=14.83$ $N_g=3.93$ $b_q=1.00$ $b_c=1.00$ $b_g=1.00$

Relazione geotecnica tombino

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B ' <m>	L ' <m>	s _q	s _c	s _g	i _q	i _c	i _g	q _{lim} <daN/mq>	R _d <daN>	Sic.
49	505859	-2429.4	0	-0	-6024.52	3.2	11.98	1.09	1.11	0.92	1	1	1	50508.5	841598	1.66
50	505859	2429.4	0	-0	6024.54	3.2	11.98	1.09	1.11	0.92	1	1	1	50508.5	841598	1.66
51	505859	-0	-2429.4	5693.72	0.01	3.18	12	1.09	1.11	0.92	1	1	1	50405.8	835638	1.65
52	505859	-0	2429.4	-5693.72	0.01	3.18	12	1.09	1.11	0.92	1	1	1	50405.8	835638	1.65

Verifiche in condizioni non drenate

c_{ur}=20000.00 <daN/mq>
N_q=1.00 N_c=5.14 b_q=0.00 b_c=1.00

CC	N <daN>	Tx <daN>	Ty <daN>	Mx <daNm>	My <daNm>	B ' <m>	L ' <m>	s _c	i _q	i _c	q _{lim} <daN/mq>	R _d <daN>	Sic.
49	505859	-2429.4	0	-0	-6024.52	3.2	11.98	1.05	0	1	109277	1820830	3.6
50	505859	2429.4	0	-0	6024.54	3.2	11.98	1.05	0	1	109277	1820830	3.6
51	505859	-0	-2429.4	5693.72	0.01	3.18	12	1.05	0	1	109228	1810800	3.58
52	505859	-0	2429.4	-5693.72	0.01	3.18	12	1.05	0	1	109228	1810800	3.58

Cedimenti

Metodo utilizzato: Bowles

Simbologia

B =Base della fondazione
L =Lunghezza della fondazione (L>B)
D =Profondità del piano di posa della fondazione
H =Spessore del terreno responsabile del cedimento
E_r =Modulo elastico rappresentativo del terreno di fondazione
v_r =Coefficiente di Poisson rappresentativo del terreno di fondazione
I_s =Coefficiente di influenza
I_f =Coefficiente di profondità
kw =Costante di sottofondo
CC =Numero della combinazione delle condizioni di carico elementari
N =Sforzo normale
q_{es} =Pressione di esercizio
Ced=Cedimento calcolato

Platea n. 403
B=3.20 <m> L=12.00 <m> D=0.50 <m> H=16.00 <m> E_r=750000.00 <daN/mq> v_r=0.40
I_s=0.75 I_f=0.97 kw=190945.00 <daN/mc>

CC	N <daN>	q _{es} <daN/mq>	Ced <cm>
1	315611	8219.05	4.3
2	315611	8219.05	4.3
3	315611	8219.05	4.3
4	315611	8219.05	4.3
5	315611	8219.05	4.3
6	315611	8219.05	4.3
7	315611	8219.05	4.3
8	315611	8219.05	4.3
9	315611	8219.05	4.3
10	315611	8219.05	4.3
11	315611	8219.05	4.3
12	315611	8219.05	4.3
13	315611	8219.05	4.3
14	315611	8219.05	4.3
15	315611	8219.05	4.3
16	315611	8219.05	4.3
17	315611	8219.05	4.3
18	315611	8219.05	4.3
19	315611	8219.05	4.3
20	315611	8219.05	4.3
21	315611	8219.05	4.3
22	315611	8219.05	4.3
23	315611	8219.05	4.3
24	315611	8219.05	4.3
25	315611	8219.05	4.3
26	315611	8219.05	4.3
27	315611	8219.05	4.3
28	315611	8219.05	4.3
29	315611	8219.05	4.3
30	315611	8219.05	4.3
31	315611	8219.05	4.3
32	315611	8219.05	4.3
33	315611	8219.05	4.3
34	315611	8219.05	4.3
35	315611	8219.05	4.3
36	315611	8219.05	4.3

Relazione geotecnica tombino

37	315611	8219.05	4.3
38	315611	8219.05	4.3
39	315611	8219.05	4.3
40	315611	8219.05	4.3
41	315611	8219.05	4.3
42	315611	8219.05	4.3
43	315611	8219.05	4.3
44	315611	8219.05	4.3
45	315611	8219.05	4.3
46	315611	8219.05	4.3
47	315611	8219.05	4.3
48	315611	8219.05	4.3
49	505859	13173.4	6.9
50	505859	13173.4	6.9
51	505859	13173.4	6.9
52	505859	13173.4	6.9
53	356039	9271.86	4.86
54	356039	9271.86	4.86
55	356039	9271.86	4.86
56	356039	9271.86	4.86
57	304199	7921.86	4.15
58	304199	7921.86	4.15
59	304199	7921.86	4.15
60	304199	7921.86	4.15
61	286919	7471.86	3.91
62	286919	7471.86	3.91
63	286919	7471.86	3.91
64	286919	7471.86	3.91